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United States Patent [19]

Weiland et al.

[11] **Patent Number:** 5,452,473[45] **Date of Patent:** Sep. 19, 1995

[54] **REVERSE LINK, TRANSMIT POWER CORRECTION AND LIMITATION IN A RADIOTELEPHONE SYSTEM**

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[73] **Assignee:** Qualcomm Incorporated, San Diego, Calif.

[21] **Appl. No.:** 203,151

[22] **Filed:** Feb. 28, 1994

[51] **Int. Cl.⁶** H04B 1/40; H04B 1/04; H04B 1/06

[52] **U.S. Cl.** 455/88; 455/89; 455/126; 455/127; 455/234.2; 330/129

[58] **Field of Search** 330/129, 132, 136; 455/73, 74, 67.1, 69, 70, 84, 73, 88, 89, 77, 115, 126, 127, 245.1, 232.1, 234.1, 234.2, 240.1, 246.1, 227, 177.1, 200.1; 375/1, 98

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Primary Examiner—Edward F. Urban

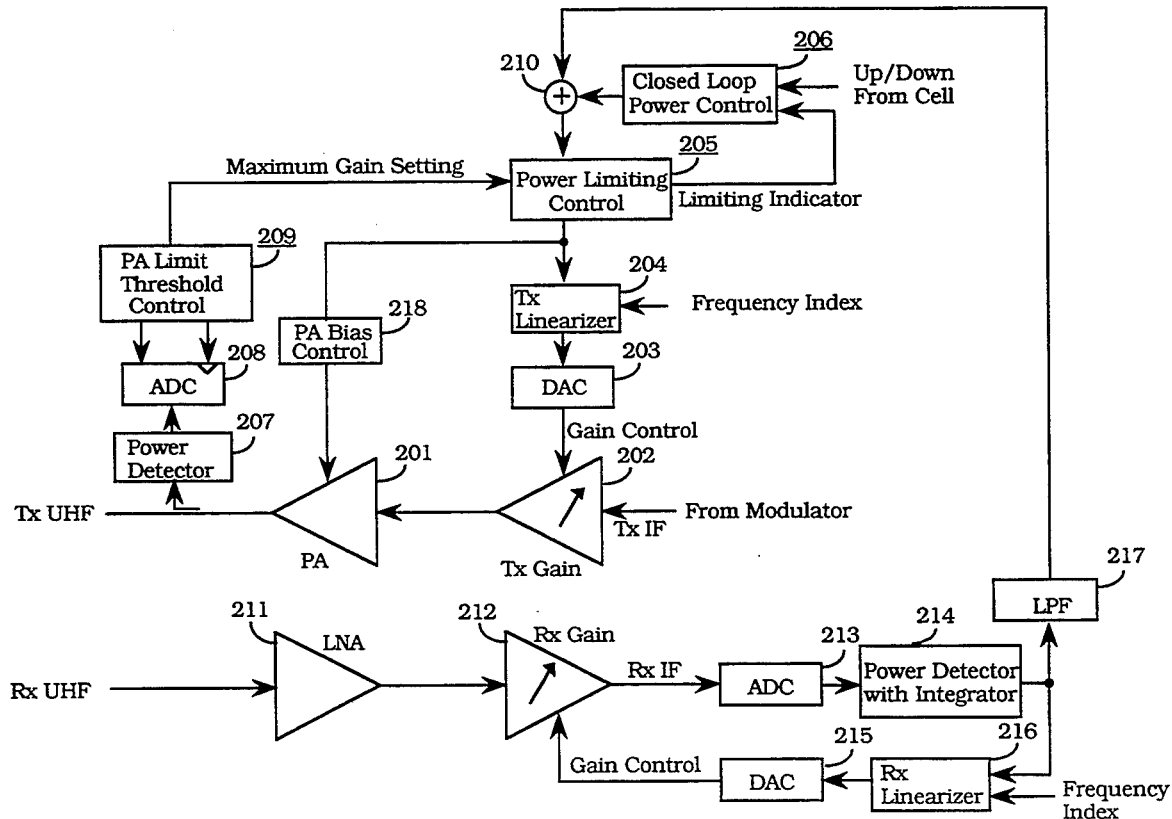
Assistant Examiner—Lisa Charouel

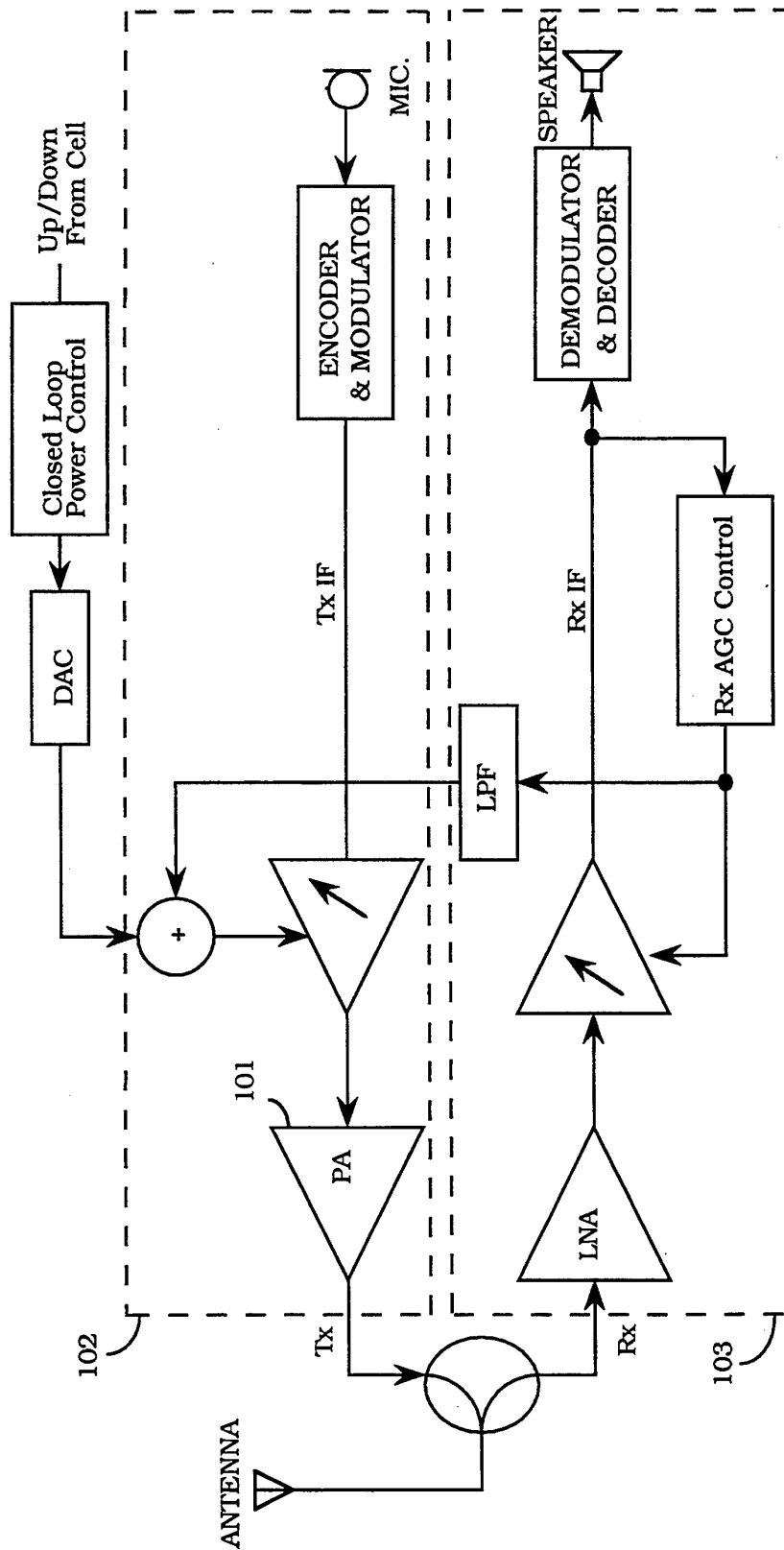
Attorney, Agent, or Firm—Kenneth W. Bolvin; Russell B. Miller

[57] ABSTRACT

The process and apparatus of the present invention limits the output power of a radiotelephone, operating in a cellular system in the preferred embodiment. This ensures the transmitted sidebands and synthesizer phase noise remains within a certain specification. This is accomplished by power detection and a correction accumulator that together generate a gain control signal by limiting the gain adjustment to a maximum value, even when the cell site communicating with the radiotelephone is sending power turn-up commands to the radiotelephone. This process includes dynamically correcting the output level of the transmitter due to gain variations in the transmitter stages or gain control elements.

