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	UTILITY			Attorney Dock	et No.	14970-	-94702	
	PATENT APPLICAT	ΓΙΟΝ		First Named In	ventor	WEI-Y	U CHEN	
	TRANSMITTA	L		Title		IMAGE CAPTURI TERMINAL	ING LENS SYSTEM, IMAGING DEVICE AND MOBILE	
(Only)	for new nonprovisional applications unde	er 37 CFR 1.53(b))		Express Mail L	abel No.			
See MPE	APPLICATION ELEME P chapter 600 concerning utility patent a	<del>-</del>	ts.	ADDRESS	5 TO:		mmissioner for Patents P.O. Box 1450 xandria, VA 22313-1450	
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See 3 3. <b>Appl</b>	licant asserts small entity status. 7 CFR 1.27 licant certifies micro entity status. S					pers document(s)) e of Assignee		
4. Spec	cant must attach form PTO/SB/15A or B  iffication [Total Po  the claims and abstract must start on a n  MPEP § 608.01(a) for information on the	ages 56 ew page.	] ement)	(when	there is an	,	Power of Attorney	
6. <b>Inventor</b> (including	ving(s) (35 U.S.C. 113) [Total Shifts of Declaration [Total Phisubstitute statements under 37 CFR 1.64 an oath or declaration under 37 CFR 1.63	ages 1 and assignments		12. English Translation Document (if applicable)  13. Information Disclosure Statement (PTO/SB/08 or PTO-1449)				
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8. <b>C</b> D-R	ROM or CD-R iplicate, large table, or Computer Program	m ( <i>Appendix</i> )		16. Certified Copy of Priority Document(s) (if foreign priority is claimed)  17. Nonpublication Request Under 35 U.S.C. 122(b)(2)(B)(i). Applicant must attach form PTO/SB/35 or equivalent.  18. Other:				
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Name (Print/Type)	Tim Tingkang Xia				_	ration No. ney/Agent)	45,242	

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constitutes the claim for priority as required by 35 U.S.C. 119(b) and 37 CFR 1.55(d). When priority is claimed to a foreign application that is eligible for retrieval under the priority document exchange program (PDX) the information will be used by the Office to automatically attempt retrieval pursuant to 37 CFR 1.55(h)(1) and (2). Under the PDX program, applicant bears the ultimate responsibility for ensuring that a copy of the foreign application is received by the Office from the participating foreign intellectual property office, or a certified copy of the foreign priority application is filed, within the time period specified in 37 CFR 1.55(g)(1).

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102139029	TW	2013-10-29							
Additional Foreign Priority	Additional Foreign Priority Data may be generated within this form by selecting the								

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Application Da	nta Sheet 37 CFR 1.76	Attorney Docket Number	14970-94702	
Application Da	ita Sileet 37 Cl K 1.70	Application Number		
Title of Invention IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL				

# Statement under 37 CFR 1.55 or 1.78 for AIA (First Inventor to File) Transition Applications

This application (1) claims priority to or the benefit of an application filed before March 16, 2013 and (2) also
contains, or contained at any time, a claim to a claimed invention that has an effective filing date on or after March
16, 2013.
NOTE: By providing this statement under 37 CFR 1.55 or 1.78, this application, with a filing date on or after March
16, 2013, will be examined under the first inventor to file provisions of the AIA.

### **Authorization to Permit Access:**

X Authorization to Permit Access to the Instant Application by the Participating Offices

If checked, the undersigned hereby grants the USPTO authority to provide the European Patent Office (EPO), the Japan Patent Office (JPO), the Korean Intellectual Property Office (KIPO), the World Intellectual Property Office (WIPO), and any other intellectual property offices in which a foreign application claiming priority to the instant patent application is filed access to the instant patent application. See 37 CFR 1.14(c) and (h). This box should not be checked if the applicant does not wish the EPO, JPO, KIPO, WIPO, or other intellectual property office in which a foreign application claiming priority to the instant patent application is filed to have access to the instant patent application.

In accordance with 37 CFR 1.14(h)(3), access will be provided to a copy of the instant patent application with respect to: 1) the instant patent application-as-filed; 2) any foreign application to which the instant patent application claims priority under 35 U.S.C. 119(a)-(d) if a copy of the foreign application that satisfies the certified copy requirement of 37 CFR 1.55 has been filed in the instant patent application; and 3) any U.S. application-as-filed from which benefit is sought in the instant patent application.

In accordance with 37 CFR 1.14(c), access may be provided to information concerning the date of filing this Authorization.

# **Applicant Information:**

Providing assignment information in this section does not substitute for compliance with any requirement of part 3 of Title 37 of CFR to have an assignment recorded by the Office.

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<ul><li>Assignee</li></ul>		◯ Legal R	epresentative un	der 35 U.S.C. 1	117	O Joint Inventor
Person to whom th	e inventor is oblig	ated to assign.		O Person	who shows	sufficient proprietary interest
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Application	n Dete	- Char	4 27 CED 4 76	Attorney Doo	ket Number	14970-9	94702	
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- A record from this system of records may be disclosed, as a routine use, in the course of presenting evidence to a court, magistrate, or administrative tribunal, including disclosures to opposing counsel in the course of settlement negotiations.
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- 7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
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# IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

#### **RELATED APPLICATIONS**

This application claims priority to Taiwan Application Serial Number 102139029, filed October 29, 2013, which is incorporated by reference herein in its entirety.

#### **BACKGROUND**

#### 10 Technical Field

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The present disclosure relates to an image capturing lens system. More particularly, the present disclosure relates to a compact image capturing lens system applicable to a mobile terminal.

#### 15 Description of Related Art

In recent years, with the popularity of mobile terminals having camera functionalities, the demand of miniaturized optical systems has been increasing. As the advanced semiconductor manufacturing technologies have allowed the pixel size of sensors to be reduced and compact optical systems have gradually evolved toward the field of higher megapixels, there is an increasing demand for compact optical systems featuring better image quality.

A conventional compact optical system in a portable electronic product typically utilizes a three-element lens structure. Due to the popularity of mobile products with high-end specifications, such as smart phones, tablet personal computers, wearable apparatus and other high-end mobile terminals, the

requirements for high resolution and image quality of present compact optical systems increase significantly. However, the conventional optical systems cannot satisfy these requirements of the compact optical systems.

Another conventional compact optical system provides a four-element lens structure. However, it is hard to make a good balance between obtaining a large field of view and a short total track length. Furthermore, it is also not favorable for the resolving power and illumination in a peripheral region of an image; therefore, it cannot satisfy the requirements of the compact optical systems featuring better image quality.

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#### SUMMARY

According to one aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power. When an axial distance between an object-side surface of the first lens element and the

image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the second lens element is f2, and a focal length of the third lens element is f3, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm; 1.0 mm < Td/tan(HFOV) < 3.75 mm; |f/f4| < 1.20; and

f2/f3 < -0.65.

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According to another aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power. When an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, and a focal length of the third lens element is f3, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

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-2.0 < f/f3 < -0.95.

According to still another aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power. When an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, and an f-number of the image capturing lens system is Fno, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

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 $1.40 < Fno \le 2.25$ .

According to yet another aspect of the present disclosure, an imaging device includes the image capturing lens system according to the aforementioned aspect and an image sensor, wherein the image sensor is located on an image plane of the image capturing lens system.

According to still yet another aspect of the present disclosure, a mobile terminal includes the imaging device according to the aforementioned aspect.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The disclosure can be more fully understood by reading the following detailed description of the embodiments, with reference made to the accompanying drawings as follows:

Fig. 1A is a schematic view of an imaging device according to the 1st embodiment of the present disclosure;

Fig. 1B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 1st embodiment;

Fig. 2A is a schematic view of an imaging device according to the 2nd embodiment of the present disclosure;

Fig. 2B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 2nd embodiment;

- Fig. 3A is a schematic view of an imaging device according to the 3rd embodiment of the present disclosure;
- Fig. 3B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 3rd embodiment;
- Fig. 4A is a schematic view of an imaging device according to the 4th embodiment of the present disclosure;

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- Fig. 4B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 4th embodiment;
- Fig. 5A is a schematic view of an imaging device according to the 5th embodiment of the present disclosure;
  - Fig. 5B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 5th embodiment;
  - Fig. 6A is a schematic view of an imaging device according to the 6th embodiment of the present disclosure;
  - Fig. 6B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 6th embodiment;
  - Fig. 7A is a schematic view of an imaging device according to the 7th embodiment of the present disclosure;
  - Fig. 7B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 7th embodiment;
    - Fig. 8A is a schematic view of an imaging device according to the 8th embodiment of the present disclosure;
    - Fig. 8B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 8th embodiment;

Fig. 9A is a schematic view of an imaging device according to the 9th embodiment of the present disclosure;

Fig. 9B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 9th embodiment;

Fig. 10A is a schematic view of an imaging device according to the 10th embodiment of the present disclosure;

Fig. 10B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 10th embodiment;

Fig. 11A shows a smart phone with an imaging device of the present disclosure installed therein;

Fig. 11B shows a tablet personal computer with an imaging device of the present disclosure installed therein; and

Fig. 11C shows a wearable device with an imaging device of the present disclosure installed therein.

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#### **DETAILED DESCRIPTION**

An image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The image capturing lens system has a total of four lens elements with refractive power.

The first lens element can have positive refractive power, so that it provides the image capturing lens system with the positive refractive power as it needs to be so as to reduce the total track length of the image capturing lens system. The first lens element can have a convex object-side surface in a

paraxial region thereof, so that it is favorable for further reducing the total track length.

The second lens element has positive refractive power, so that it is favorable for the second lens element adjusting the light gathering ability of the first lens element. The second lens element has a convex image-side surface in a paraxial region thereof, so that it is favorable for correcting the astigmatism of the image capturing lens system.

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The third lens element has negative refractive power, so that it is favorable for correcting the aberration of the image capturing lens system. The third lens element has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof, so that it is favorable for correcting the astigmatism of the image capturing lens system.

The fourth lens element can have a convex object-side surface in a paraxial region thereof and has a concave image-side surface in a paraxial region thereof. Furthermore, the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. Therefore, it is favorable for correcting the astigmatism and aberration of the off-axis.

When an axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied: 0.5 mm < Td < 3.2 mm. Therefore, it is favorable for keeping the image capturing lens system compact. Preferably, the following condition is satisfied: 0.8 mm < Td < 2.5 mm.

When the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and half of a maximal field of view of the image capturing lens system is HFOV, the

following condition is satisfied: 1.0 mm < Td/tan(HFOV) < 3.75 mm. Therefore, it is favorable for obtaining a large field of view and short total track length for the image capturing lens system. Preferably, the following condition is satisfied: 1.2 mm < Td/tan(HFOV) < 2.75 mm.

When a focal length of the image capturing lens system is f, and a focal length of the fourth lens element is f4, the following condition is satisfied: |f/f4| < 1.20. Therefore, it is favorable for the principal point of the image capturing lens system being positioned away from the image plane so as to reduce the total track length and keep the image capturing lens system compact.

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When a focal length of the second lens element is f2, and a focal length of the third lens element is f3, the following condition is satisfied: f2/f3 < -0.65. Therefore, it is favorable for balancing the refractive powers of the second lens element and the third lens element so as to correct the aberration and reduce the photosensitivity. Preferably, the following condition is satisfied: f2/f3 < -0.75.

When the focal length of the image capturing lens system is f, and the focal length of the third lens element is f3, the following condition is satisfied: -2.0 < f/f3 < -0.95. Therefore, the third lens element serves as a correcting lens for balancing and correcting the aberrations of the image capturing lens system so as to obtain better image quality.

When an f-number of the image capturing lens system is Fno, and the following condition is satisfied:  $1.40 < \text{Fno} \le 2.25$ . Therefore, it is favorable for improving the illumination in a peripheral region of the image capturing lens system.

When the focal length of the image capturing lens system is f, and a focal length of the first lens element is f1, the following condition is satisfied: -0.25 < f/f1 < 0.75. Therefore, the first lens element will have a more proper refractive power so as to avoid excess photosensitivity. Preferably, the following condition is satisfied: 0.25 < f/f1 < 0.75.

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When a curvature radius of the object-side surface of the second lens element is R3, and a curvature radius of the image-side surface of the second lens element is R4, the following condition is satisfied: 0.5 < (R3+R4)/(R3-R4) < 2.5. Therefore, it is favorable for further correcting the aberration of the image capturing lens system.

When the focal length of the image capturing lens system is f, and the following condition is satisfied: 0.5 mm < f < 2.0 mm. Therefore, it is favorable for providing a proper total track length.

When a sum of the central thicknesses of the first lens element, the second lens element, the third lens element, and the fourth lens element is  $\Sigma$ CT, and the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, the following condition is satisfied: 0.80 <  $\Sigma$ CT/Td < 0.95. Therefore, it is favorable for assembling the lens elements of the image capturing lens system so as to reduce the photosensitivity.

When an Abbe number of the first lens element is V1, and the following condition is satisfied: 45 < V1. Therefore, it is favorable for correcting the chromatic aberration of the image capturing lens system.

When a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens

element is CT3, and a central thickness of the fourth lens element is CT4, the following condition is satisfied: 0.65 < CT2/(CT1+CT3+CT4) < 2.0. Therefore, the thickness of each lens element is favorable for manufacturing and assembling the lens elements.

When a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied: 80 degrees < FOV < 110 degrees. Therefore, it is favorable for obtaining enough field of view.

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According to the image capturing lens system of the present disclosure, the lens elements thereof can be made of glass or plastic material. When the lens elements are made of glass material, the distribution of the refractive power of the image capturing lens system may be more flexible to design. When the lens elements are made of plastic material, the manufacturing cost can be effectively reduced. Furthermore, surfaces of each lens element can be arranged to be aspheric, since the aspheric surface of the lens element is easy to form a shape other than spherical surface so as to have more controllable variables for eliminating the aberration thereof, and to further decrease the required number of the lens elements. Therefore, the total track length of the image capturing lens system can also be reduced.

According to the image capturing lens system of the present disclosure, each of an object-side surface in a paraxial region thereof and an image-side surface has a paraxial region and an off-axis region. The paraxial region refers to the region of the surface where light rays travel close to the optical axis, and the off-axis region refers to the region of the surface where light rays travel away from the optical axis. Particularly, when the lens element has a convex surface, it indicates that the surface is convex in the paraxial region thereof;

when the lens element has a concave surface, it indicates that the surface is concave in the paraxial region thereof.

According to the image capturing lens system of the present disclosure, the image capturing lens system can include at least one stop, such as an aperture stop, a glare stop or a field stop. Said glare stop or said field stop is for eliminating the stray light and thereby improving the image resolution thereof.

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According to the image capturing lens system of the present disclosure, an aperture stop can be configured as a front stop or a middle stop. A front stop disposed between an imaged object and the first lens element can provide a longer distance between an exit pupil of the image capturing lens system and the image plane and thereby improves the image-sensing efficiency of an image sensor. A middle stop disposed between the first lens element and the image plane is favorable for enlarging the field of view of the image capturing lens system and thereby provides a wider field of view for the same.

The present image capturing lens system can be optionally applied to moving focus optical systems. According to the image capturing lens system of the present disclosure, the image capturing lens system is featured with good correction ability and high image quality, and can be applied to 3D (three-dimensional) image capturing applications, in products such as digital cameras, mobile devices, digital tablets, wearable devices and other mobile terminals.

According to the present disclosure, an imaging device is provided. The imaging device includes the image capturing lens system according to the aforementioned image capturing lens system of the present disclosure, and an

image sensor, wherein the image sensor is disposed on an image plane of the aforementioned image capturing lens system. As a result, it is favorable for reducing the total track length of the image capturing lens system while obtaining large field of view. Furthermore, it is also favorable for improving the resolving power and illumination so as to achieve the best image quality. Preferably, the imaging device can further include a barrel member, a holding member or a combination thereof.