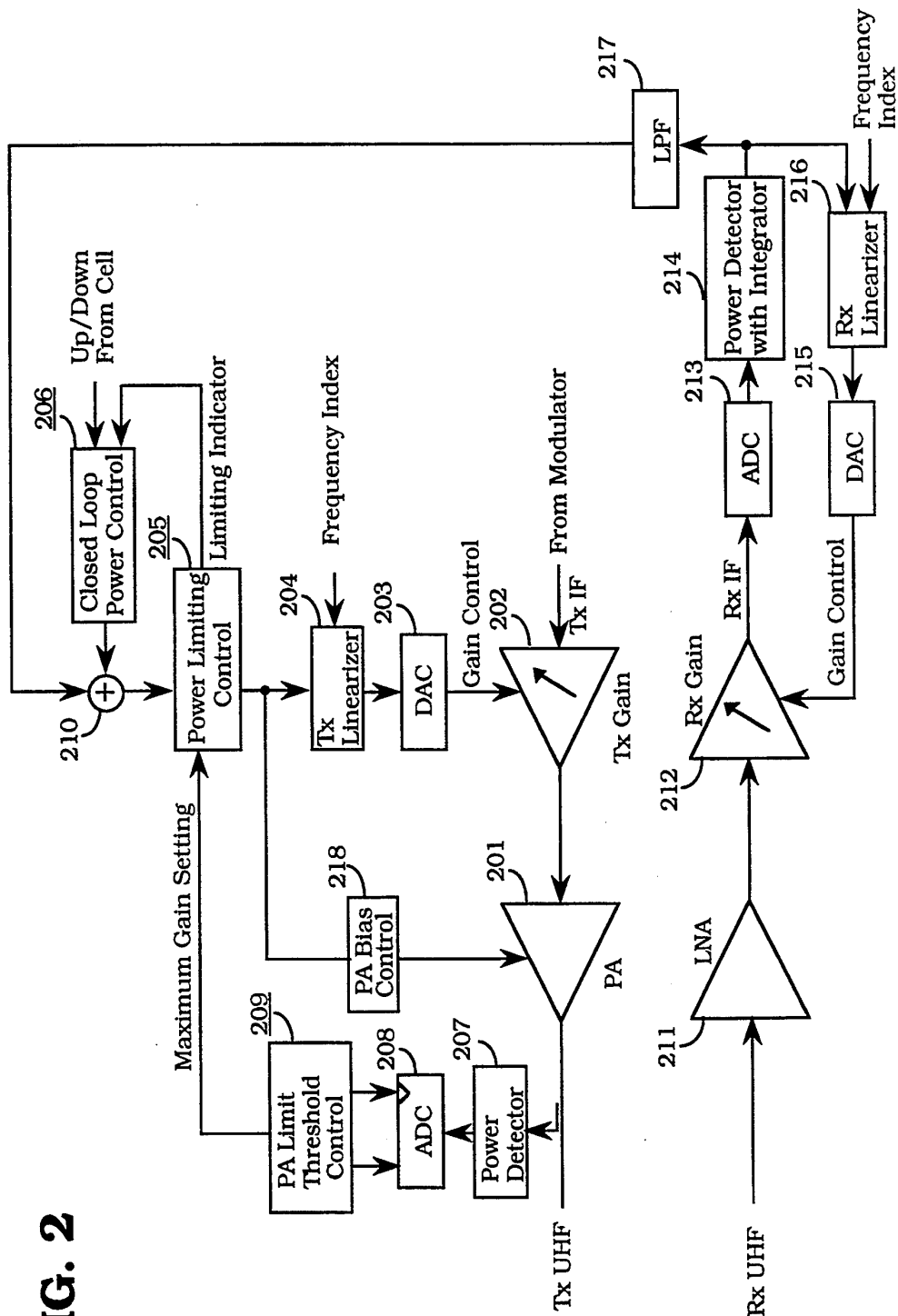
4 Claims, 9 Drawing Sheets

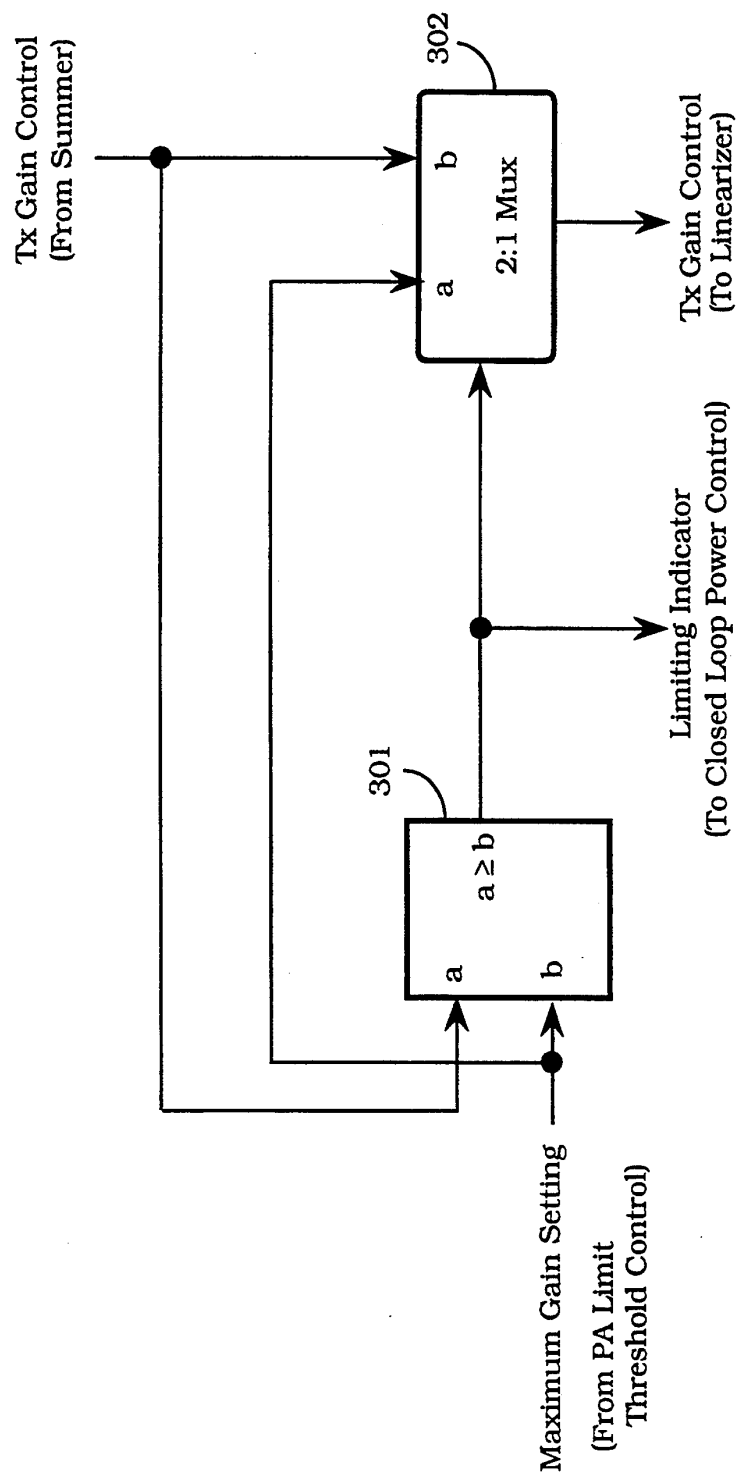




- Prior Art -

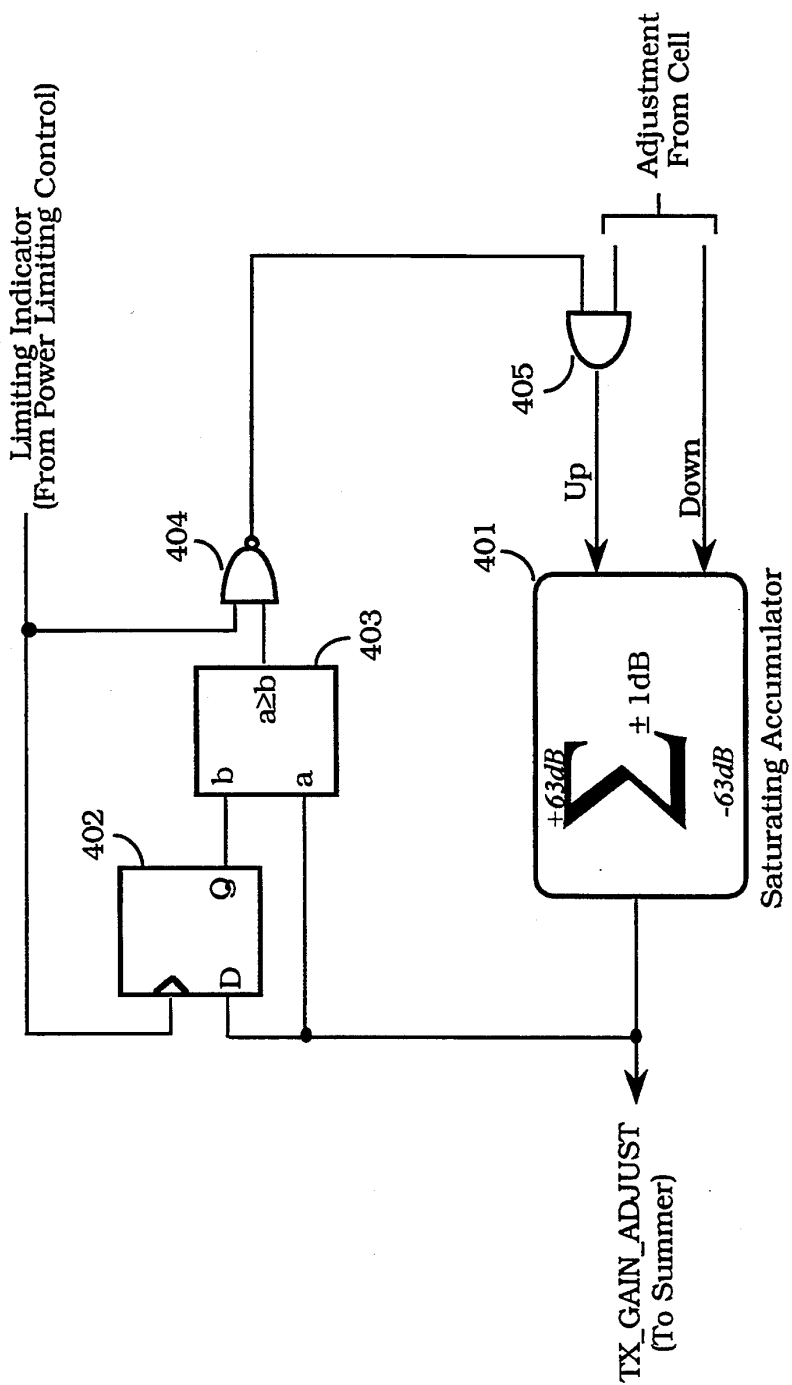
FIG. 1

FIG. 2

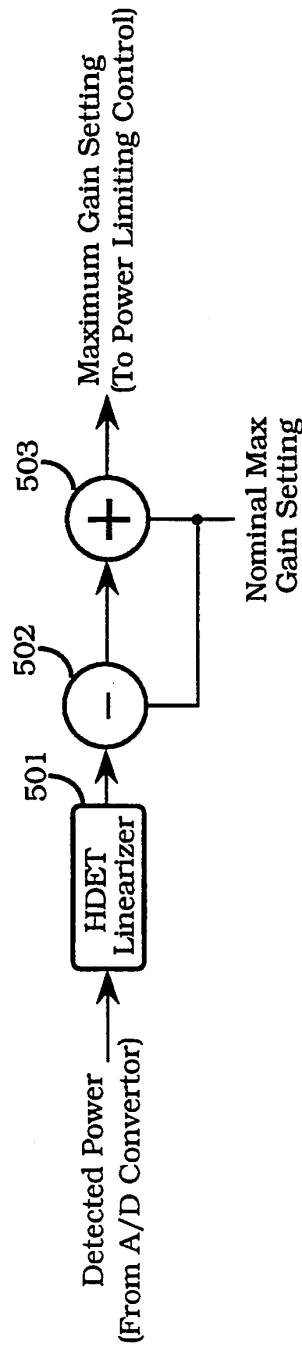


205

FIG. 3



206
FIG. 4



209

FIG. 5

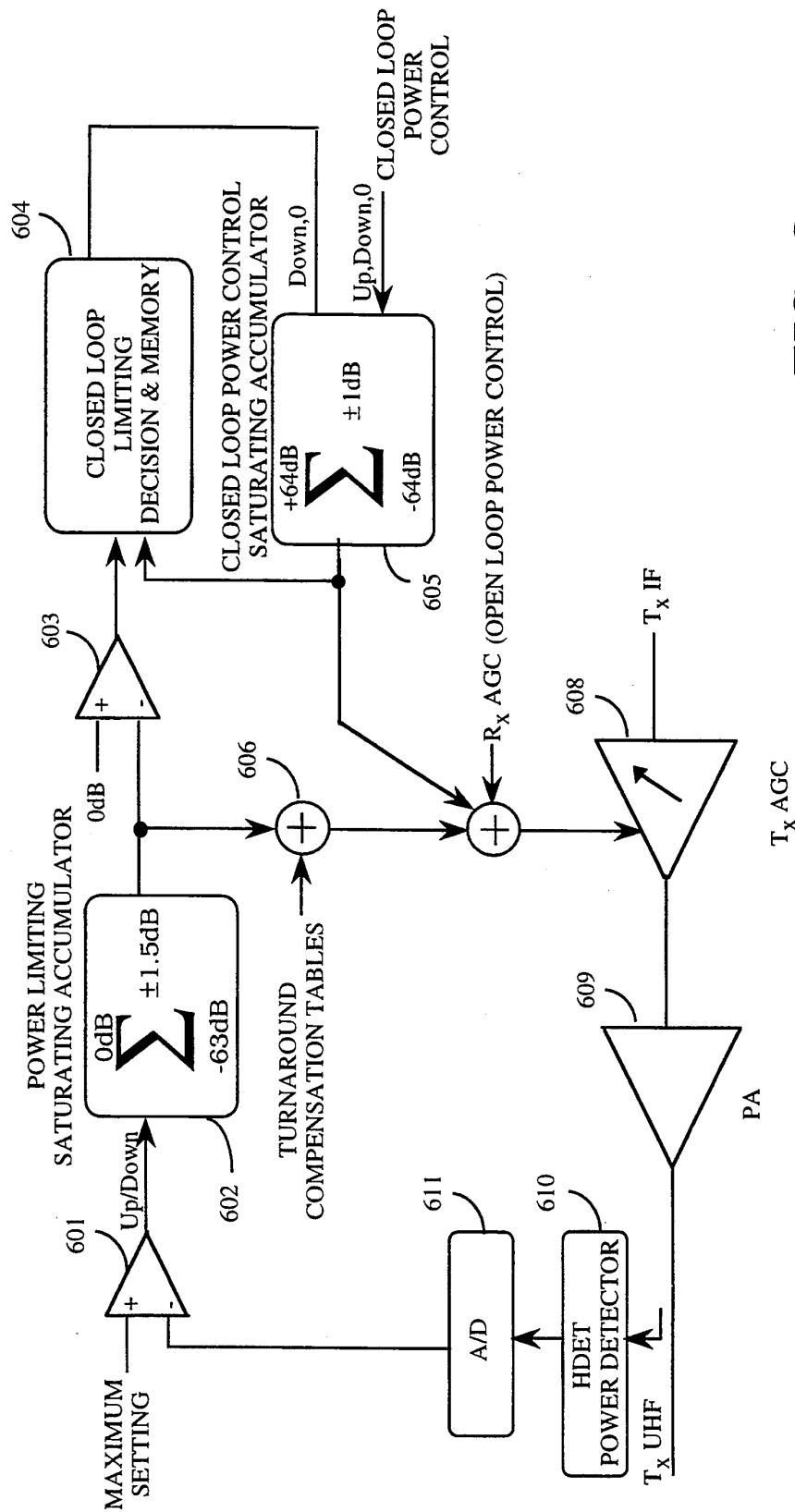


FIG. 6

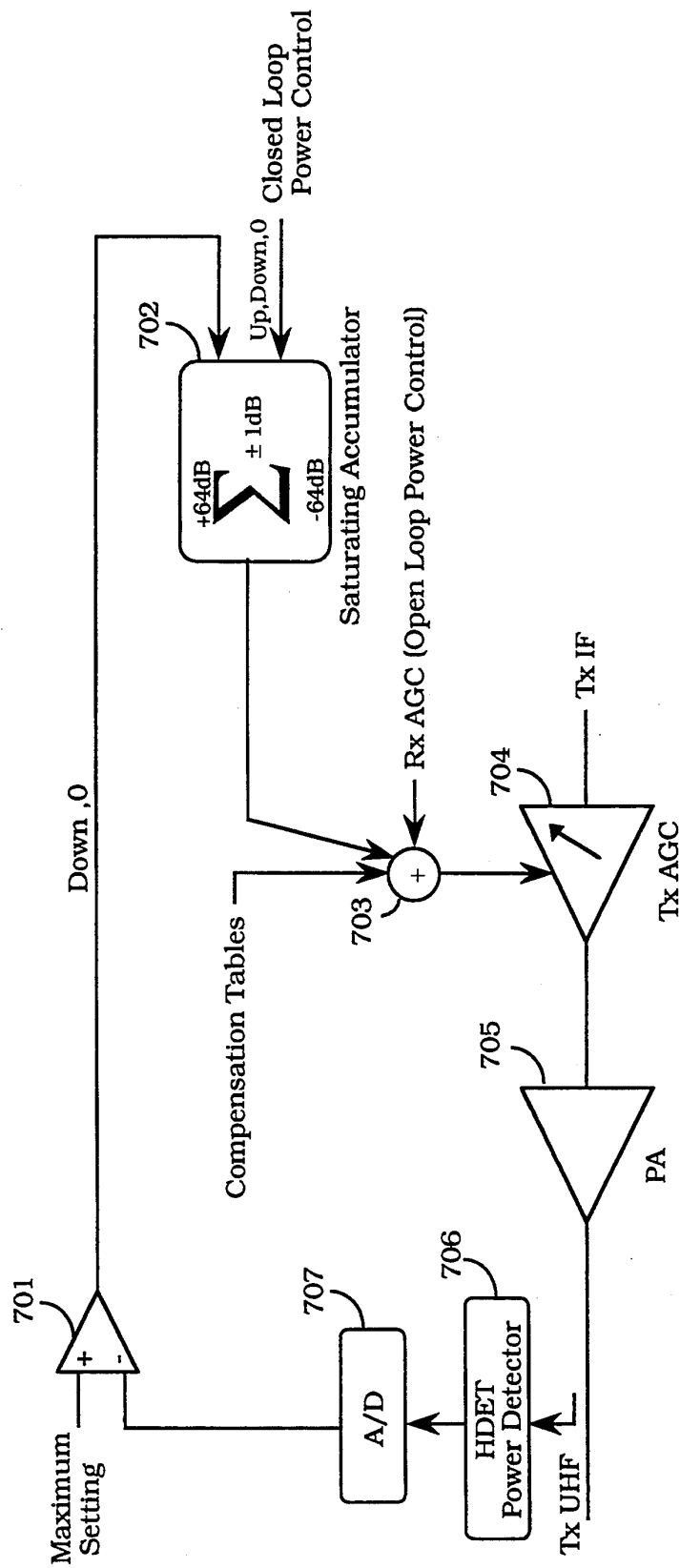


FIG. 7

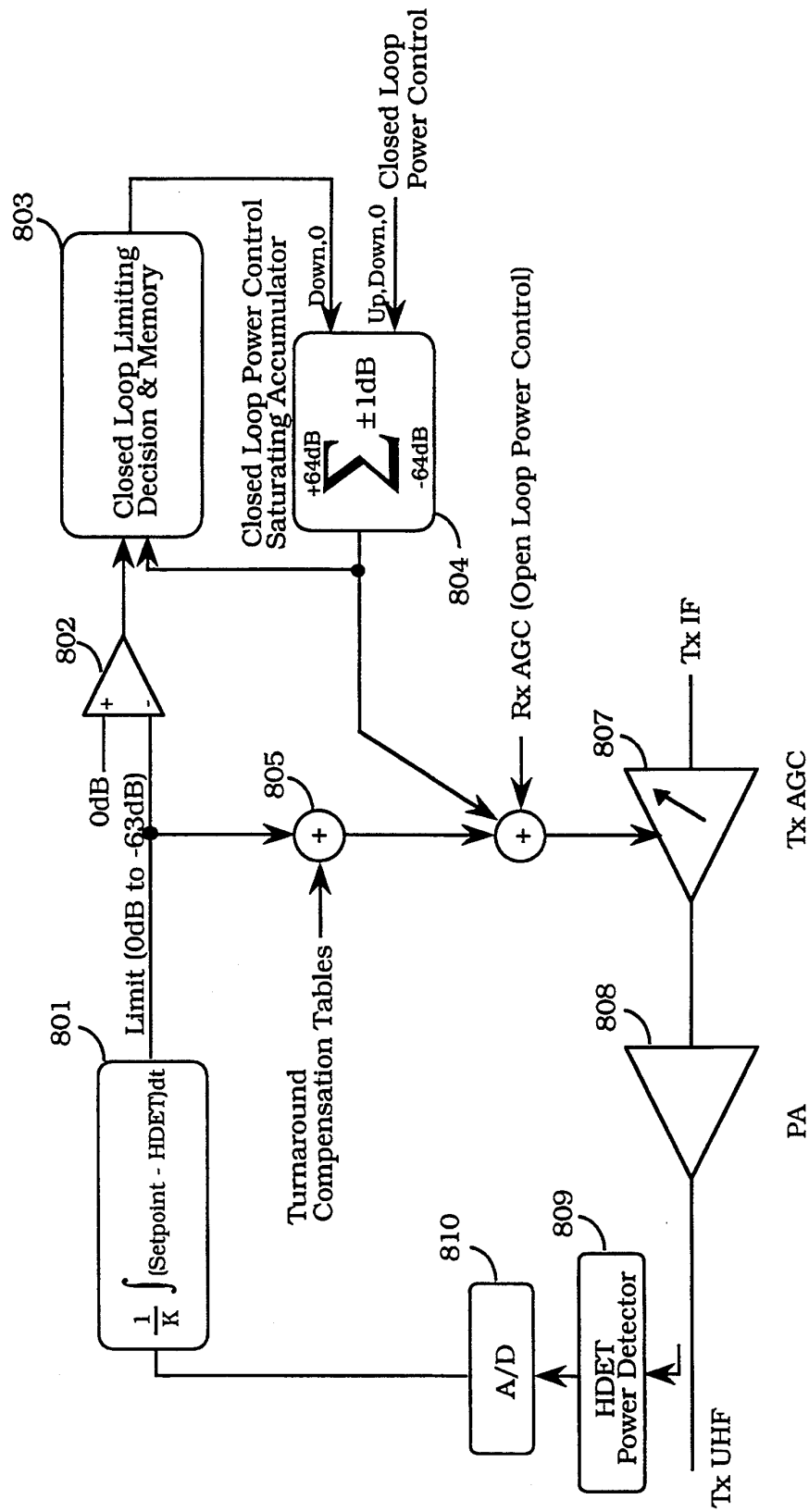


FIG. 8

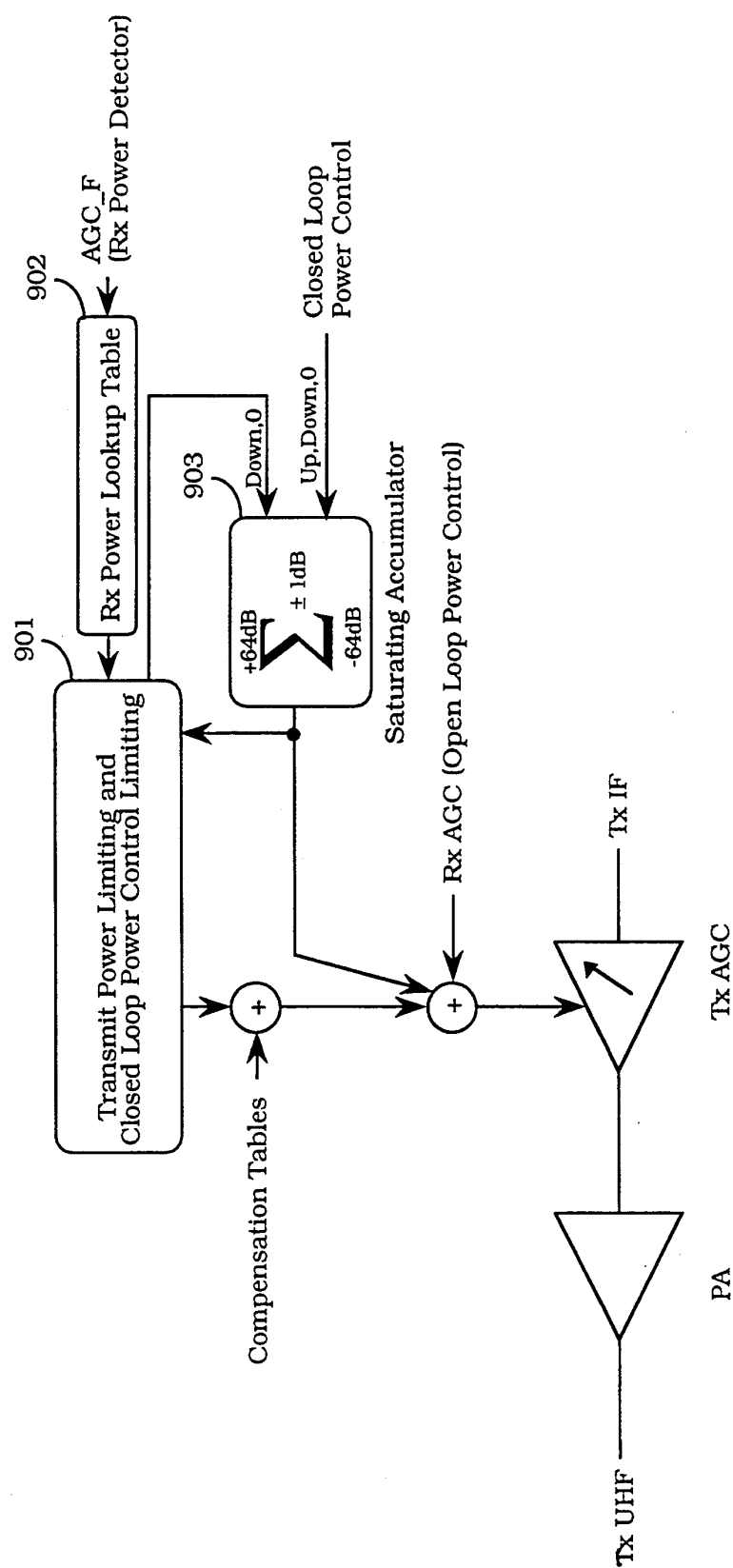


FIG. 9

REVERSE LINK, TRANSMIT POWER CORRECTION AND LIMITATION IN A RADIOTELEPHONE SYSTEM

BACKGROUND OF THE INVENTION

I. Field of the Invention

The present invention relates to radio communications. More particularly, the present invention relates to power control in a radiotelephone system.

II. Description of the Related Art

The Federal Communications Commission (FCC) governs the use of the radio frequency (RF) spectrum. The FCC allocates certain bandwidths within the RF spectrum for specific uses. A user of an allocated bandwidth of the RF spectrum must take measures to ensure that the radiated emissions inside and outside of that bandwidth are maintained within acceptable levels to avoid interfering with other users operating in the same and or other bandwidths. These levels are governed by both the FCC and the particular user groups of said bandwidth.

The 800 MHz cellular telephone system operates its forward link, the cell to radiotelephone transmission, in the bandwidth of 869.01 MHz to 893.97 MHz and the reverse link, the radiotelephone to cell transmission, in the bandwidth of 824.01 MHz to 848.97 MHz. The forward and reverse link bandwidths are split up into channels each of which occupies a 30 kHz bandwidth. A particular user of the cellular system may operate on one or several of these channels at a time. All users of the system must ensure that they are compliant with the level of radiated emissions allowable inside and outside of the channel or channels that they have been assigned.

There are several different techniques of modulation that can be used in the cellular telephone system. Two examples of modulation techniques are frequency division multiple access (FDMA) and code division multiple access (CDMA).

The FDMA modulation technique generates signals that occupy one channel at a time while the CDMA modulation technique generates signals that occupy several channels. Both of these techniques must control their return link radiated emissions to within acceptable limits inside and outside of the assigned channel or channels. For maximum system performance, users of the CDMA technique must carefully control the level of radiated power inside the channels in which they are operating.

FIG. 1 shows a typical prior cellular radiotelephone. In both an FDMA and a CDMA based radiotelephone, there exists the possibility of driving the power amplifier (101) in the transmitter beyond a point where acceptable out of channel radiated emissions are maintained. This is primarily due to the increased distortion output