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According to the present disclosure, a mobile terminal is provided, wherein the mobile terminal includes the aforementioned imaging device. The imaging device includes the image capturing lens system according to the aforementioned image capturing lens system of the present disclosure, and the image sensor, wherein the image sensor is disposed on an image plane of the aforementioned image capturing lens system. As a result, it is favorable for reducing the total track length of the image capturing lens system while obtaining large field of view. Furthermore, it is also favorable for improving the resolving power and illumination so as to achieve the best image quality.

In Fig. 11A, Fig. 11B and Fig. 11C, an imaging device 1101 may be installed in but not limited to a mobile terminal, including a smart phone 1110, a tablet personal computer 1120 or a wearable device 1130. The three exemplary figures of different kinds of mobile terminal are only exemplary for showing the imaging device of present disclosure installing in a mobile terminal and is not limited thereto. Preferably, the mobile terminal can further include but not limited to display, control unit, random access memory unit (RAM) a read only memory unit (ROM) or a combination thereof.

According to the above description of the present disclosure, the following 1st – 10th specific embodiments are provided for further explanation.

#### 1st Embodiment

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Fig. 1A is a schematic view of an imaging device according to the 1st embodiment of the present disclosure. Fig. 1B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 1st embodiment.

In Fig. 1A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 170. The image capturing lens system includes, in order from an object side to an image side, a first lens element 110, an aperture stop 100, a second lens element 120, a third lens element 130, a fourth lens element 140, an IR-cut filter 150 and an image plane 160, wherein the image capturing lens system has a total of four lens elements (110-140) with refractive power.

The first lens element 110 with positive refractive power has a convex object-side surface 111 in a paraxial region thereof and a concave image-side surface 112 in a paraxial region thereof, which are both aspheric, and the first lens element 110 is made of plastic material.

The second lens element 120 with positive refractive power has a convex object-side surface 121 in a paraxial region thereof and a convex image-side surface 122 in a paraxial region thereof, which are both aspheric, and the second lens element 120 is made of plastic material.

The third lens element 130 with negative refractive power has a concave object-side surface 131 in a paraxial region thereof and a convex image-side

surface 132 in a paraxial region thereof, which are both aspheric, and the third lens element 130 is made of plastic material.

The fourth lens element 140 with positive refractive power has a convex object-side surface 141 in a paraxial region thereof and a concave image-side surface 142 in a paraxial region thereof, which are both aspheric, and the fourth lens element 140 is made of plastic material. Furthermore, the image-side surface 142 of the fourth lens element 140 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 150 is made of glass and located between the fourth lens element 140 and the image plane 160, and will not affect the focal length of the image capturing lens system. The image sensor 170 is disposed on the image plane 160 of the image capturing lens system.

The equation of the aspheric surface profiles of the aforementioned lens elements of the 1st embodiment is expressed as follows:

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$$X(Y) = (Y^2/R)/(1 + sqrt(1 - (1+k) \times (Y/R)^2)) + \sum_{i} (Ai) \times (Y^i)$$

, where,

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X is the relative distance between a point on the aspheric surface spaced at a distance Y from the optical axis and the tangential plane at the aspheric surface vertex on the optical axis;

Y is the vertical distance from the point on the aspheric surface to the optical axis;

R is the curvature radius;

k is the conic coefficient; and

25 Ai is the i-th aspheric coefficient.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a focal length of the image capturing lens system is f, an f-number of the image capturing lens system is Fno, and half of a maximal field of view of the image capturing lens system is HFOV, these parameters have the following values: f = 1.17 mm; Fno = 2.20; and HFOV = 46.7 degrees.

In the image capturing lens system of the imaging device according to the 1st embodiment, when an Abbe number of the first lens element 110 is V1, the following condition is satisfied: V1 = 21.4.

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In the image capturing lens system according to the 1st embodiment, when a central thickness of the second lens element 120 is CT2, a central thickness of the first lens element 110 is CT1, a central thickness of the third lens element 130 is CT3, and a central thickness of the fourth lens element 140 is CT4, the following condition is satisfied: CT2/(CT1+CT3+CT4) = 0.69.

In the image capturing lens system according to the 1st embodiment, when a curvature radius of the object-side surface 121 of the second lens element 120 is R3, and a curvature radius of the image-side surface 122 of the second lens element 120 is R4, the following condition is satisfied: (R3+R4)/(R3-R4) = 0.85.

In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and a focal length of the first lens element 110 is f1, the following condition is satisfied: f/f1 = 0.12.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a focal length of the second lens element 120 is f2, and a focal length of the third lens element 130 is f3, the following condition is satisfied: f2/f3 = -0.77.

In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and a focal length of the fourth lens element 140 is f4, the following condition is satisfied: |f/f4| = 0.77.

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In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and the focal length of the third lens element 130 is f3, the following condition is satisfied: f/f3 = -1.10.

In the image capturing lens system according to the 1st embodiment, when an axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is Td, the following condition is satisfied: Td = 1.850 mm.

In the image capturing lens system according to the 1st embodiment, when a sum of the central thicknesses of the first lens element 110, the second lens element 120, the third lens element 130, and the fourth lens element 140 is  $\Sigma$ CT, and the axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is Td, the following condition is satisfied:  $\Sigma$ CT/Td = 0.89.

In the image capturing lens system according to the 1st embodiment, when the axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is Td, and half of the maximal field of view of the image capturing lens system is HFOV, the following condition is satisfied: Td/tan(HFOV) = 1.74 mm.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a maximal field of view of the image capturing lens system is FOV, the following condition is satisfied: FOV = 93.4 degrees.

The detailed optical data of the 1st embodiment are shown in Table 1

and the aspheric surface data are shown in Table 2 below.

TABLE 1											
	Embodiment 1										
f = 1.17 mm, Fno = 2.20, HFOV = 46.7 deg.											
Surface #		Curvatur	Curvature Radius		Material	Index	Abbe #	Focal Length			
0	Object	Pla	ıno	Infinity							
1	Lens 1	1.666	ASP	0.256	Plastic	1.650	21.4	9.56			
2		2.139	ASP	0.031							
3	Ape. Stop	Pla	ino	0.019							
4	Lens 2	5.712	ASP	0.671	Plastic	1.544	55.9	0.82			
5		-0.464	ASP	0.130							
6	Lens 3	-0.228	ASP	0.230	Plastic	1.634	23.8	-1.06			
7		-0.480	ASP	0.030							
8	Lens 4	0.679	ASP	0.483	Plastic	1.535	55.7	1.52			
9		3.062	ASP	0.300							
10	IR-cut filter	Pla	ino	0.145	Glass	1.517	64.2	-			
11		Pla	Plano								
12	Image	Pla	Plano								
Note: Refere	ence wavelen	gth is 587	.6 nm (d-li	ne).							

TABLE 2										
Aspheric Coefficients										
Surface #	1	5								
k =	1.2237E+00	1.7244E+01	9.0000E+01	-6.9311E-01						
A4 =	3.1416E-01	1.1703E+00	-4.1498E-01	-6.9345E-01						
A6 =	-1.0010E+00	-2.0080E+01	3.6416E+00	1.3202E+00						
A8 =	4.5872E+01	5.2569E+02	4.3035E+01	1.0955E+01						
A10 =	-5.9339E+02	-3.0044E+03	-7.4996E+03	-3.8285E+02						
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0040E+03						
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04						
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04						
Surface #	6	7	8	9						

k =	-9.8477E-01	-3.2669E+00	-6.1619E-01	-1.4636E+01
A4 =	3.5682E+00	-1.8915E+00	-1.2870E+00	1.2883E+00
A6 =	-3.7958E+00	8.7075E+00	3.1244E+00	-3.7603E+00
A8 =	-1.1135E+02	-3.6761E+01	-9.1933E+00	5.9040E+00
A10 =	1.5862E+03	1.7257E+02	1.7146E+01	-5.8521E+00
A12 =	-8.7685E+03	-4.8146E+02	-1.9850E+01	3.5356E+00
A14 =	2.3054E+04	6.7728E+02	1.2752E+01	-1.1759E+00
A16 =	-2.3557E+04	-3.6747E+02	-3.5165E+00	1.6169E-01

In Table 1, the curvature radius, the thickness and the focal length are shown in millimeters (mm). Surface numbers 0-12 represent the surfaces sequentially arranged from the object-side to the image-side along the optical axis. In Table 2, k represents the conic coefficient of the equation of the aspheric surface profiles. A1-A16 represent the aspheric coefficients ranging from the 1st order to the 16th order. The tables presented below for each embodiment are the corresponding schematic parameter and aberration curves, and the definitions of the tables are the same as Table 1 and Table 2 of the 1st embodiment. Therefore, an explanation in this regard will not be provided again.

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#### 2nd Embodiment

Fig. 2A is a schematic view of an imaging device according to the 2nd embodiment of the present disclosure. Fig. 2B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 2nd embodiment.

In Fig. 2A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 270. The image capturing lens system includes, in order from an object side to

an image side, a first lens element 210, an aperture stop 200, a second lens element 220, a third lens element 230, a fourth lens element 240, an IR-cut filter 250 and an image plane 260, wherein the image capturing lens system has a total of four lens elements (210-240) with refractive power.

The first lens element 210 with positive refractive power has a convex object-side surface 211 in a paraxial region thereof and a concave image-side surface 212 in a paraxial region thereof, which are both aspheric, and the first lens element 210 is made of plastic material.

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The second lens element 220 with positive refractive power has a convex object-side surface 221 in a paraxial region thereof and a convex image-side surface 222 in a paraxial region thereof, which are both aspheric, and the second lens element 220 is made of plastic material.

The third lens element 230 with negative refractive power has a concave object-side surface 231 in a paraxial region thereof and a convex image-side surface 232 in a paraxial region thereof, which are both aspheric, and the third lens element 230 is made of plastic material.

The fourth lens element 240 with positive refractive power has a convex object-side surface 241 in a paraxial region thereof and a concave image-side surface 242 in a paraxial region thereof, which are both aspheric, and the fourth lens element 240 is made of plastic material. Furthermore, the image-side surface 242 of the fourth lens element 240 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 250 is made of glass and located between the fourth lens element 240 and the image plane 260, and will not affect the focal length of the

image capturing lens system. The image sensor 270 is disposed on the image plane 260 of the image capturing lens system.

The detailed optical data of the 2nd embodiment are shown in Table 3 and the aspheric surface data are shown in Table 4 below.

TABLE 3										
	Embodiment 2									
f = 1.23 mm, Fno = 2.45, HFOV = 45.6 deg.										
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length		
0	Object	Pla	ano	Infinity						
1	Lens 1	1.728	ASP	0.217	Plastic	1.640	22.0	1207.16		
2		1.647	ASP	0.041						
3	Ape. Stop	Pla	no	0.020						
4	Lens 2	2.201	ASP	0.685	Plastic	1.544	55.9	0.78		
5		-0.465	ASP	0.138						
6	Lens 3	-0.213	ASP	0.222	Plastic	1.634	23.8	-0.90		
7		-0.479	ASP	0.030						
8	Lens 4	0.691	ASP	0.430	Plastic	1.535	55.7	1.40		
9		7.112	ASP	0.300						
10	IR-cut filter	Pla	no	0.300	Glass	1.517	64.2	-		
11		Pla	Plano							
12	Image	Pla	no	-						
Note: Refere	ence wavelen	gth is 587	.6 nm (d-l	ine).						

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		TABLE 4		
		Aspheric Coefficie	ents	
Surface #	1	2	4	5
k =	-7.8611E-01	2.2256E+01	4.4287E+01	-6.8249E-01
A4 =	2.7433E-01	3.5449E-01	-1.1581E+00	-5.9944E-01
A6 =	-1.5466E+00	-2.9377E+01	8.9406E-01	3.6061E-01
A8 =	4.7455E+01	6.4129E+02	4.1870E+01	1.6896E+01
A10 =	-6.0092E+02	-3.8207E+03	-7.3180E+03	-3.8194E+02
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0043E+03
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04
Surface #	6	7	8	9
k =	-1.0107E+00	-3.0532E+00	-7.4231E-01	2.2155E+01
A4 =	3.8803E+00	-1.7079E+00	-1.1152E+00	1.6267E+00
A6 =	-4.2860E+00	8.7245E+00	2.9613E+00	-4.5228E+00
A8 =	-1.1314E+02	-3.7291E+01	-9.2058E+00	6.4630E+00

A10 =	1.5859E+03	1.7181E+02	1.7048E+01	-5.8730E+00
A12 =	-8.7686E+03	-4.8143E+02	-1.9563E+01	3.4083E+00
A14 =	2.3054E+04	6.7878E+02	1.3110E+01	-1.1920E+00
A16 =	-2.3557E+04	-3.6776E+02	-4.1607E+00	1.9105E-01

In the 2nd embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 2nd embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 3 and Table 4 as the following values and satisfy the following conditions:

2nd Embodiment					
f [mm]	1.23	f2/f3	-0.87		
Fno	2.45	f/f4	0.88		
HFOV [deg.]	45.6	f/f3	-1.37		
V1	22.0	Td [mm]	1.783		
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.87		
(R3+R4)/(R3-R4)	0.65	Td/tan(HFOV) [mm]	1.75		
f/f1	0.00	FOV [deg.]	91.2		

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#### 3rd Embodiment

Fig. 3A is a schematic view of an imaging device according to the 3rd embodiment of the present disclosure. Fig. 3B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 3rd embodiment.

In Fig. 3A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

370. The image capturing lens system includes, in order from an object side to an image side, a first lens element 310, an aperture stop 300, a second lens element 320, a third lens element 330, a fourth lens element 340, an IR-cut filter 350 and an image plane 360, wherein the image capturing lens system has a total of four lens elements (310-340) with refractive power.

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The first lens element 310 with positive refractive power has a convex object-side surface 311 in a paraxial region thereof and a concave image-side surface 312 in a paraxial region thereof, which are both aspheric, and the first lens element 310 is made of plastic material.

The second lens element 320 with positive refractive power has a concave object-side surface 321 in a paraxial region thereof and a convex image-side surface 322 in a paraxial region thereof, which are both aspheric, and the second lens element 320 is made of plastic material.

The third lens element 330 with negative refractive power has a concave object-side surface 331 in a paraxial region thereof and a convex image-side surface 332 in a paraxial region thereof, which are both aspheric, and the third lens element 330 is made of plastic material.

The fourth lens element 340 with positive refractive power has a convex object-side surface 341 in a paraxial region thereof and a concave image-side surface 342 in a paraxial region thereof, which are both aspheric, and the fourth lens element 340 is made of plastic material. Furthermore, the image-side surface 342 of the fourth lens element 340 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 350 is made of glass and located between the fourth lens element 340 and the image plane 360, and will not affect the focal length of the

image capturing lens system. The image sensor 370 is disposed on the image plane 360 of the image capturing lens system.

The detailed optical data of the 3rd embodiment are shown in Table 5 and the aspheric surface data are shown in Table 6 below.

	TABLE 5								
	Embodiment 3								
		f = 1.66 r	nm, Fno =	2.15, HFO	V = 46.8 d	eg.			
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	1.333	ASP	0.286	Plastic	1.544	55.9	2.50	
2		59.851	ASP	0.005					
3	Ape. Stop	Pla	ino	0.195					
4	Lens 2	-1.920	ASP	0.409	Plastic	1.544	55.9	1.60	
5		-0.644	ASP	0.156					
6	Lens 3	-0.263	ASP	0.200	Plastic	1.650	21.4	-1.49	
7		-0.470	ASP	0.030					
8	Lens 4	0.677	ASP	0.363	Plastic	1.535	55.7	2.33	
9		1.206	ASP	0.400					
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-	
11		Pla	ino	0.431					
12	Image	Plano		-					
Note: Refere	ence wavelen	gth is 587	.6 nm (d-li	ne).					
The effective	The effective radius of Surface 1 is 0.510 mm.								

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		TABLE 6		
		Aspheric Coefficie	ents	
Surface #	1	2	4	5
k =	-2.4704E+00	9.0000E+01	5.8947E+00	-3.7972E-01
A4 =	-3.4848E-02	-3.8775E-01	-9.3075E-01	-3.3741E-01
A6 =	-4.4471E-01	-2.8417E+00	3.6516E+00	9.2277E-01
A8 =	-4.9925E-01	1.8185E+01	-4.0769E+01	-3.9461E+00
A10 =	-1.2166E+01	-2.0954E+01	-4.4351E+00	-1.9037E+01
A12 =	3.9114E+01	-1.4998E+03	1.2130E+03	4.9148E+01
A14 =	-1.7950E+02	1.2389E+04	-4.4615E+03	1.0076E+02
A16 =	3.3572E+02	-2.9058E+04	6.2425E+03	8.0489E+01
Surface #	6	7	8	9
k =	-1.1491E+00	-2.3808E+00	-1.7649E+00	-1.0689E+01
A4 =	4.2079E+00	2.1562E-01	-6.9591E-01	9.1971E-01
A6 =	-2.8310E+01	-4.4239E+00	1.2041E+00	-3.0958E+00

A8 =	1.2287E+02	1.8790E+01	-2.9023E+00	4.8713E+00
A10 =	-3.9035E+02	-4.1840E+01	4.4195E+00	-4.6279E+00
A12 =	8.5064E+02	5.5883E+01	-3.7857E+00	2.6418E+00
A14 =	-9.7331E+02	-4.0255E+01	1.6532E+00	-8.3581E-01
A16 =	4.7213E+02	1.4428E+01	-2.8192E-01	1.1204E-01

In the 3rd embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 3rd embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 5 and Table 6 as the following values and satisfy the following conditions:

3rd Embodiment					
f [mm]	1.66	f2/f3	-1.07		
Fno	2.15	f/f4	0.71		
HFOV [deg.]	46.8	f/f3	-1.11		
V1	55.9	Td [mm]	1.644		
CT2/(CT1+CT3+CT4)	0.48	ΣCT/Td	0.77		
(R3+R4)/(R3-R4)	2.01	Td/tan(HFOV) [mm]	1.54		
f/f1	0.66	FOV [deg.]	93.6		

## 4th Embodiment

Fig. 4A is a schematic view of an imaging device according to the 4th embodiment of the present disclosure. Fig. 4B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 4th embodiment.

In Fig. 4A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

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470. The image capturing lens system includes, in order from an object side to an image side, a first lens element 410, an aperture stop 400, a second lens element 420, a third lens element 430, a fourth lens element 440, an IR-cut filter 450 and an image plane 460, wherein the image capturing lens system has a total of four lens elements (410-440) with refractive power.

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The first lens element 410 with negative refractive power has a convex object-side surface 411 in a paraxial region thereof and a concave image-side surface 412 in a paraxial region thereof, which are both aspheric, and the first lens element 410 is made of plastic material.

The second lens element 420 with positive refractive power has a convex object-side surface 421 in a paraxial region thereof and a convex image-side surface 422 in a paraxial region thereof, which are both aspheric, and the second lens element 420 is made of plastic material.

The third lens element 430 with negative refractive power has a concave object-side surface 431 in a paraxial region thereof and a convex image-side surface 432 in a paraxial region thereof, which are both aspheric, and the third lens element 430 is made of plastic material.

The fourth lens element 440 with positive refractive power has a convex object-side surface 441 in a paraxial region thereof and a concave image-side surface 442 in a paraxial region thereof, which are both aspheric, and the fourth lens element 440 is made of plastic material. Furthermore, the image-side surface 442 of the fourth lens element 440 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 450 is made of glass and located between the fourth lens element 440 and the image plane 460, and will not affect the focal length of the

image capturing lens system. The image sensor 470 is disposed on the image plane 460 of the image capturing lens system.

The detailed optical data of the 4th embodiment are shown in Table 7 and the aspheric surface data are shown in Table 8 below.

	TABLE 7								
	Embodiment 4								
		f = 1.15 r	nm, Fno =	2.22, HFO	V = 48.5 d	eg.			
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	no	Infinity					
1	Lens 1	1.999	ASP	0.200	Plastic	1.544	55.9	-46.83	
2		1.789	ASP	0.021					
3	Ape. Stop	Pla	ino	0.037					
4	Lens 2	1.606	ASP	0.471	Plastic	1.544	55.9	0.81	
5		-0.543	ASP	0.184					
6	Lens 3	-0.207	ASP	0.209	Plastic	1.634	23.8	-1.22	
7		-0.393	ASP	0.030					
8	Lens 4	0.747	ASP	0.319	Plastic	1.535	55.7	1.62	
9		4.607	ASP	0.300					
10	IR-cut filter	Pla	ino	0.300	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	ino	-					
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

		TABLE 8		
		Aspheric Coefficie	ents	
Surface #	1	2	4	5
k =	-2.2996E+01	3.4247E+01	9.8701E+00	-4.2975E-01
A4 =	-2.1353E-01	-2.0670E+00	-2.2221E+00	-6.3795E-01
A6 =	-3.6880E+00	-3.6063E+01	-8.7081E+00	-6.5092E+00
A8 =	5.2789E+01	6.9201E+02	1.4888E+02	4.6114E+01
A10 =	-6.4083E+02	-4.8238E+03	-8.2602E+03	-4.7532E+02
A12 =	4.0983E+03	-1.6432E+05	1.3290E+05	3.0044E+03
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0679E+04
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3828E+04
Surface #	6	7	8	9
k =	-1.0439E+00	-2.0056E+00	-6.4024E-01	-3.3636E+00
A4 =	4.2327E+00	-9.7476E-01	-8.3147E-01	1.0958E+00
A6 =	-3.4551E+00	1.0236E+01	2.1761E+00	-1.7086E+00
A8 =	-1.0303E+02	-3.7610E+01	-4.8336E+00	1.3575E+00

A10 =	1.5970E+03	1.6620E+02	5.0397E+00	-2.6285E+00
A12 =	-8.9315E+03	-4.9093E+02	-4.1411E+00	4.3863E+00
A14 =	2.3054E+04	6.8046E+02	3.4069E+00	-3.3963E+00
A16 =	-2.3558E+04	-3.4010E+02	-1.6576E+00	9.5967E-01

In the 4th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 4th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 7 and Table 8 as the following values and satisfy the following conditions:

	Attle Esseles	-12	
	4th Embo	alment	
f [mm]	1.15	f2/f3	-0.66
Fno	2.22	f/f4	0.71
HFOV [deg.]	48.5	f/f3	-0.94
V1	55.9	Td [mm]	1.471
CT2/(CT1+CT3+CT4)	0.65	ΣCT/Td	0.82
(R3+R4)/(R3-R4)	0.49	Td/tan(HFOV) [mm]	1.30
f/f1	-0.02	FOV [deg.]	97.0

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#### 5th Embodiment

Fig. 5A is a schematic view of an imaging device according to the 5th embodiment of the present disclosure. Fig. 5B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 5th embodiment.

In Fig. 5A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

570. The image capturing lens system includes, in order from an object side to an image side, a first lens element 510, an aperture stop 500, a second lens element 520, a third lens element 530, a fourth lens element 540, an IR-cut filter 550 and an image plane 560, wherein the image capturing lens system has a total of four lens elements (510-540) with refractive power.

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The first lens element 510 with negative refractive power has a convex object-side surface 511 in a paraxial region thereof and a concave image-side surface 512 in a paraxial region thereof, which are both aspheric, and the first lens element 510 is made of glass material.

The second lens element 520 with positive refractive power has a convex object-side surface 521 in a paraxial region thereof and a convex image-side surface 522 in a paraxial region thereof, which are both aspheric, and the second lens element 520 is made of glass material.

The third lens element 530 with negative refractive power has a concave object-side surface 531 in a paraxial region thereof and a convex image-side surface 532 in a paraxial region thereof, which are both aspheric, and the third lens element 530 is made of plastic material.

The fourth lens element 540 with positive refractive power has a convex object-side surface 541 in a paraxial region thereof and a concave image-side surface 542 in a paraxial region thereof, which are both aspheric, and the fourth lens element 540 is made of plastic material. Furthermore, the image-side surface 542 of the fourth lens element 540 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 550 is made of glass and located between the fourth lens element 540 and the image plane 560, and will not affect the focal length of the

image capturing lens system. The image sensor 570 is disposed on the image plane 560 of the image capturing lens system.

The detailed optical data of the 5th embodiment are shown in Table 9 and the aspheric surface data are shown in Table 10 below.

TABLE 9								
	Embodiment 5							
		f = 2.24 r	nm, Fno =	2.51, HFO	V = 44.2 d	 eq.		
Surface #			e Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Pla	ano	Infinity				
1	Lens 1	1.367	ASP	0.300	Glass	2.144	17.8	-13.68
2		1.110	ASP	0.144				
3	Ape. Stop	Pla	ano	-0.015				
4	Lens 2	3.909	ASP	1.483	Glass	1.525	70.3	1.60
5		-0.932	ASP	0.325				
6	Lens 3	-0.341	ASP	0.277	Plastic	1.639	23.5	-1.72
7		-0.651	ASP	0.030				
8	Lens 4	0.897	ASP	0.606	Plastic	1.565	57.0	2.00
9		3.302	ASP	0.800				
10	IR-cut filter	Pla	no	0.300	Glass	1.517	64.2	-
11		Pla	Plano					
12	Image	Plano		-				
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).							

TABLE 10								
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	1.1992E+00	1.9195E+00	2.1734E+01	-7.2786E-01				
A4 =	5.8324E-02	1.2422E-01	-9.9032E-02	-1.2252E-01				
A6 =	-1.4402E-01	-5.2189E-01	5.9983E+00	5.2990E-01				
A8 =	1.0028E+00	4.2713E+00	-1.1966E+02	-3.0301E+00				
A10 =	-4.0021E+00	1.8016E+01	1.4083E+03	7.9248E+00				
A12 =	8.9035E+00	-4.2193E+02	-9.4428E+03	-1.0795E+01				
A14 =	-9.8479E+00	2.2697E+03	3.3923E+04	6.3429E+00				
A16 =	3.0263E+00	-4.1004E+03	-5.0610E+04	-8.0066E-01				
Surface #	6	7	8	9				
k =	-9.8774E-01	-3.1767E+00	-8.3817E-01	-2.4331E+01				
A4 =	2.5606E+00	-1.2881E-01	-4.2259E-01	3.5717E-01				
A6 =	-7.9740E+00	-6.6170E-01	4.3675E-01	-4.5759E-01				
A8 =	1.4853E+01	1.1888E+00	-4.6275E-01	2.9937E-01				

A10 =	-1.1480E+01	-4.2607E-01	3.1380E-01	-1.1921E-01
A12 =	-4.4740E+00	-5.1720E-01	-1.2912E-01	2.8364E-02
A14 =	1.2594E+01	5.0722E-01	2.9275E-02	-3.7104E-03
A16 =	-5.4160E+00	-1.2485E-01	-2.8533E-03	2.0238E-04

In the 5th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 5th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 9 and Table 10 as the following values and satisfy the following conditions:

5th Embodiment						
f [mm]	2.24	f2/f3	-0.93			
Fno	2.51	f/f4	1.12			
HFOV [deg.]	44.2	f/f3	-1.30			
V1	17.8	Td [mm]	3.150			
CT2/(CT1+CT3+CT4)	1.25	ΣCT/Td	0.85			
(R3+R4)/(R3-R4)	0.61	Td/tan(HFOV) [mm]	3.24			
f/f1	-0.16	FOV [deg.]	88.4			

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# 6th Embodiment

Fig. 6A is a schematic view of an imaging device according to the 6th embodiment of the present disclosure. Fig. 6B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 6th embodiment.

In Fig. 6A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

670. The image capturing lens system includes, in order from an object side to an image side, a first lens element 610, an aperture stop 600, a second lens element 620, a third lens element 630, a fourth lens element 640, an IR-cut filter 650 and an image plane 660, wherein the image capturing lens system has a total of four lens elements (610-640) with refractive power.

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The first lens element 610 with positive refractive power has a convex object-side surface 611 in a paraxial region thereof and a convex image-side surface 612 in a paraxial region thereof, which are both aspheric, and the first lens element 610 is made of plastic material.

The second lens element 620 with positive refractive power has a concave object-side surface 621 in a paraxial region thereof and a convex image-side surface 622 in a paraxial region thereof, which are both aspheric, and the second lens element 620 is made of plastic material.

The third lens element 630 with negative refractive power has a concave object-side surface 631 in a paraxial region thereof and a convex image-side surface 632 in a paraxial region thereof, which are both aspheric, and the third lens element 630 is made of plastic material.

The fourth lens element 640 with positive refractive power has a convex object-side surface 641 in a paraxial region thereof and a concave image-side surface 642 in a paraxial region thereof, which are both aspheric, and the fourth lens element 640 is made of plastic material. Furthermore, the image-side surface 642 of the fourth lens element 640 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 650 is made of glass and located between the fourth lens element 640 and the image plane 660, and will not affect the focal length of the

image capturing lens system. The image sensor 670 is disposed on the image plane 660 of the image capturing lens system.

The detailed optical data of the 6th embodiment are shown in Table 11 and the aspheric surface data are shown in Table 12 below.

TABLE 11									
	Embodiment 6								
	f = 1.27 mm, Fno = 2.10, HFOV = 44.4 deg.								
Surface #			Curvature Radius		Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	2.393	ASP	0.280	Plastic	1.544	55.9	3.85	
2		-16.057	ASP	0.017					
3	Ape. Stop	Pla	ino	0.044					
4	Lens 2	-30.373	ASP	0.755	Plastic	1.544	55.9	0.87	
5		-0.468	ASP	0.121					
6	Lens 3	-0.246	ASP	0.240	Plastic	1.639	23.5	-0.90	
7		-0.594	ASP	0.030					
8	Lens 4	0.639	ASP	0.522	Plastic	1.530	55.8	1.47	
9		2.521	ASP	0.400					
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	Plano						
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

		TABLE 12					
	T	Aspheric Coefficie	ents				
Surface #	1	2	4	5			
k =	1.7241E+00	-8.9754E+01	-9.0000E+01	-7.5923E-01			
A4 =	2.1410E-01	1.4516E+00	1.5168E-01	-5.4982E-01			
A6 =	-2.3810E-01	-1.0826E+01	4.8929E+00	2.0791E+00			
A8 =	2.3555E+01	1.9495E+02	-3.2116E+01	8.2787E-01			
A10 =	-2.5034E+02	-5.1780E+02	-2.6801E+03	-1.4893E+02			
A12 =	1.4357E+03	-5.7593E+04	4.6579E+04	1.0534E+03			
A14 =	-4.2381E+03	9.2351E+05	-3.3256E+05	-3.0936E+03			
A16 =	4.9589E+03	-4.2045E+06	9.0327E+05	3.3098E+03			
Surface #	6	7	8	9			
k =	-9.9704E-01	-3.7851E+00	-7.3474E-01	-2.0751E+00			
A4 =	2.9255E+00	-1.3600E+00	-1.2133E+00	1.8260E+00			
A6 =	-2.4852E+00	5.5927E+00	3.0817E+00	-5.9653E+00			
A8 =	-5.7718E+01	-1.8755E+01	-1.0034E+01	9.6816E+00			

A10 =	6.7135E+02	7.3016E+01	1.9498E+01	-9.2466E+00
A12 =	-3.0733E+03	-1.6937E+02	-2.1549E+01	5.1894E+00
A14 =	6.6780E+03	1.9522E+02	1.2590E+01	-1.5760E+00
A16 =	-5.6393E+03	-8.6932E+01	-3.0510E+00	1.9769E-01

In the 6th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 6th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 11 and Table 12 as the following values and satisfy the following conditions:

6th Embodiment						
f [mm]	1.27	f2/f3	-0.97			
Fno	2.10	f/f4	0.86			
HFOV [deg.]	44.4	f/f3	-1.41			
V1	55.9	Td [mm]	2.009			
CT2/(CT1+CT3+CT4)	0.72	ΣCT/Td	0.89			
(R3+R4)/(R3-R4)	1.03	Td/tan(HFOV) [mm]	2.05			
f/f1	0.33	FOV [deg.]	88.8			

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#### 7th Embodiment

Fig. 7A is a schematic view of an imaging device according to the 7th embodiment of the present disclosure. Fig. 7B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 7th embodiment.