levels of the power amplifier (101) at high output powers. Also, driving the power amplifier (101) beyond a certain point can cause interference internal to the radio. For example, PA puncturing in CDMA affects synthesizer phase noise due to large current transitions. Both of these issues cause unacceptable radio performance.

Maintaining the proper on-channel output power can be difficult due to several undesirable effects in the radiotelephone hardware. For example, the CDMA based radio must implement a power control system that operates over a very wide dynamic range, 80 dB to

90 dB, such that the transmitted output power is linearly related to the received input power.

Closed loop and open loop power control together determine the return link transmit energy, as disclosed in U.S. Pat. No. 5,056,109 to Gilhousen et al. and assigned to Qualcomm, Incorporated. Therefore, the linear and nonlinear errors produced in both the receiver (103) and transmitter (102) RF sections can cause unacceptable power control performance. Also, both the FDMA and CDMA based radios must operate on different channels while maintaining acceptable output power levels. Variation in output power level and input power detection versus frequency can cause an unacceptable amount of error in the amount of return link transmitted energy.

These issues present significant problems to the designer of both FDMA and CDMA based radiotelephones. There is a resulting need for an effective, cost efficient means of correcting these problems.

SUMMARY OF THE INVENTION

The process of the present invention enables a radiotelephone to operate in a linear fashion over a wide dynamic range while maintaining acceptable transmit output power levels inside and outside of the return link bandwidth. The forward and return link power are measured by power detectors and input to an analog to digital converter accessible by both control hardware and/or software. The closed loop power control setting is also monitored. The radiotelephone uses the detected power levels and closed loop power control setting to index a set of correction tables that indicate the reverse link transmit power error and desired power amplifier biasing for the particular operating point. The radiotelephone also determines if the transmitter is operating above a maximum set point. The transmit gain and power amplifier biasing of the radiotelephone are adjusted to correct the undesired error and maintain the desired output power.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows a block diagram of a typical prior art radiotelephone frequency section for use in a radiotelephone system.

FIG. 2 shows a block diagram of the preferred embodiment power control correction implementation.

FIG. 3 shows a block diagram of the power limiting control section as related to FIG. 2.

FIG. 4 shows a block diagram of the closed loop power control section as related to FIG. 2.

FIG. 5 shows a block diagram of the PA limit threshold control section as related to FIG. 2.