In Fig. 7A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

770. The image capturing lens system includes, in order from an object side to an image side, an aperture stop 700, a first lens element 710, a second lens element 720, a third lens element 730, a fourth lens element 740, an IR-cut filter 750 and an image plane 760, wherein the image capturing lens system has a total of four lens elements (710-740) with refractive power.

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The first lens element 710 with positive refractive power has a convex object-side surface 711 in a paraxial region thereof and a concave image-side surface 712 in a paraxial region thereof, which are both aspheric, and the first lens element 710 is made of plastic material.

The second lens element 720 with positive refractive power has a concave object-side surface 721 in a paraxial region thereof and a convex image-side surface 722 in a paraxial region thereof, which are both aspheric, and the second lens element 720 is made of plastic material.

The third lens element 730 with negative refractive power has a concave object-side surface 731 in a paraxial region thereof and a convex image-side surface 732 in a paraxial region thereof, which are both aspheric, and the third lens element 730 is made of plastic material.

The fourth lens element 740 with positive refractive power has a convex object-side surface 741 in a paraxial region thereof and a concave image-side surface 742 in a paraxial region thereof, which are both aspheric, and the fourth lens element 740 is made of plastic material. Furthermore, the image-side surface 742 of the fourth lens element 740 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 750 is made of glass and located between the fourth lens element 740 and the image plane 760, and will not affect the focal length of

the image capturing lens system. The image sensor 770 is disposed on the image plane 760 of the image capturing lens system.

The detailed optical data of the 7th embodiment are shown in Table 13 and the aspheric surface data are shown in Table 14 below.

TABLE 13									
	Embodiment 7								
	f = 1.57 mm, Fno = 2.05, HFOV = 48.5 deg.								
Surface #			e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	no	Infinity					
1	Ape. Stop	Pla	no	-0.052					
2	Lens 1	1.142	ASP	0.279	Plastic	1.544	55.9	2.84	
3		4.008	ASP	0.159					
4	Lens 2	-4.075	ASP	0.614	Plastic	1.544	55.9	1.24	
5		-0.608	ASP	0.142					
6	Lens 3	-0.255	ASP	0.230	Plastic	1.634	23.8	-1.37	
7		-0.487	ASP	0.030					
8	Lens 4	0.636	ASP	0.414	Plastic	1.535	55.7	2.35	
9		0.998	ASP	0.500					
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	Plano						
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

TABLE 14								
	Aspheric Coefficients							
Surface #	2	3	4	5				
k =	-5.4318E-01	6.9324E+01	6.0179E+01	-4.8138E-01				
A4 =	1.1275E-01	-3.4138E-01	-6.6571E-01	-8.5384E-02				
A6 =	-1.4350E+00	-2.7321E+00	4.9846E-01	-6.6518E-01				
A8 =	6.0529E+00	2.0740E+01	-4.5807E+00	-2.1554E-01				
A10 =	4.7148E+01	-7.0776E+01	-1.7027E+02	-7.9977E+00				
A12 =	-1.4571E+02	-1.4998E+03	1.2130E+03	2.5638E+01				
A14 =	-3.8164E+03	1.2389E+04	-4.4615E+03	-4.3167E+01				
A16 =	1.5882E+04	-2.9058E+04	6.2425E+03	7.2938E+01				
Surface #	6	7	8	9				
k =	-1.1103E+00	-3.0258E+00	-9.3042E-01	-5.1455E+00				
A4 =	5.4423E+00	4.5345E-01	-7.7223E-01	7.0200E-01				
A6 =	-3.5666E+01	-4.9768E+00	9.4468E-01	-1.5850E+00				
A8 =	1.3446E+02	1.9752E+01	-1.3669E+00	1.7028E+00				

A10 =	-2.5131E+02	-4.2912E+01	1.1409E+00	-1.1082E+00
A12 =	-7.3665E+01	5.3544E+01	-5.2307E-01	4.3302E-01
A14 =	1.1117E+03	-3.5702E+01	1.2365E-01	-9.2838E-02
A16 =	-1.2600E+03	1.0063E+01	-1.1645E-02	8.3092E-03

In the 7th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 7th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 13 and Table 14 as the following values and satisfy the following conditions:

7th Embodiment						
f [mm]	1.57	f2/f3	-0.91			
Fno	2.05	f/f4	0.67			
HFOV [deg.]	48.5	f/f3	-1.15			
V1	55.9	Td [mm]	1.868			
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.82			
(R3+R4)/(R3-R4)	1.35	Td/tan(HFOV) [mm]	1.65			
f/f1	0.55	FOV [deg.]	97.0			

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# 8th Embodiment

Fig. 8A is a schematic view of an imaging device according to the 8th embodiment of the present disclosure. Fig. 8B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 8th embodiment.

In Fig. 8A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

870. The image capturing lens system includes, in order from an object side to an image side, a first lens element 810, an aperture stop 800, a second lens element 820, a third lens element 830, a fourth lens element 840, an IR-cut filter 850 and an image plane 860, wherein the image capturing lens system has a total of four lens elements (810-840) with refractive power.

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The first lens element 810 with positive refractive power has a convex object-side surface 811 in a paraxial region thereof and a concave image-side surface 812 in a paraxial region thereof, which are both aspheric, and the first lens element 810 is made of plastic material.

The second lens element 820 with positive refractive power has a concave object-side surface 821 in a paraxial region thereof and a convex image-side surface 822 in a paraxial region thereof, which are both aspheric, and the second lens element 820 is made of plastic material.

The third lens element 830 with negative refractive power has a concave object-side surface 831 in a paraxial region thereof and a convex image-side surface 832 in a paraxial region thereof, which are both aspheric, and the third lens element 830 is made of plastic material.

The fourth lens element 840 with positive refractive power has a convex object-side surface 841 in a paraxial region thereof and a concave image-side surface 842 in a paraxial region thereof, which are both aspheric, and the fourth lens element 840 is made of plastic material. Furthermore, the image-side surface 842 of the fourth lens element 840 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 850 is made of glass and located between the fourth lens element 840 and the image plane 860, and will not affect the focal length of

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the image capturing lens system. The image sensor 870 is disposed on the image plane 860 of the image capturing lens system.

The detailed optical data of the 8th embodiment are shown in Table 15 and the aspheric surface data are shown in Table 16 below.

TABLE 15									
	Embodiment 8								
f = 1.68 mm, Fno = 2.10, HFOV = 46.0 deg.									
Surface #			Curvature Radius		Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	1.787	ASP	0.278	Plastic	1.544	55.9	3.81	
2		12.133	ASP	0.022					
3	Ape. Stop	Pla	ino	0.145					
4	Lens 2	-3.839	ASP	0.668	Plastic	1.544	55.9	1.38	
5		-0.668	ASP	0.194					
6	Lens 3	-0.273	ASP	0.230	Plastic	1.639	23.5	-1.18	
7		-0.569	ASP	0.030					
8	Lens 4	0.784	ASP	0.496	Plastic	1.530	55.8	1.65	
9		5.992	ASP	0.400					
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	Plano						
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

TABLE 16								
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	-1.3232E+00	5.3151E+01	5.1693E+01	-5.9308E-01				
A4 =	1.6281E-02	-1.2122E-02	-2.5602E-01	-1.1508E-01				
A6 =	1.5823E-01	-1.1940E+00	-1.0332E+00	-6.8787E-01				
A8 =	5.9941E-01	1.2093E+01	1.0464E+01	-9.7964E-02				
A10 =	-1.3812E+01	-2.0003E+01	-1.9940E+02	-6.2734E+00				
A12 =	4.5317E+01	-1.4998E+03	1.2130E+03	2.8529E+01				
A14 =	-4.4460E+01	1.2389E+04	-4.4615E+03	-4.4589E+01				
A16 =	-4.7734E+01	-2.9058E+04	6.2425E+03	2.7908E+01				
Surface #	6	7	8	9				
k =	-1.0578E+00	-3.0032E+00	-8.6121E-01	5.6610E+00				
A4 =	4.0391E+00	9.4553E-02	-6.6716E-01	7.7788E-01				
A6 =	-2.6571E+01	-4.4170E+00	1.1395E+00	-1.2944E+00				
A8 =	1.2417E+02	1.9085E+01	-1.7698E+00	1.0967E+00				

A10 =	-3.9394E+02	-4.1568E+01	1.6239E+00	-5.7605E-01
A12 =	8.2748E+02	5.5376E+01	-8.6944E-01	1.8609E-01
A14 =	-9.7331E+02	-4.1902E+01	2.5418E-01	-3.3617E-02
A16 =	4.7213E+02	1.3653E+01	-3.1838E-02	2.5144E-03

In the 8th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 8th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 15 and Table 16 as the following values and satisfy the following conditions:

8th Embodiment						
f [mm]	1.68	f2/f3	-1.17			
Fno	2.10	f/f4	1.02			
HFOV [deg.]	46.0	f/f3	-1.42			
V1	55.9	Td [mm]	2.063			
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.81			
(R3+R4)/(R3-R4)	1.42	Td/tan(HFOV) [mm]	1.99			
f/f1	0.44	FOV [deg.]	92.0			

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## 9th Embodiment

Fig. 9A is a schematic view of an imaging device according to the 9th embodiment of the present disclosure. Fig. 9B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 9th embodiment.

In Fig. 9A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

970. The image capturing lens system includes, in order from an object side to an image side, a first lens element 910, an aperture stop 900, a second lens element 920, a third lens element 930, a fourth lens element 940, an IR-cut filter 950 and an image plane 960, wherein the image capturing lens system has a total of four lens elements (910-940) with refractive power.

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The first lens element 910 with positive refractive power has a convex object-side surface 911 in a paraxial region thereof and a convex image-side surface 912 in a paraxial region thereof, which are both aspheric, and the first lens element 910 is made of plastic material.

The second lens element 920 with positive refractive power has a convex object-side surface 921 in a paraxial region thereof and a convex image-side surface 922 in a paraxial region thereof, which are both aspheric, and the second lens element 920 is made of plastic material.

The third lens element 930 with negative refractive power has a concave object-side surface 931 in a paraxial region thereof and a convex image-side surface 932 in a paraxial region thereof, which are both aspheric, and the third lens element 930 is made of plastic material.

The fourth lens element 940 with positive refractive power has a convex object-side surface 941 in a paraxial region thereof and a concave image-side surface 942 in a paraxial region thereof, which are both aspheric, and the fourth lens element 940 is made of plastic material. Furthermore, the image-side surface 942 of the fourth lens element 940 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 950 is made of glass and located between the fourth lens element 940 and the image plane 960, and will not affect the focal length of

the image capturing lens system. The image sensor 970 is disposed on the image plane 960 of the image capturing lens system.

The detailed optical data of the 9th embodiment are shown in Table 17 and the aspheric surface data are shown in Table 18 below.

	TABLE 17								
	Embodiment 9								
f = 0.92 mm, Fno = 2.45, HFOV = 43.9 deg.									
Surface #		Curvature	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	no	Infinity					
1	Lens 1	100.000	ASP	0.205	Plastic	1.633	23.4	13.12	
2		-9.046	ASP	0.017					
3	Ape. Stop	Pla	Plano						
4	Lens 2	1.695	ASP	0.475	Plastic	1.544	55.9	0.54	
5		-0.319	ASP	0.100					
6	Lens 3	-0.148	ASP	0.160	Plastic	1.634	23.8	-0.65	
7		-0.329	ASP	0.030					
8	Lens 4	0.595	ASP	0.239	Plastic	1.530	55.8	1.28	
9		4.109	ASP	0.300					
10	IR-cut filter	Pla	no	0.145	Glass	1.517	64.2	-	
11		Plano		0.151					
12	Image	Plano		-					
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

TABLE 18							
	Aspheric Coefficients						
Surface #	1	2	4	5			
k =	-9.0000E+01	9.0000E+01	3.3243E+01	-6.6437E-01			
A4 =	2.5656E-01	2.4894E+00	-1.9077E+00	-1.5093E+00			
A6 =	-1.0613E+00	-9.5530E+01	-1.3506E+01	4.3096E+00			
A8 =	1.6769E+02	3.0126E+03	1.0928E+01	1.6065E+02			
A10 =	-3.7307E+03	-2.3016E+04	-4.4021E+04	-2.9203E+03			
A12 =	3.9786E+04	-1.5960E+06	1.2908E+06	2.9181E+04			
A14 =	-2.1485E+05	4.6819E+07	-1.6860E+07	-1.5683E+05			
A16 =	4.5990E+05	-3.8994E+08	8.3772E+07	3.0696E+05			
Surface #	6	7	8	9			
k =	-1.0921E+00	-2.4247E+00	-6.0015E-01	3.3921E+01			
A4 =	8.8579E+00	-1.7457E+00	-1.8642E+00	3.4965E+00			
A6 =	-9.7201E+00	2.7059E+01	4.2816E+00	-1.7965E+01			
A8 =	-4.6210E+02	-1.6609E+02	-3.6842E+01	3.3243E+01			

A10 =	1.0079E+04	1.0699E+03	9.4802E+01	-3.1178E+01
A12 =	-8.5169E+04	-4.7330E+03	-1.9140E+02	1.8452E+01
A14 =	3.3855E+05	1.0605E+04	3.6755E+02	-3.7397E+01
A16 =	-5.2300E+05	-7.7191E+03	-9.3365E+02	3.7762E+01

In the 9th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 9th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 17 and Table 18 as the following values and satisfy the following conditions:

9th Embodiment						
f [mm]	0.92	f2/f3	-0.83			
Fno	2.45	f/f4	0.72			
HFOV [deg.]	43.9	f/f3	-1.42			
V1	23.4	Td [mm]	1.250			
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.86			
(R3+R4)/(R3-R4)	0.68	Td/tan(HFOV) [mm]	1.30			
f/f1	0.07	FOV [deg.]	87.8			

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## 10th Embodiment

Fig. 10A is a schematic view of an imaging device according to the 10th embodiment of the present disclosure. Fig. 10B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 10th embodiment.

In Fig. 10A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

1070. The image capturing lens system includes, in order from an object side to an image side, an aperture stop 1000, a first lens element 1010, a second lens element 1020, a third lens element 1030, a fourth lens element 1040, an IR-cut filter 1050 and an image plane 1060, wherein the image capturing lens system has a total of four lens elements (1010-1040) with refractive power.

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The first lens element 1010 with positive refractive power has a convex object-side surface 1011 in a paraxial region thereof and a concave image-side surface 1012 in a paraxial region thereof, which are both aspheric, and the first lens element 1010 is made of plastic material.

The second lens element 1020 with positive refractive power has a concave object-side surface 1021 in a paraxial region thereof and a convex image-side surface 1022 in a paraxial region thereof, which are both aspheric, and the second lens element 1020 is made of plastic material.

The third lens element 1030 with negative refractive power has a concave object-side surface 1031 in a paraxial region thereof and a convex image-side surface 1032 in a paraxial region thereof, which are both aspheric, and the third lens element 1030 is made of plastic material.

The fourth lens element 1040 with positive refractive power has a convex object-side surface 1041 in a paraxial region thereof and a concave image-side surface 1042 in a paraxial region thereof, which are both aspheric, and the fourth lens element 1040 is made of plastic material. Furthermore, the image-side surface 1042 of the fourth lens element 1040 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 1050 is made of glass and located between the fourth lens element 1040 and the image plane 1060, and will not affect the focal length

of the image capturing lens system. The image sensor 1070 is disposed on the image plane 1060 of the image capturing lens system.

The detailed optical data of the 10th embodiment are shown in Table 19 and the aspheric surface data are shown in Table 20 below.

TARI F 10									
	TABLE 19								
Embodiment 10									
	f = 1.80 mm, Fno = 2.12, HFOV = 47.2 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ano	Infinity					
1	Ape. Stop	Pla	ano	-0.060					
2	Lens 1	1.246	ASP	0.289	Plastic	1.544	55.9	2.97	
3		5.018	ASP	0.191					
4	Lens 2	-3.749	ASP	0.593	Plastic	1.544	55.9	1.57	
5		-0.733	ASP	0.156					
6	Lens 3	-0.288	ASP	0.248	Plastic	1.634	23.8	-1.33	
7		-0.584	ASP	0.030					
8	Lens 4	0.704	ASP	0.601	Plastic	1.535	55.7	2.05	
9		1.382	ASP	0.500					
10	IR-cut filter	Pla	no	0.210	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	Plano						
Note: Refer	Note: Reference wavelength is 587.6 nm (d-line).								
The effective radius of Surface 9 is 1.676 mm.									

	TABLE 20						
		Aspheric Coefficie	ents				
Surface #	2	3	4	5			
k =	-5.0585E-01	9.0000E+01	3.6143E+01	-3.9805E-01			
A4 =	8.6099E-02	-2.2970E-01	-4.8540E-01	-1.5034E-01			
A6 =	-9.1382E-01	-1.8900E+00	2.7508E-01	-5.1276E-01			
A8 =	1.9706E+00	1.1233E+01	-2.0152E+00	-1.5742E-01			
A10 =	1.9492E+01	-3.0654E+01	-6.3534E+01	-3.0117E+00			
A12 =	-3.5519E+01	-4.4967E+02	3.6120E+02	7.3424E+00			
A14 =	-8.0910E+02	2.9681E+03	-1.0702E+03	-1.0241E+01			
A16 =	2.4600E+03	-5.5960E+03	1.2022E+03	1.7746E+01			
Surface #	6	7	8	9			
k =	-1.1070E+00	-2.9894E+00	-9.3316E-01	-5.2865E+00			
A3 =			-1.4739E-01	5.0831E-01			
A4 =	4.3809E+00	4.3352E-01	-3.5412E+00	2.6512E+00			

A5 =			2.4672E-02	1.3099E-01
A6 =	-2.6437E+01	-3.7903E+00	1.0303E+01	-3.1255E+01
A7 =			3.7082E-02	2.0652E-01
A8 =	9.1296E+01	1.0965E+01	-3.1616E+01	1.1148E+02
A9 =			-2.2687E-03	-9.0797E-01
A10 =	-1.5853E+02	-1.4675E+01	6.3626E+01	-2.2327E+02
A11 =			-2.3794E-03	3.6058E-01
A12 =	8.3141E+00	7.7310E+00	-7.5604E+01	2.6201E+02
A13 =			8.0966E-03	1.7201E-01
A14 =	3.8963E+02	1.2159E+00	4.7652E+01	-1.7041E+02
A15 =			-5.5857E-02	1.0396E-01
A16 =	-3.9976E+02	-1.8447E+00	-1.2153E+01	4.7523E+01

In the 10th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 10th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 19 and Table 20 as the following values and satisfy the following conditions:

10th Embodiment						
f [mm]	1.80	f2/f3	-1.18			
Fno	2.12	f/f4	0.88			
HFOV [deg.]	47.2	f/f3	-1.35			
V1	55.9	Td [mm]	2.108			
CT2/(CT1+CT3+CT4)	0.52	ΣCT/Td	0.82			
(R3+R4)/(R3-R4)	1.49	Td/tan(HFOV) [mm]	1.95			
f/f1	0.61	FOV [deg.]	94.4			

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The foregoing description, for purpose of explanation, has been described with reference to specific embodiments. It is to be noted that

TABLES 1-20 show different data of the different embodiments; however, the data of the different embodiments are obtained from experiments. The embodiments were chosen and described in order to best explain the principles of the disclosure and its practical applications, to thereby enable others skilled in the art to best utilize the disclosure and various embodiments with various modifications as are suited to the particular use contemplated. The embodiments depicted above and the appended drawings are exemplary and are not intended to be exhaustive or to limit the scope of the present disclosure to the precise forms disclosed. Many modifications and variations are possible in view of the above teachings.

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#### **CLAIMS**

## WHAT IS CLAIMED IS:

1. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and

a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the second lens element is f2, a focal length of the third lens element is f3, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

f2/f3 < -0.65.

- 2. The image capturing lens system of claim 1, wherein the fourth lens element has the object-side surface being convex in a paraxial region thereof.
- 3. The image capturing lens system of claim 2, wherein the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

$$-0.25 < f/f1 < 0.75$$
.

4. The image capturing lens system of claim 2, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:

$$0.8 \text{ mm} < Td < 2.5 \text{ mm}.$$

5. The image capturing lens system of claim 2, wherein an f-number of the image capturing lens system is Fno, and the following condition is satisfied:

$$1.40 < Fno \le 2.25$$
.

6. The image capturing lens system of claim 2, wherein a curvature radius of the object-side surface of the second lens element is R3, a curvature radius of the image-side surface of the second lens element is R4, and the following condition is satisfied:

$$0.5 < (R3+R4)/(R3-R4) < 2.5.$$

- 7. The image capturing lens system of claim 2, wherein the focal length of the image capturing lens system is f, and the following condition is satisfied:
  - 0.5 mm < f < 2.0 mm.
- 8. The image capturing lens system of claim 1, wherein the first lens element has a convex object-side surface in a paraxial region thereof.
- 9. The image capturing lens system of claim 8, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of the maximal field of view of the image capturing lens system is HFOV, and the following condition is satisfied:
  - 1.2 mm < Td/tan(HFOV) < 2.75 mm.
- 10. The image capturing lens system of claim 8, wherein a sum of the central thicknesses of the first lens element, the second lens element, the third lens element, and the fourth lens element is  $\Sigma$ CT, the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:
  - $0.80 < \Sigma CT/Td < 0.95$ .
- 11. The image capturing lens system of claim 8, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

12. The image capturing lens system of claim 8, wherein a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens element is CT3, a central thickness of the fourth lens element is CT4, and the following condition is satisfied:

0.65 < CT2/(CT1+CT3+CT4) < 2.0.

13. An imaging device, comprising:

the image capturing lens system of claim 1; and an image sensor.

14. A mobile terminal, comprising:

the imaging device of claim 13.

15. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and

a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the third lens element is f3, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

-2.0 < f/f3 < -0.95.

16. The image capturing lens system of claim 15, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

17. The image capturing lens system of claim 15, wherein the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

-0.25 < f/f1 < 0.75.

18. The image capturing lens system of claim 15, wherein a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied:

80 degrees < FOV < 110 degrees.

19. The image capturing lens system of claim 15, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:

0.8 mm < Td < 2.5 mm.

20. The image capturing lens system of claim 15, wherein a focal length of the second lens element is f2, the focal length of the third lens element is f3, and the following condition is satisfied:

f2/f3 < -0.75.

21. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and

a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, an f-number of the image capturing lens system is Fno, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

 $1.40 < Fno \le 2.25$ .

22. The image capturing lens system of claim 21, wherein a focal length of the second lens element is f2, a focal length of the third lens element is f3, and the following condition is satisfied:

f2/f3 < -0.65.

23. The image capturing lens system of claim 21, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

24. The image capturing lens system of claim 21, wherein the first lens element has positive refractive power, the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

0.25 < f/f1 < 0.75.

25. The image capturing lens system of claim 21, wherein a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied:

80 degrees < FOV < 110 degrees.

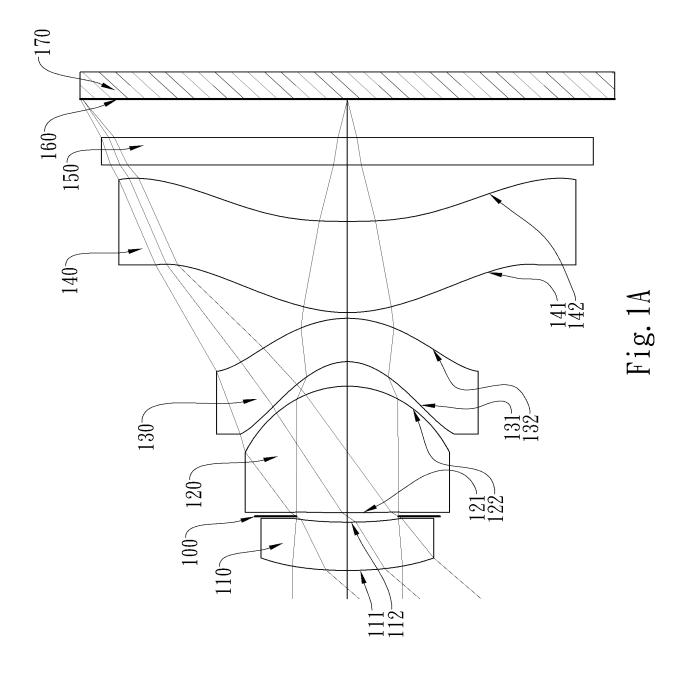
26. The image capturing lens system of claim 21, wherein a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens element is CT3, a central thickness of the fourth lens element is CT4, and the following condition is satisfied:

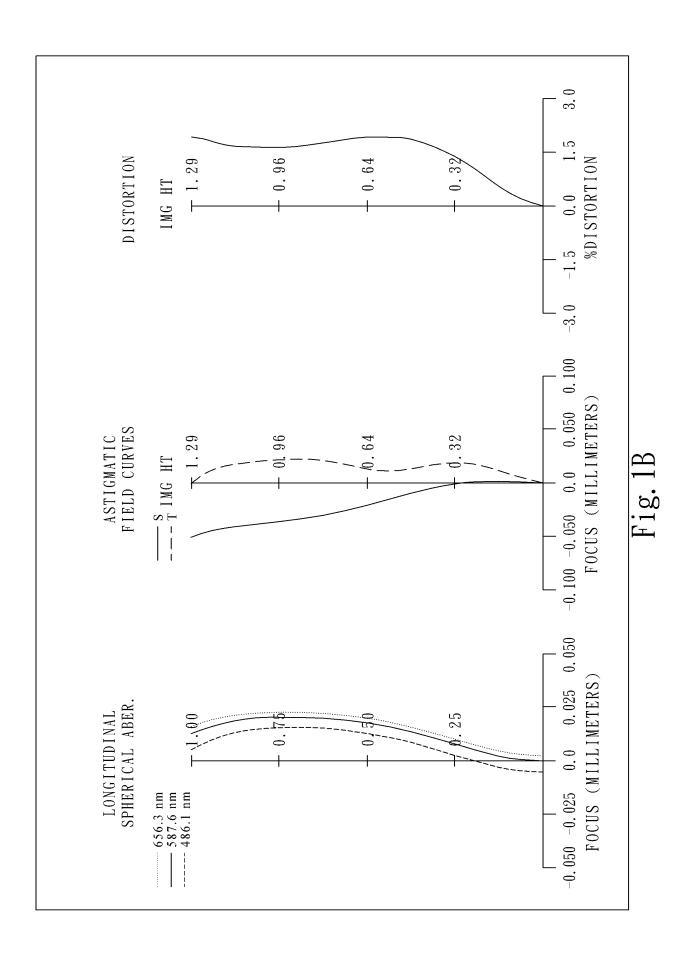
0.65 < CT2/(CT1+CT3+CT4) < 2.0.

## ABSTRACT OF THE DISCLOSURE

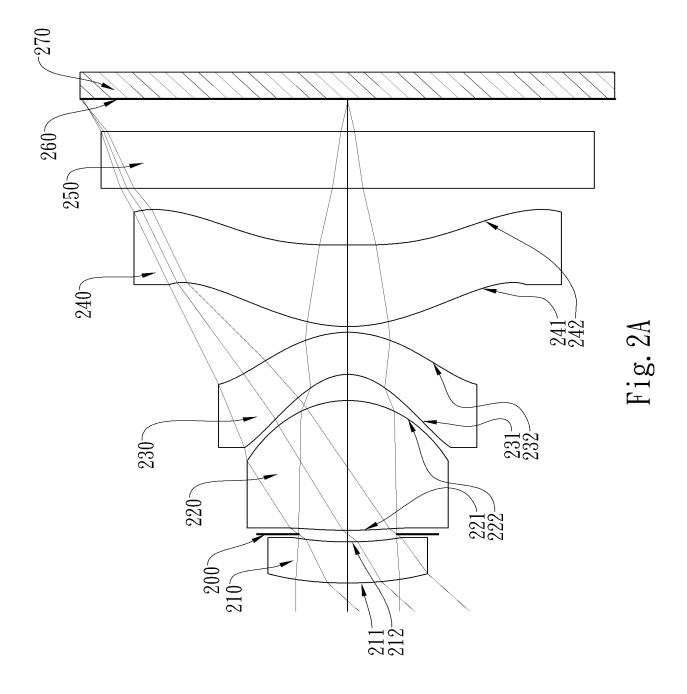
An image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface thereof are aspheric, and the image-side surface thereof has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power.