FIG. 6 shows an alternate embodiment of the present invention that employs a power limiting control system based on accumulator feedback control.

FIG. 7 shows an alternate embodiment of the present invention that employs a power limiting control system based on the closed loop power control accumulator.

FIG. 8 shows an alternate embodiment of the present invention that employs a power limiting control system based on integral feedback control.

FIG. 9 shows an alternate embodiment of the present invention that employs a power limiting control system based on a measure of receive power and the closed loop power control setting to estimate output power.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The process of the present invention provides power control correction for a mobile radiotelephone as well as maintaining acceptable in and out of band maximum emission levels. This is accomplished by real-time compensation utilizing a set of correction tables that are generated during the production testing of each radiotelephone.

FIG. 2 shows a block diagram of a CDMA radiotelephone with the preferred embodiment power control correction implementation. FIGS. 3, 4, and 5 detail specific blocks of FIG. 2. The radiotelephone is comprised of a receive linearization section, transmit linearization section, power amplifier bias control section, and power limiting control section.

The receive linearization section includes an automatic gain control (AGC) section. The signal input to the AGC section is received on the forward link and amplified by a low noise amplifier (LNA) (211). The output of the LNA (211) is input to a variable gain amplifier (212). The variable gain amplifier (212) produces a signal that is converted to a digital signal using an analog to digital converter (ADC) (213).

The power of the digitized received signal is next computed by a digital power detector (214). The power detector (214) includes an integrator that integrates the detected power with respect to a reference voltage. In the preferred embodiment, this reference voltage is provided by the radio's demodulator to indicate the nominal value at which the demodulator requires the loop to lock in order to hold the power level constant. The demodulator requires this value for optimum performance since a power level too far out of the optimum range will degrade the performance of the demodulator. The power detector (214) performs the integration, thus generating an AGC setpoint. The setpoint and a receive frequency index are input to a receiver linearizing table (216).

The AGC setpoint and the frequency index are used to address the linearizer (216), thus accessing the proper calibration value. This calibration value is then output to a digital to analog converter (215) that generates the analog representation of the receive AGC setting.

The analog value adjusts the biasing of the variable gain amplifier (212). The control of the variable gain amplifier (212) forces the receive AGC loop to close such that the input to the receiver linearizing table (216) follows a predetermined straight line with respect to RF input power. This linearization removes the undesired linear and non-linear errors in addition to variations versus frequency that would otherwise be apparent at the input to the receiver linearizing table (216) in the receiver. These errors and variations would contribute to errors in the transmitter.

In order to reduce the error in the receive and transmit chains versus frequency, the receive and transmit linearizers utilize the frequency index that specifies the current center frequency on which the receive and transmit chains are operating. During factory calibration of the radiotelephone, the linearizers are loaded with values, in addition to the previously mentioned calibration values, that are indexed by frequency to correct the errors related to operating center frequency.

The AGC setpoint is the open loop power control signal for the radio. In the preferred embodiment, this is the power control performed by the radio by itself

without control input from the cells. As the power of the signal received from the cell increases, the radio decreases its transmit power. This output power control is accomplished by the AGC setpoint that is filtered by a low pass filter (217).

The transmit section includes a digital summer (210) that combines the AGC setpoint and a closed loop power control setting (206). The output of the summer (210) is fed into a power control limiting section (205). The operation of the power control limiting section (205) and the closed loop power control section (206), illustrated in FIGS. 3 and 4 respectively, will be discussed subsequently in greater detail.

The output of the power control limiting section (205), along with the transmit frequency index, are used to address values stored in a transmitter linearizing table (204). The transmitter linearizing table (204) contains values determined from production testing of the radiotelephone. The selected value is input to a digital to analog converter (203) whose output, an analog representation of the digital value input, controls a variable gain amplifier (202).

The biasing of the variable gain amplifier (202) is adjusted by the analog calibration value to a point such that the input to the transmitter linearizing table (204) follows a predetermined straight line with respect to transmitted RF output power. This linearization removes the undesired linear and non-linear errors along with variations versus frequency in the transmitter. This, combined with the previously mentioned receive linearization, greatly reduces the open and closed loop power control errors due to RF performance imperfections.

The power amplifier (PA) bias control section (218) controls the bias point of the transmit PA (201) based on the transmit gain setting such that the transmit sidebands for the given gain setting are optimized versus PA (201) current consumption. This allows a battery powered telephone to maximize talk time by reducing PA (201) current consumption at lower output powers while still maintaining acceptable sideband levels at higher output power levels.

The power control limiting section (205) is illustrated in FIG. 3. The power control limiting section (205) controls the closed loop power control and transmit gain settings when the output of the transmit gain summer (210) corresponds to a transmit output power level which is equal to or greater than the intended maximum output power. The maximum gain setting is determined by the PA limit threshold control section (209).

The threshold control section (209) determines the maximum gain setting based on a nominal value that is modified by a real-time measurement of the transmitted output power. The measurement is accomplished by an analog power detector (207) whose output transformed into a digital signal by an analog to digital converter (208). The digitized power value is then input to the threshold control section (209).

The threshold control section, detailed in FIG. 5, operates by the high power detector (HDET) linearizer (501) scaling the input digitized power value in order to match the numerology of the digital transmit gain control section. The scaled output from the linearizer (501) is subtracted (502) from the nominal maximum gain setting. This maximum gain setting can be hard coded into the radio during assembly or input during manufacturing and testing of the radio.

The difference of the maximum gain setting and the scaled output power is then added, by the adder (503), to the maximum gain setting. The sum of these signals is then used as the corrected maximum gain setting. This real-time modification of the detected power helps mitigate the errors introduced by temperature variations and aging of the transmitter PAs. In other words, if the difference between the maximum gain setting and the real-time measured power value is 0, then no correction is necessary. If there is a difference between the two, the difference is used to correct the maximum gain setting.

Referring to FIG. 3, a digital comparator (301) detects when the output of the transmit gain summer (210) equals or exceeds the maximum gain setting. The comparator (301) controls a 2:1 multiplexer (302) that outputs the maximum allowable setting when the output of the summer (210) exceeds the maximum allowable setting. When the output of the summer (210) is less than the maximum allowable setting, the multiplexer (302) outputs the direct output of the summer (210). This prohibits the transmitter from exceeding its maximum operating point.

The closed loop power control section (206), illustrated in FIG. 4, accumulates the power control commands sent on the forward link by the controlling radio-telephone cell site and outputs a gain adjust signal. The power control commands are collected in an accumulator (401). The operation of the accumulator (401) is controlled by the power control limiting section (205) when the transmit power amplifier (201) is outputting the maximum allowable power.

When the output of the summer (210) changes from being less than to equal or greater than the maximum allowable setting, the output of the closed loop power control accumulator (401) is latched into a flip-flop (402). While the output of the summer (210) is equal to or greater than the maximum allowable setting, as determined by the comparator (403) and NAND gate (404) circuit, an AND gate (405) masks off any closed loop power control up commands that would force the accumulator (401) above the flip-flop's (402) latched value. This prevents the accumulator from saturating during power limiting yet allows the closed loop power control setting to change anywhere below the latched value.

An alternate embodiment of the process of the present invention is illustrated in FIG. 6. In this embodiment, a power limiting control system is employed based on accumulator feedback control. The system operates by first measuring the output power of the power amplifier (609) using a power detector (610). The detected power is then digitized by an ADC (611) and compared to a maximum allowable setting by the comparator (601). If the output power is greater than the maximum setting, the power limiting accumulator (602) begins turning power down by reducing the gain of the variable gain amplifier (608). If the output power is less than the maximum setting the power limiting accumulator (602) returns to a 0 dB correction value.

In this embodiment, a closed loop power control limiting function (604 and 605), similar to the preferred embodiment, is employed. However, the trigger for the closed loop power control limiting function is a comparator (603) that detects when the power limiting accumulator (602) is limiting the output power by comparing the accumulator (602) output to 0 dB with the comparator (603). The linearizing compensation tables,

similar to the tables in the preferred embodiment, are added into the transmit gain control using a summer (606).