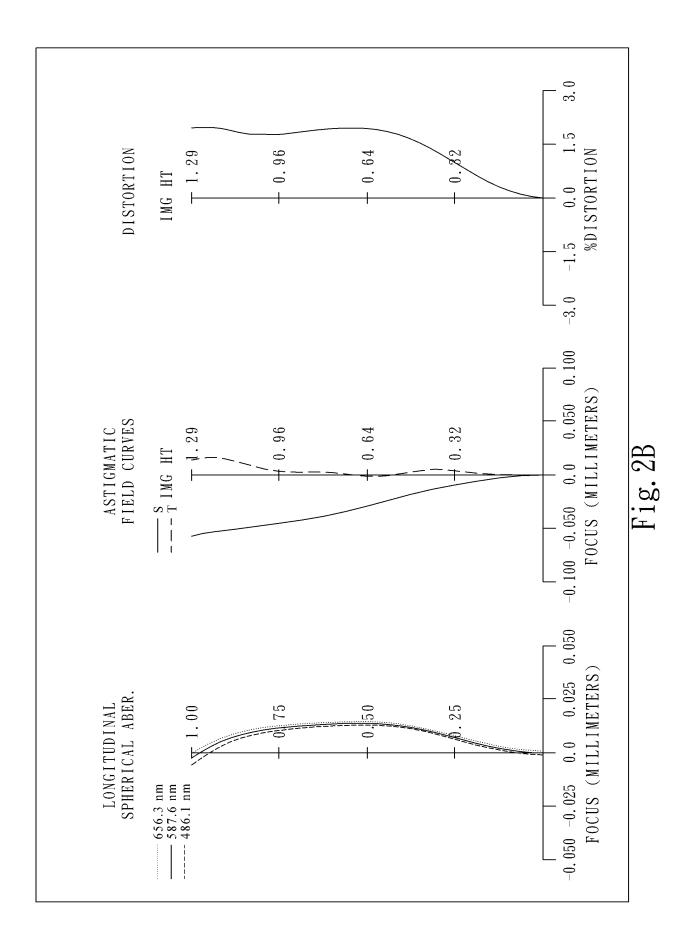
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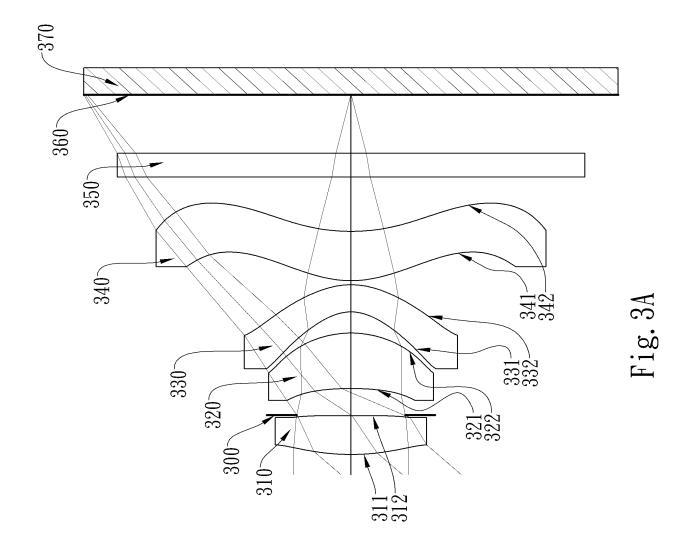


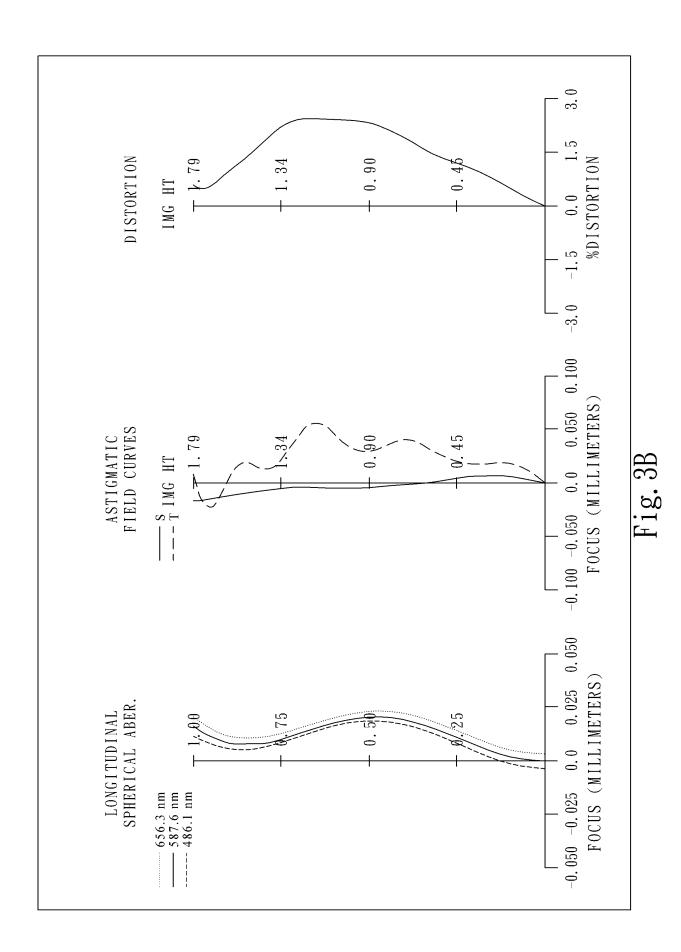
HP, Ex. 1002 Page 66



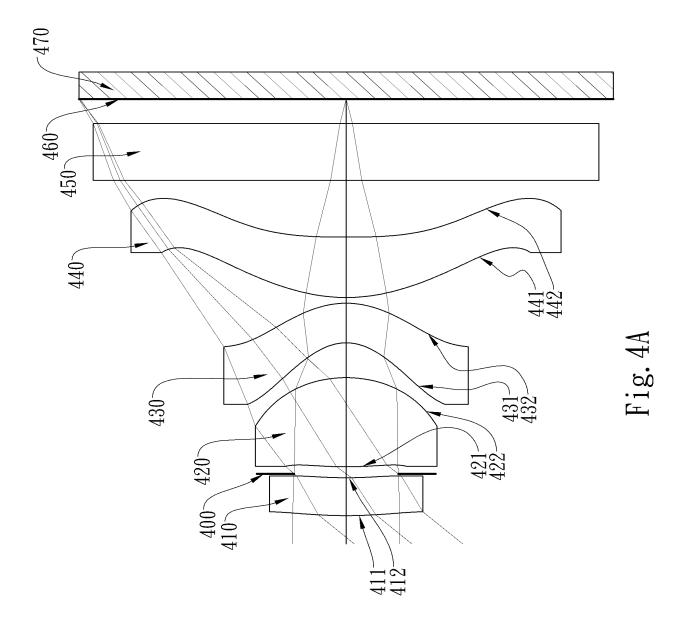


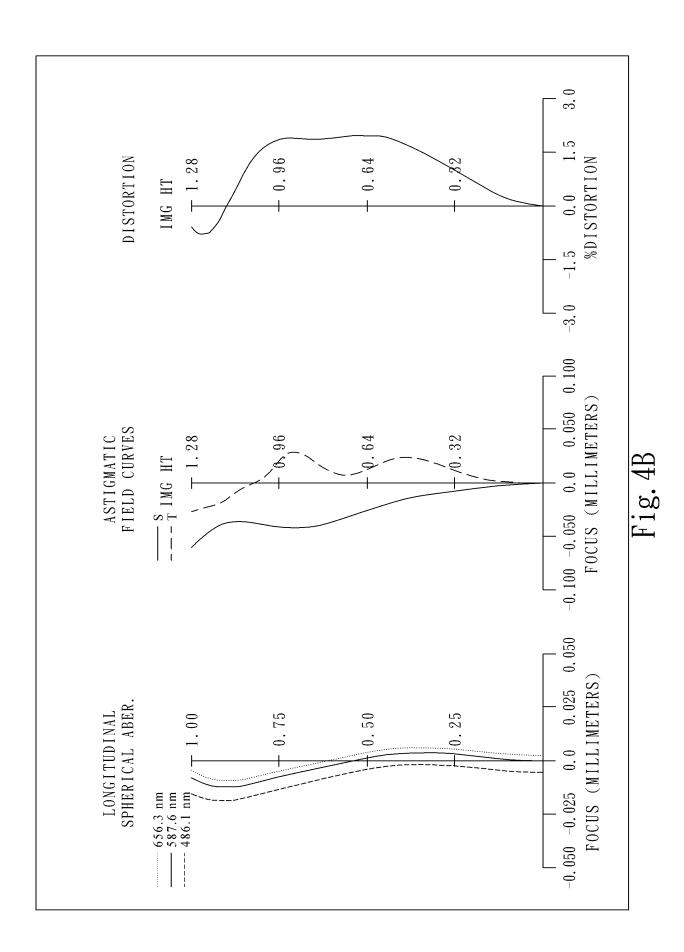
HP, Ex. 1002 Page 68



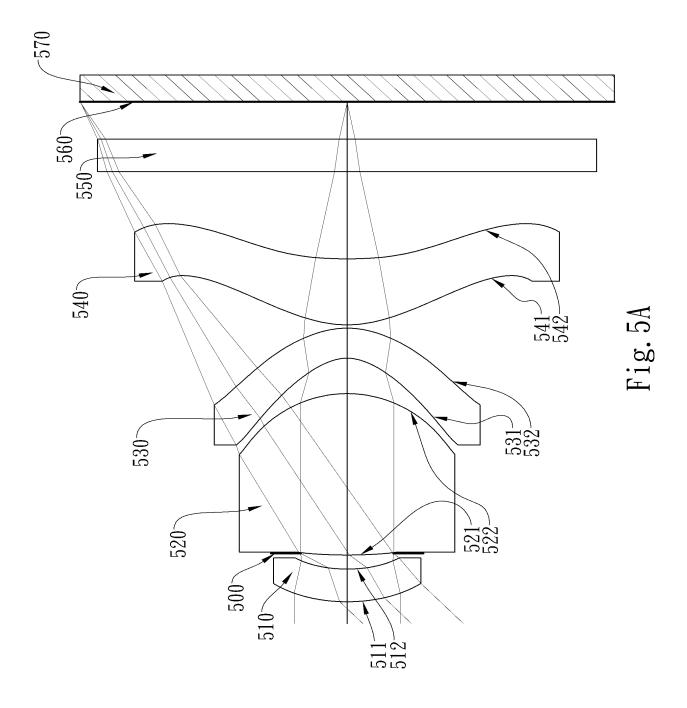


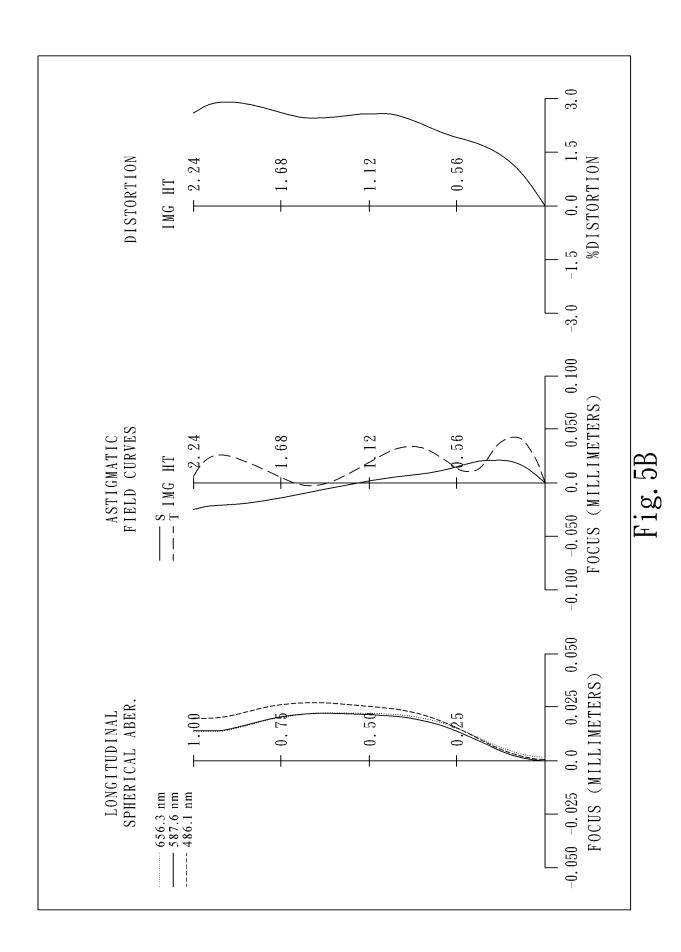
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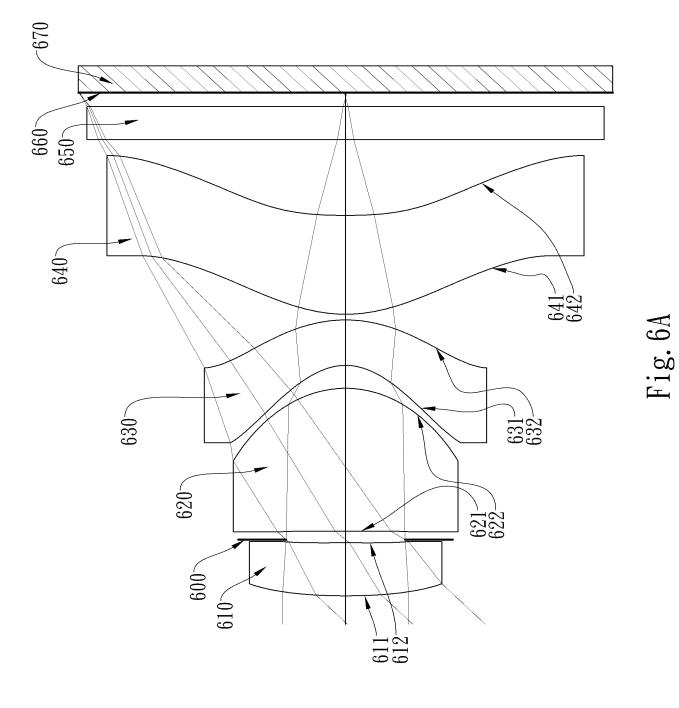


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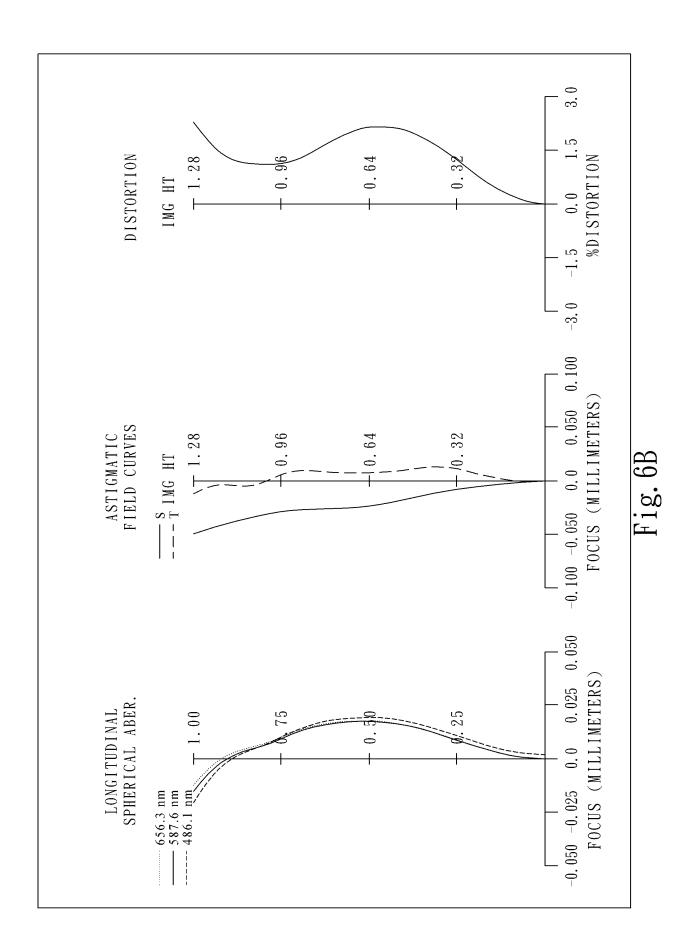




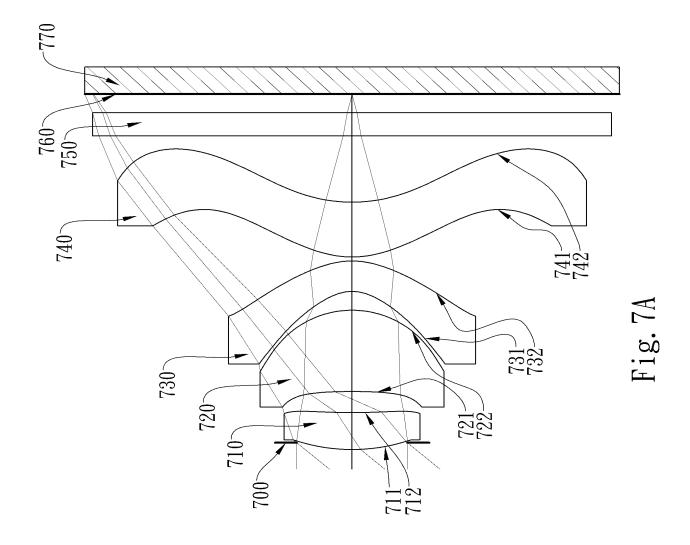
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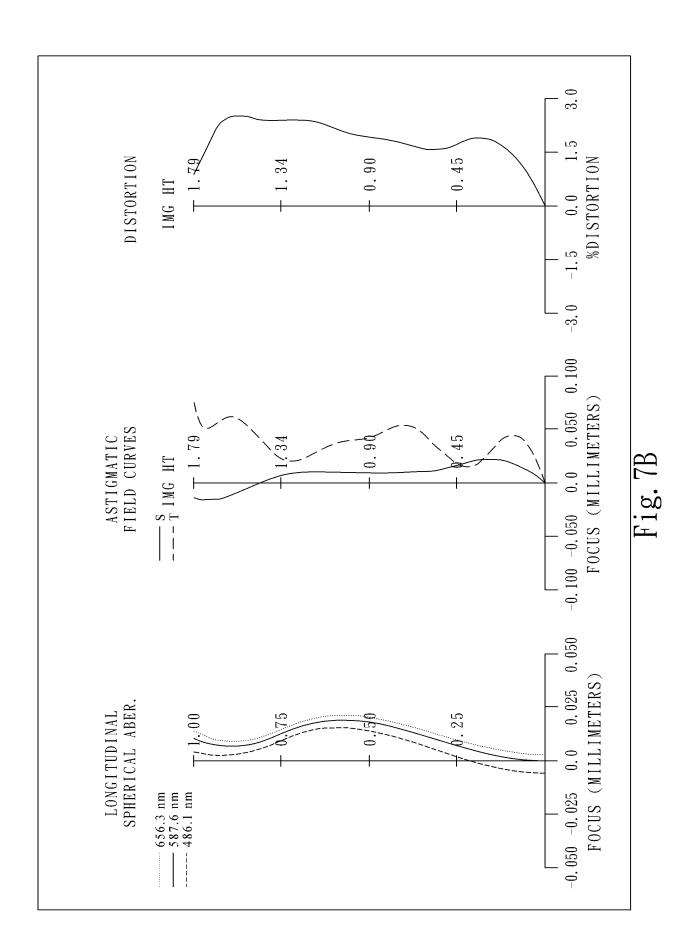


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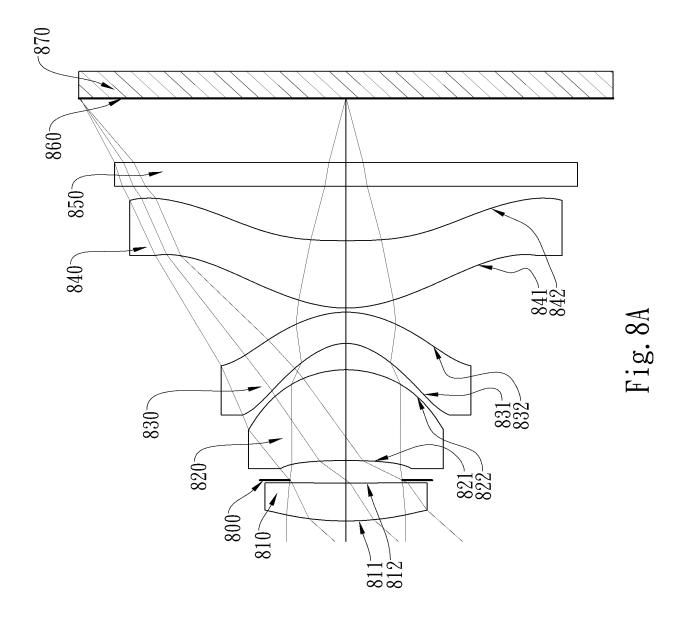


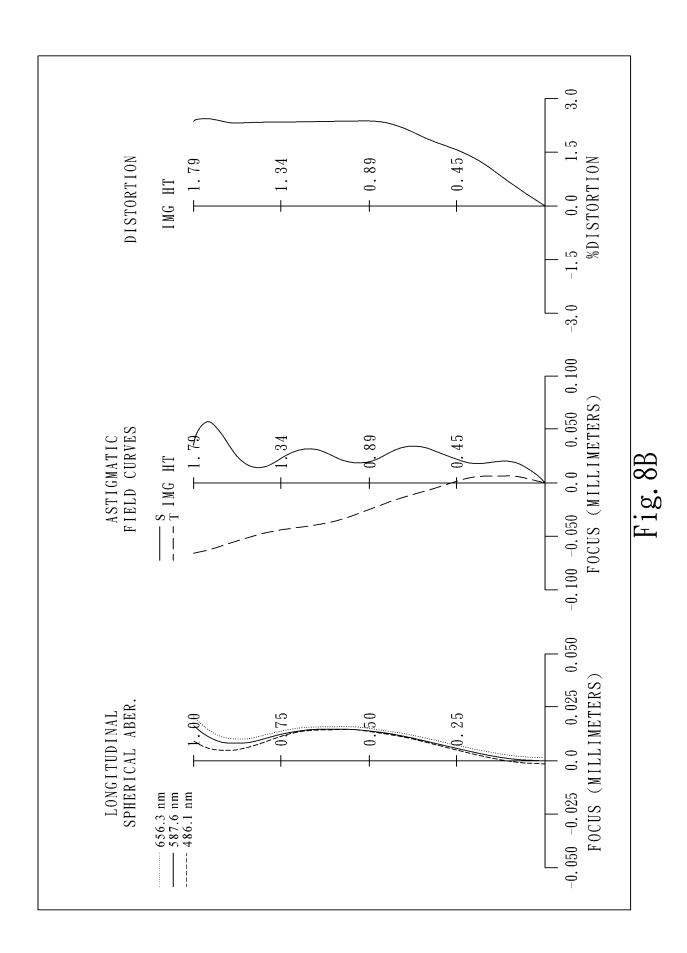
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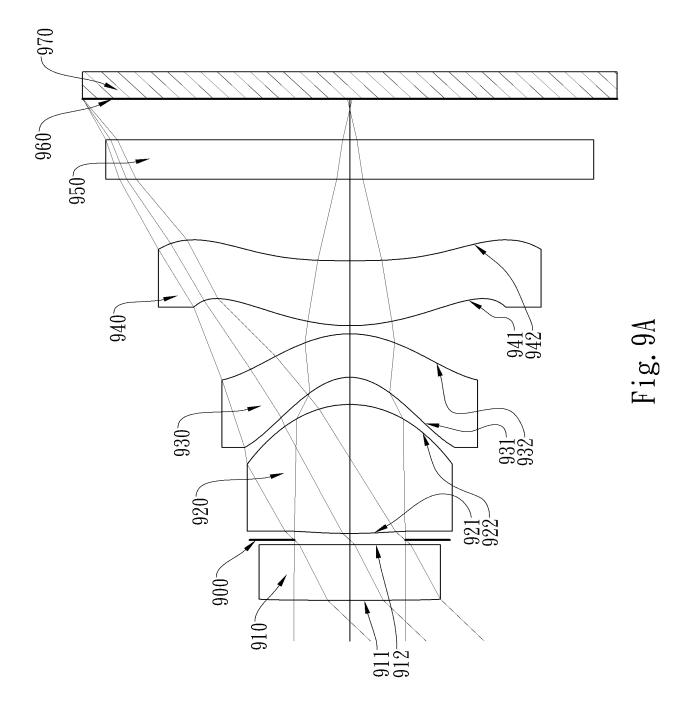


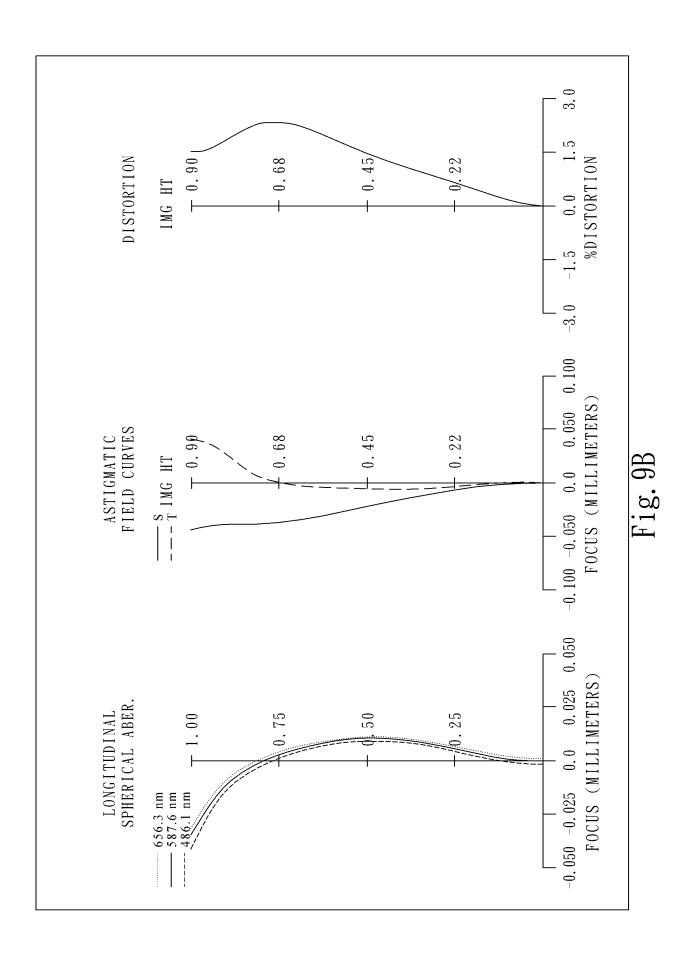
HP, Ex. 1002 Page 78



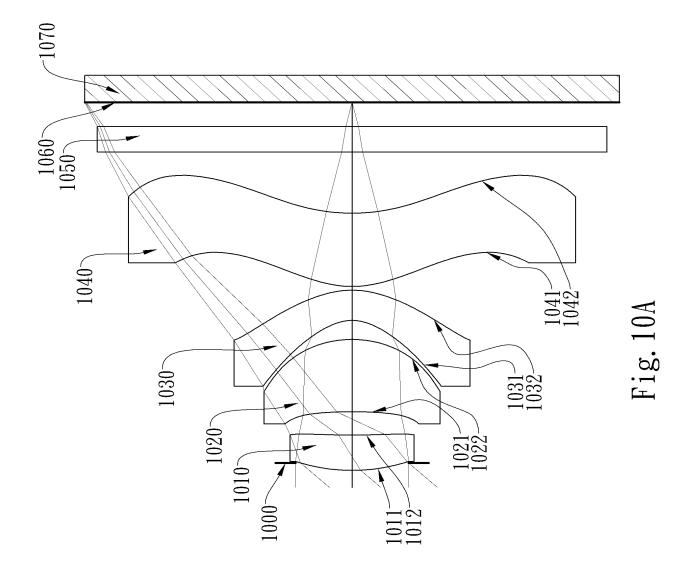


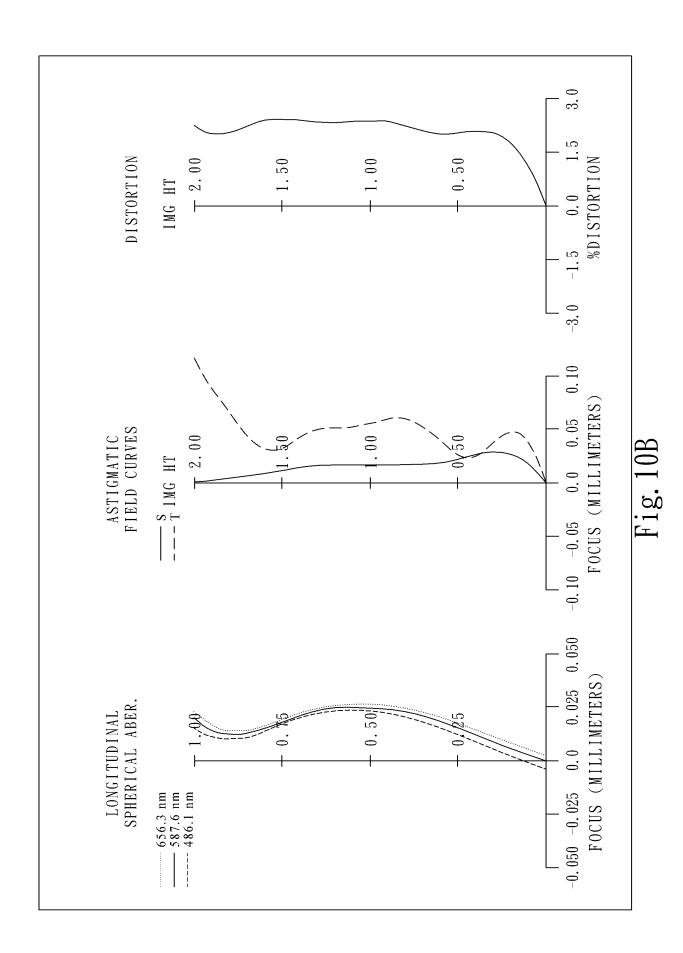
HP, Ex. 1002 Page 80



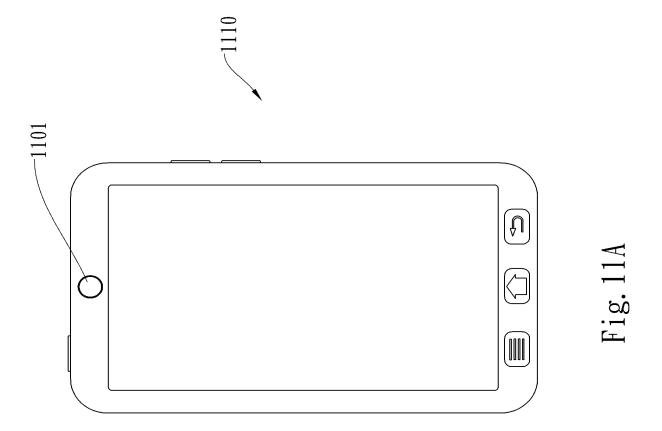


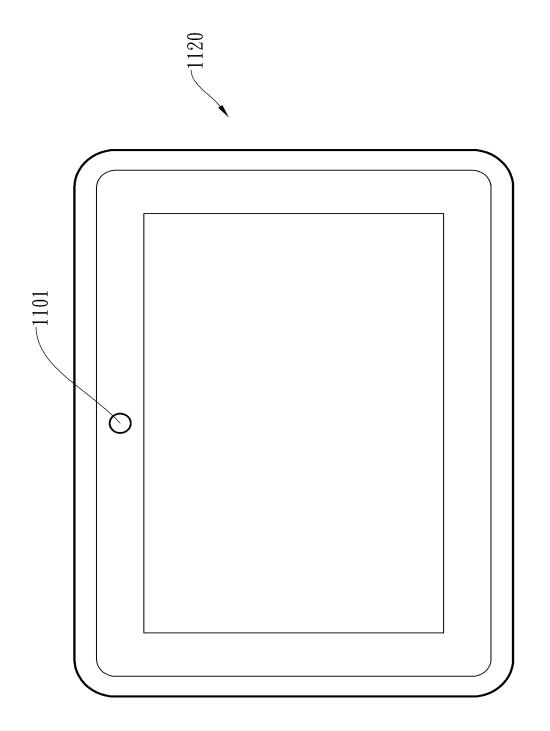
HP, Ex. 1002 Page 82

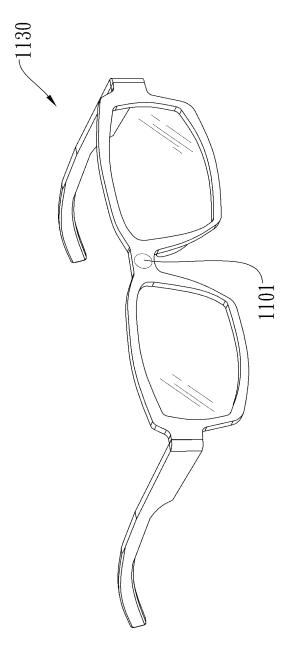




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Application Number					
Filing Date		December 13, 2013			
First Named Inv	entor	WEI-YU CHEN			
Title		IMAGE CAPTURING LENS SYSTEM, IM	IAGING DEV	ICE AND MOBILE TERMINAL	
Art Unit					
Examiner Name	•				
Attorney Docket	Number	14970-94702			
	SIGNAT	URE of Applicant or Patent Practitioner			
Signature	/Tim Tingk	ang Xia/	Date	December 13, 2013	
Name	Tim Ting	Tim Tingkang Xia		4044953678	
Registration Number 45242					
NOTE: This form must be signed in accordance with 37 CFR 1.33. See 37 CFR 1.4(d) for signature requirements and certifications.					
*Total of _1 forms are submitted.					