In another alternate embodiment, illustrated in FIG. 7, a power limiting control system is employed that is based on the closed loop power control accumulator (702). The system operates by first measuring the output power of the power amplifier (705) using a power detector (706). The detected power is digitized (707) and compared to a maximum allowable setting by the comparator (701). If the output power is greater than the maximum setting, the closed loop power control accumulator (702) is modified to turn the amplifier (704) power down by one step each 1.25 ms until the output power is less than the maximum setting. If the output power is less than the maximum setting, the closed loop power control accumulator is not modified. The linearizing compensation tables, similar to the preferred embodiment, are added into the transmit gain control using a summer (703).

In yet another embodiment, illustrated in FIG. 8, a power limiting control system is employed that is based on integral feedback control. The system operates by first measuring the output power of the power amplifier (808) using a power detector (809). The detected power is digitized (810) and input to an integrator (801) that follows the equation:

$$\frac{1}{K} \cdot \int (\text{Setpoint} - \text{Detected}) dt.$$

The integrator (801), generating a gain control signal, saturates at 0 dB and -63 dB of correction. The gain control signal is thus limited within a range. If the output power is greater than the setpoint, the integrator turns down the output power of the amplifier (807) at a rate based on the integration constant K until the setpoint is reached. The integrator is allowed to turn power down by as much as 63 dB. If the output power is less than the setpoint, the output of the integrator (801) will be forced to zero, thus not adjusting output power.

In this embodiment, a closed loop power control limiting function (803 and 804), similar to the preferred embodiment, is employed. The trigger for the closed loop power control limiting function, however, is a comparator (802) that detects when the power limiting integrator (801) is limiting the output power. The linearizing compensation tables, similar to the preferred embodiment, are added into the transmit gain control using a summer (805).

In still another embodiment, illustrated in FIG. 9, a power limiting control system is employed that is based only on a measure of receive power, as determined by the Rx power lookup table (902), and the closed loop power control setting as opposed to actual output power. The transmit power limiting and closed loop power control limiting function (901) can be implemented with either the preferred embodiment using the saturating accumulator (903) or one of the alternate embodiments. However, only the receive power and closed loop power control setting are used to estimate transmit output power.

In summary, the process of the present invention ensures that the transmitted sidebands and synthesizer phase noise of a radio transmitter remains within a predetermined specification by limiting the maximum output power. This power limitation is accomplished by a

control loop including a calibration look-up table. Therefore, a radiotelephone using the process of the present invention would not exceed its nominal maximum power level due to the cell issuing too many power turn-up commands. The radiotelephone limits the power output even when the cell erroneously decides the radiotelephone power should be increased.

We claim:

1. A method for correcting transmit power of a radio device having a plurality of predetermined calibration values and a reference voltage signal, the radio device transmitting and receiving on a plurality of frequencies, each frequency having a frequency index, the method comprising the steps of:

receiving a first signal having a first gain, a first frequency of the plurality of frequencies, and the first frequency having a first frequency index;
determining a receive power value of the first signal;
generating an automatic gain control setpoint in response to the receive power value and the reference voltage signal;
selecting a first predetermined calibration value in response to the automatic gain control setpoint and the first frequency index;
adjusting the first gain in response to the first calibration value;
transmitting a second signal having a second gain and a second frequency of the plurality of frequencies, the second frequency having a second frequency index;
determining a transmit power value of the second signal;
generating a second calibration value in response to the automatic gain control setpoint, the second frequency index, and the transmit power value; and
adjusting the second gain in response to the second calibration value.

2. The method of claim 1 and further including the steps of digitizing the receive power value before generating the automatic gain control setpoint and converting the first predetermined calibration value to an analog value before adjusting the first gain.

3. A radio performing transmit power calibration, the radio transmitting and receiving signals having a plurality of frequencies, each frequency having a frequency index, the radio transmitting signals through a variable gain, transmit amplifier having a control input and receiving signals through a variable gain, receive amplifier having a control input, the radio comprising:

a power detector, coupled to the receive amplifier, for generating a first power value from a received signal having a first frequency;
an integrator, coupled to the power detector, for generating an automatic gain control setpoint from the first power value;
a receive linearizer, coupled to the integrator and the receive amplifier, for generating a receive calibration value in response to the automatic gain control setpoint and a first frequency index corresponding

to the first frequency, the receive calibration value being coupled to the receive amplifier control input for adjusting the gain of the receive amplifier;
a second power detector, coupled to the transmit amplifier, for generating a second power value from a transmitted signal having a second frequency; and
a transmit linearizer for generating a transmit calibration value in response to the automatic gain control setpoint, the second power value, and a frequency index corresponding to the second frequency, the transmit calibration value being coupled to the control input of the transmit amplifier for adjusting the gain of the transmit amplifier.

4. A radio performing transmit power calibration, the radio transmitting and receiving signals having a plurality of frequencies, each frequency having a frequency index, the radio transmitting a signal, having a first frequency, through a variable gain transmit amplifier having a control input and receiving a signal, having a second frequency, through a variable gain receive amplifier having a control input, the radio comprising:

a first analog to digital converter, coupled to the receive amplifier, for generating a digital signal from the received signal;
a power detector, coupled to the first analog to digital converter, for generating a power value from the digital signal;
an integrator, coupled to the power detector, for generating an automatic gain control setpoint from the power value;
a receive linearizer, coupled to the integrator, for generating a receive calibration value in response to the automatic gain control set point and a first frequency index corresponding to the second frequency;
a first digital to analog converter, coupled to the receive linearizer, for generating an analog, receive calibration value from the receive calibration value, the analog calibration value coupled to the receive amplifier control input for varying the gain of the receive amplifier;
a second power detector, coupled to the transmit amplifier, for generating an analog power value from the transmitted signal;
a second analog to digital converter, coupled to the second power detector, for generating a digital power value from the analog power value;
a transmit linearizer, coupled to the integrator, for generating a transmit calibration value in response to the automatic gain control setpoint, the digital power value, and a second frequency index corresponding to the first frequency; and
a second digital to analog converter, coupled to the second control input, for generating an analog, transmit calibration value from the transmit calibration value, the analog, transmit calibration value adjusting the gain of the transmit amplifier.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 5,452,473
DATED : September 19, 1995
INVENTOR(S) : Weiland et al.

Page 1 of 1

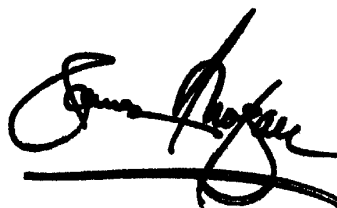
It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Title page.

Item [75], Inventor, please remove "**John E. Maloney**" as an inventor.

Signed and Sealed this

Eleventh Day of November, 2003

A handwritten signature in black ink, appearing to read "James E. Rogan", with a long horizontal flourish extending from the bottom of the signature.

JAMES E. ROGAN
Director of the United States Patent and Trademark Office



US005452473C1

(12) **EX PARTE REEXAMINATION CERTIFICATE** (6913th)
United States Patent
Weiland et al.

(10) **Number:** **US 5,452,473 C1**(45) **Certificate Issued:** **Jul. 7, 2009**

(54) **REVERSE LINK, TRANSMIT POWER CORRECTION AND LIMITATION IN A RADIOTELEPHONE SYSTEM**

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(73) Assignee: **Qualcomm Incorporated**, San Diego, CA (US)

Dec. 12, 2007 Final Initial and Recommended Decision.

Reexamination Request:

No. 90/008,720, Jun. 20, 2007

United States Court of Appeals for the Federal Circuit; 2008-1318 Qualcomm Incorporated (Appellant) v. International Trade Commission (Appellee) v. Nokia Corporation and Nokia Inc. (Inventors); Appeal from the United States International Trade Commission in Investigation No. 337-TA-578, Order on Motion; Oct. 15, 2008; 2 pages.

Reexamination Certificate for:

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Appl. No.: **08/203,151**
Filed: **Feb. 28, 1994**

Primary Examiner—Charles Craver

Certificate of Correction issued Nov. 11, 2003.

(51) **Int. Cl.**
H04B 7/005 (2006.01)

(52) **U.S. Cl.** **455/88; 455/126; 455/127.2; 455/234.2; 455/522; 330/129**

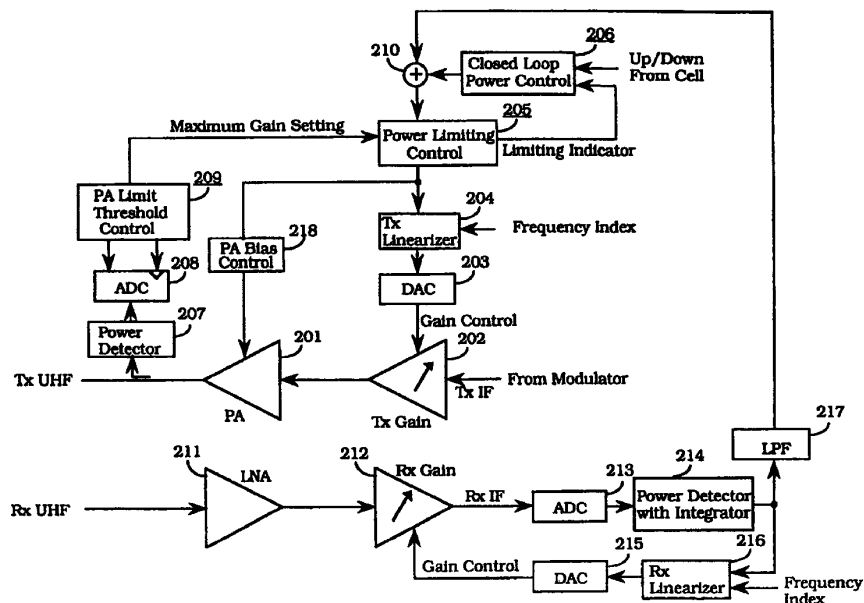
(58) **Field of Classification Search** None
See application file for complete search history.

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(57) ABSTRACT

The process and apparatus of the present invention limits the output power of the radiotelephone, operating in a cellular system in the preferred embodiment. This ensures the transmitted sidebands and synthesizer phase noise remains within a certain specification. This is accomplished by power detection and a correction accumulator that together generate a gain control signal by limiting the gain adjustment to a maximum value, even when the cell site communicating with the radio-telephone is sending power turn-up commands to the radiotelephone. This process includes dynamically correcting the output level of the transmitter due to gain variations in the transmitter stages or gain control elements.



1
EX PARTE
REEXAMINATION CERTIFICATE
ISSUED UNDER 35 U.S.C. 307

THE PATENT IS HEREBY AMENDED AS
INDICATED BELOW.

Matter enclosed in heavy brackets [] appeared in the patent, but has been deleted and is no longer a part of the patent; matter printed in italics indicates additions made to the patent.

AS A RESULT OF REEXAMINATION, IT HAS BEEN DETERMINED THAT:

Claims 1, 3 and 4 are determined to be patentable as amended.

Claim 2 dependent on an amended claim, is determined to be patentable.

1. A method for correcting transmit power of a radio device having a plurality of predetermined calibration values and a reference voltage signal, the radio device transmitting and receiving on a plurality of frequencies, each frequency having a frequency index, the method comprising the steps of:

receiving a first signal having a first gain, a first frequency of the plurality of frequencies, and the first frequency having a first frequency index;

determining a receive power value of the first signal; generating an automatic gain control setpoint response to the receive power value and the reference voltage signal;

selecting a first predetermined calibration value in response to the automatic gain control setpoint and the first frequency index;

adjusting the first gain in response to the first calibration value;

transmitting a second signal having a second gain and a second frequency of the plurality of frequencies, the second frequency having a second frequency index;

determining a transmit power value of the second signal;

generating a second calibration value in response to the automatic gain control setpoint, the second frequency index, and the transmit power value; and

adjusting the second gain in response to the second calibration value;

wherein generating the second calibration value comprises the steps of:

determining a gain adjust signal in response to a power control command transmitted from a base station;

combining the automatic gain control setpoint and the gain adjust signal to produce a summation signal;

determining a maximum gain setting;

comparing the summation signal to the maximum gain setting;

if the summation signal is greater than or equal to the maximum gain setting, adjusting the second calibration value in response to the maximum gain setting, the second frequency index, and the transmit power value; and

if the summation signal is less than the maximum gain setting, adjusting the second calibration value in response to the summation signal, the second frequency index, and the transmit power value.

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3. A radio performing transmit power calibration, the radio transmitting and receiving signals having a plurality of frequencies, each frequency having a frequency index, the radio transmitting signals through a variable gain, transmit amplifier having a control input and receiving signals through a variable gain, receive amplifier having a control input, the radio comprising:

a power detector, coupled to the receive amplifier, for generating a first power value from

a received signal having a first frequency;

an integrator, coupled to the power detector, for generating an automatic gain control setpoint from the first power value;

a receive linearizer, coupled to the integrator and the receive amplifier, for generating a receive calibration value in response to the automatic gain control setpoint and a first frequency index corresponding to the first frequency, the receive calibration value being coupled to the receive amplifier control input for adjusting the gain of the receive amplifier;

a second power detector, coupled to the transmit amplifier, for generating a second power value from a transmitted signal having a second frequency;

a threshold control circuit for determining a maximum gain setting;

a power control command circuit for determining a gain adjust signal in response to a power control command transmitted to the radio from a base station;

a summer for combining the automatic gain control setpoint and the gain adjust signal to produce a summation signal;

a power limiting control circuit, coupled to the summer, for comparing the summation signal to the maximum gain setting;

a transmit linearizer for generating a transmit calibration value in response to the automatic gain control setpoint, the second power value, and a frequency index corresponding to the second frequency, the transmit calibration value being coupled to the control input of the transmit amplifier for adjusting the gain of the transmit amplifier;

wherein generating the transmit calibration value comprises:

if the summation signal is greater than or equal to the maximum gain setting, adjusting the transmit calibration value in response to the maximum gain setting, the frequency index corresponding to the second frequency, and the second power value; and

if the summation signal is less than the maximum gain setting, adjusting the transmit calibration value in response to the summation signal, the frequency index corresponding to the second frequency, and the second power value.

4. A radio performing transmit power calibration, the radio transmitting and receiving signals having a plurality of frequencies, each frequency having a frequency index, the radio transmitting a signal, having a first frequency, through a variable gain transmit amplifier having a control input and receiving a signal, having a second frequency, through a variable gain receive amplifier having a control input, the radio comprising:

a first analog to digital converter, coupled to the receive amplifier, for generating a digital signal from the received signal;

a power detector, coupled to the first analog to digital converter, for generating a power value from the digital signal;

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an integrator, coupled to the power detector, for generating an automatic gain control setpoint from the power value;

a receive linearizer, coupled to the integrator, for generating a receive calibration value in response to the automatic gain control set point and a first frequency index corresponding to the second frequency;

a first digital to analog converter, coupled to the receive linearizer, for generating an analog, receive calibration value from the receive calibration value, the analog calibration value coupled to the receive amplifier control input for varying the gain of the receive amplifier;

a second power detector, coupled to the transmit amplifier, for generating an analog power value from the transmitted signal;

a second analog to digital converter, coupled to the second power detector, for generating a digital power value from the analog power value;

a threshold control circuit for determining a maximum gain setting;

a power control command circuit for determining a gain adjust signal in response to a power control command transmitted to the radio from a base station;

a summer for combining the automatic gain control setpoint and the gain adjust signal to produce a summation signal;

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a power limiting control circuit, coupled to the summer, for comparing the summation signal to the maximum gain setting;

a transmit linearizer, coupled to the integrator, for generating a transmit calibration value in response to the automatic gain control setpoint, the digital power value, and a second frequency index corresponding to the first frequency;

a second digital to analog converter, coupled to the second control input, for generating an analog, transmit calibration value from the transmit calibration value, the analog, transmit calibration value adjusting the gain of the transmit amplifier;

wherein generating the transmit calibration value comprises:

if the summation signal is greater than or equal to the maximum gain setting, adjusting the transmit calibration value in response to the maximum gain setting, the second frequency index, and the digital power value; and

if the summation signal is less than the maximum gain setting, adjusting the transmit calibration value in response to the summation signal, the second frequency index, and the digital power value.

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