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### DECLARATION (37 CFR 1.63) FOR UTILITY OR DESIGN APPLICATION USING AN **APPLICATION DATA SHEET (37 CFR 1.76)**

Title of Invention	IMAGE CAPTUR	RING LENS SYSTEM, IMA	GING DEVICE AND MOBILE TERMINAL	:
As the below	w named inventor, I her	reby declare that:		
This declaration is directed to:				
	United St	tates application or PCT internation	nal application number	
	filed on _	ii yaqaiili yii a	<u></u>	
The above-i	dentified application wa	as made or authorized to be made t	by me.	
I believe tha	t I am the original inver	ntor or an original joint inventor of a	claimed invention in the application.	
I hereby ack by fine or im	nowledge that any willf prisonment of not more	ful false statement made in this decle than five (5) years, or both.	elaration is punishable under 18 U.S.C. 1001	
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LEGAL N	AME OF INVENTOR			
Inventor: _	Chen, Wei-Yu √Peì-Yu	. Chon	Date (Optional): 21 <sup>5t</sup> Nov 2013	
Note: An appl Use an additio	ication data sheet (PTO/A onal PTO/SB/AIA01 form f	MA/14 or equivalent), including naming the for each additional inventor.	the entire inventive entity, must accompany this form.	-

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Electronic Patent Application Fee Transmittal					
Application Number:					
Filing Date:					
Title of Invention:	IM.	AGE CAPTURING LE	NS SYSTEM, IM.	AGING DEVICE AND	) MOBILE TERMINAL
First Named Inventor/Applicant Name:	WE	I-YU CHEN			
Filer:	Tin	n Tingkang Xia/Deb	by Yew		
Attorney Docket Number:	149	970-94702			
Filed as Large Entity					
Utility under 35 USC 111(a) Filing Fees					
Description		Fee Code	Quantity	Amount	Sub-Total in USD(\$)
Basic Filing:					
Utility application filing		1011	1	280	280
Utility Search Fee		1111	1	600	600
Utility Examination Fee	Utility Examination Fee			720	720
Pages:					
Claims:					
Claims in Excess of 20		1202	6	80	480
Miscellaneous-Filing:					
Petition:					

Description	Fee Code	Quantity	Amount	Sub-Total in USD(\$)			
Patent-Appeals-and-Interference:							
Post-Allowance-and-Post-Issuance:	Post-Allowance-and-Post-Issuance:						
Extension-of-Time:	Extension-of-Time:						
Miscellaneous:							
	Tot	al in USD	(\$)	2080			

Electronic Acknowledgement Receipt			
EFS ID:	17655791		
Application Number:	14105811		
International Application Number:			
Confirmation Number:	5836		
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL		
First Named Inventor/Applicant Name:	WEI-YU CHEN		
Customer Number:	24728		
Filer:	Tim Tingkang Xia/Debby Yew		
Filer Authorized By:	Tim Tingkang Xia		
Attorney Docket Number:	14970-94702		
Receipt Date:	13-DEC-2013		
Filing Date:			
Time Stamp:	14:55:47		
Application Type:	Utility under 35 USC 111(a)		

# **Payment information:**

Submitted with Payment	yes
Payment Type	Deposit Account
Payment was successfully received in RAM	\$2080
RAM confirmation Number	1437
Deposit Account	503537
Authorized User	

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# File Listing:

Document Number	Document Description	File Name	File Size(Bytes)/ Message Digest	Multi Part /.zip	Pages (if appl.)
	T	1.40700.47007	191208		
1 Transmittal of New Application		1497094702Trans.pdf	c911943ffb92207dc234e0ab91fe63eb9832 931f	no	1
Warnings:					
Information:					
2	Fee Worksheet (SB06)	1497094702FeeTrans.pdf	169762	no	1
		·	6a72dbc31ee8e1ad06a105b03d9d230aa9 2a63fb		
Warnings:					
Information:					
3	Application Data Sheet	1497094702ADS.pdf	1505518	no	6
		·	d1e35235108adc89f4784a7b68494652a15 af800		
Warnings:					
Information:					
4		1497094702Spec.pdf	296526	yes	56
			832ad976d3e8915629b09063f87e1e98258 4299f		
	Multip	art Description/PDF files in	.zip description		
	Document Des	scription	Start	E	nd
	Specificati	on	1	47	
	Claims		48	į	55
	Abstrac	t	56		56
Warnings:					
Information:					
5	Drawings-only black and white line	1497094702 Drawings.pdf	619675	no	23
3	drawings	1497094702DIawings.pui	c0565e7bd2ed4bfa2dbfc4191ecf76326662 d2e0	no	23
Warnings:					
Information:					
6	Power of Attorney	1497094702POA.pdf	374075	no	2
	. 5 5. /		6db2169529065c90f140c5297ce56f97e547 deaf		-
Warnings:					

7	Oath or Declaration filed	1497094702Dec.pdf	442888	no	1
,	Cath of Decidiation filed	1437034702Dec.pui	acf5d5ef1ae069bf729dd454b2bc3aa80d36 b133		'
Warnings:					
Information:	<b>!</b>				
8	Fee Worksheet (SB06)	fee-info.pdf	37137	no	2
Ŭ	rec worksheet (5500)	rec imo.pui	ce80c93b35e126b657e711b774b52e7114 277f93		_
Warnings:					
Information:					
		3636789			

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#### New Applications Under 35 U.S.C. 111

If a new application is being filed and the application includes the necessary components for a filing date (see 37 CFR 1.53(b)-(d) and MPEP 506), a Filing Receipt (37 CFR 1.54) will be issued in due course and the date shown on this Acknowledgement Receipt will establish the filing date of the application.

#### National Stage of an International Application under 35 U.S.C. 371

If a timely submission to enter the national stage of an international application is compliant with the conditions of 35 U.S.C. 371 and other applicable requirements a Form PCT/DO/EO/903 indicating acceptance of the application as a national stage submission under 35 U.S.C. 371 will be issued in addition to the Filing Receipt, in due course.

#### New International Application Filed with the USPTO as a Receiving Office

If a new international application is being filed and the international application includes the necessary components for an international filing date (see PCT Article 11 and MPEP 1810), a Notification of the International Application Number and of the International Filing Date (Form PCT/RO/105) will be issued in due course, subject to prescriptions concerning national security, and the date shown on this Acknowledgement Receipt will establish the international filing date of the application.

									Application or Docket Number 14/105,811		
	APPL	LICATION A	S FILE		umn 2)	SMALL	ENTITY	OR	OTHER SMALL		
	FOR	NUMBE	R FILE	D NUMBE	R EXTRA	RATE(\$)	FEE(\$)	1	RATE(\$)	FEE(\$)	
	IC FEE FR 1.16(a), (b), or (c))	N	I/A	N	I/A	N/A		1	N/A	280	
SEA	RCH FEE FR 1.16(k), (i), or (m))	N	I/A	N	J/A	N/A		1	N/A	600	
EXA	MINATION FEE FR 1.16(o), (p), or (q))	N	I/A	N	J/A	N/A		1	N/A	720	
TOT	AL CLAIMS FR 1.16(i))	26	minus	20= *	6			OR	x 80 =	480	
INDE	EPENDENT CLAIM FR 1.16(h))	<sup>1S</sup> 3	minus	3 = *				1	x 420 =	0.00	
APF FEE	LICATION SIZE	\$310 (\$15 50 sheets	oaper, th 5 for sm or fraction	and drawings e e application si all entity) for ea on thereof. See CFR 1.16(s).	ze fee due is ch additional					0.00	
MUL	TIPLE DEPENDE	NT CLAIM PRE	SENT (3	7 CFR 1.16(j))						0.00	
* If th	ne difference in col	lumn 1 is less th	nan zero,	enter "0" in colur	mn 2.	TOTAL		1	TOTAL	2080	
AMENDMENT A	Total	CLAIMS REMAINING AFTER AMENDMENT	Minus	HIGHEST NUMBER PREVIOUSLY PAID FOR	PRESENT EXTRA	RATE(\$)	ADDITIONAL FEE(\$)		RATE(\$)	ADDITIONAL FEE(\$)	
	(37 CFR 1.16(i))			***	-	X =		OR	X =		
빌	Independent (37 CFR 1.16(h))		Minus			X =		OR	X =		
₹	Application Size Fee	e (37 CFR 1.16(s))	1					4			
	FIRST PRESENTA	TION OF MULTIPI	LE DEPEN	DENT CLAIM (37 (	CFR 1.16(j))			OR			
						TOTAL ADD'L FEE		OR	TOTAL ADD'L FEE		
1 B		(Column 1)  CLAIMS  REMAINING  AFTER  AMENDMENT		(Column 2) HIGHEST NUMBER PREVIOUSLY PAID FOR	(Column 3) PRESENT EXTRA	RATE(\$)	ADDITIONAL FEE(\$)		RATE(\$)	ADDITIONAL FEE(\$)	
AMENDMENT	Total	*	Minus	**	=	х =		OR	x =		
	(37 CFR 1.16(i)) Independent	*	Minus	***	=	x =		OR	x =		
¥ŀ	(37 CFR 1.16(h))  Application Size Fee	e (37 CFR 1.16(s))	<u> </u>					1			
<u> </u>	FIRST PRESENTA			DENT CLAIM (37 (	CFR 1.16(ii)			OR			
						TOTAL ADD'L FEE		OR	TOTAL ADD'L FEE		
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#### United States Patent and Trademark Office

UNITED STATES DEPARTMENT OF COMMERCE United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov

	APPLICATION	FILING or	GRP ART				
	NUMBER	371(c) DATE	UNIT	FIL FEE REC'D	ATTY.DOCKET.NO	TOT CLAIMS	IND CLAIMS
•	14/105.811	12/13/2013	2872	2080	14970-94702	26	3

**CONFIRMATION NO. 5836** 

24728 MORRIS MANNING MARTIN LLP 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326

FILING RECEIPT

Date Mailed: 01/08/2014

Receipt is acknowledged of this non-provisional patent application. The application will be taken up for examination in due course. Applicant will be notified as to the results of the examination. Any correspondence concerning the application must include the following identification information: the U.S. APPLICATION NUMBER, FILING DATE, NAME OF APPLICANT, and TITLE OF INVENTION. Fees transmitted by check or draft are subject to collection. Please verify the accuracy of the data presented on this receipt. If an error is noted on this Filing Receipt, please submit a written request for a Filing Receipt Correction. Please provide a copy of this Filing Receipt with the changes noted thereon. If you received a "Notice to File Missing Parts" for this application, please submit any corrections to this Filing Receipt with your reply to the Notice. When the USPTO processes the reply to the Notice, the USPTO will generate another Filing Receipt incorporating the requested corrections

Inventor(s)

WEI-YU CHEN, Taichung, TAIWAN;

Applicant(s)

LARGAN PRECISION CO., LTD., Taichung, TAIWAN

**Assignment For Published Patent Application** 

LARGAN PRECISION CO., LTD., Taichung, TAIWAN

**Power of Attorney:** The patent practitioners associated with Customer Number <u>24728</u>

#### Domestic Applications for which benefit is claimed - None.

A proper domestic benefit claim must be provided in an Application Data Sheet in order to constitute a claim for domestic benefit. See 37 CFR 1.76 and 1.78.

**Foreign Applications** (You may be eligible to benefit from the **Patent Prosecution Highway** program at the USPTO. Please see <a href="http://www.uspto.gov">http://www.uspto.gov</a> for more information.) TAIWAN 102139029 10/29/2013

Permission to Access - A proper **Authorization to Permit Access to Application by Participating Offices** (PTO/SB/39 or its equivalent) has been received by the USPTO.

#### If Required, Foreign Filing License Granted: 01/02/2014

The country code and number of your priority application, to be used for filing abroad under the Paris Convention,

is **US 14/105,811** 

**Projected Publication Date: 04/30/2015** 

Non-Publication Request: No Early Publication Request: No

page 1 of 3

#### **Title**

IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

#### **Preliminary Class**

359

Statement under 37 CFR 1.55 or 1.78 for AIA (First Inventor to File) Transition Applications: No

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Since the rights granted by a U.S. patent extend only throughout the territory of the United States and have no effect in a foreign country, an inventor who wishes patent protection in another country must apply for a patent in a specific country or in regional patent offices. Applicants may wish to consider the filing of an international application under the Patent Cooperation Treaty (PCT). An international (PCT) application generally has the same effect as a regular national patent application in each PCT-member country. The PCT process **simplifies** the filing of patent applications on the same invention in member countries, but **does not result** in a grant of "an international patent" and does not eliminate the need of applicants to file additional documents and fees in countries where patent protection is desired.

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Applicants also are advised that in the case of inventions made in the United States, the Director of the USPTO must issue a license before applicants can apply for a patent in a foreign country. The filing of a U.S. patent application serves as a request for a foreign filing license. The application's filing receipt contains further information and guidance as to the status of applicant's license for foreign filing.

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#### Title 37, Code of Federal Regulations, 5.11 & 5.15

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## United States Patent and Trademark Office

12/13/2013

UNITED STATES DEPARTMENT OF COMMERCE UNITED STATES DEPARTMENT OF COMMI United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Vriginia 22313-1450 www.uspto.gov

APPLICATION NUMBER FILING OR 371(C) DATE FIRST NAMED APPLICANT WEI-YU CHEN

ATTY. DOCKET NO./TITLE 14970-94702

14/105,811

24728 MORRIS MANNING MARTIN LLP 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326

**CONFIRMATION NO. 5836 POA ACCEPTANCE LETTER** 



Date Mailed: 01/08/2014

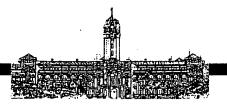
#### NOTICE OF ACCEPTANCE OF POWER OF ATTORNEY

This is in response to the Power of Attorney filed 12/13/2013.

The Power of Attorney in this application is accepted. Correspondence in this application will be mailed to the above address as provided by 37 CFR 1.33.

/hnguyen/	
Office of Data Management, Application Assistance Unit (571)	272-4000, or (571) 272-4200, or 1-888-786-0101

page 1 of 1



# 中華民國經濟部智慧財產局

INTELLECTUAL PROPERTY OFFICE MINISTRY OF ECONOMIC AFFAIRS REPUBLIC OF CHINA

茲證明所附文件,係本局存檔中原申請案的副本,正確無訛, 其申請資料如下 :

This is to certify that annexed is a true copy from the records of this office of the application as originally filed which is identified hereunder:

申 請 日: 西元 2013 年 10 月 29 日

Application Date Oct. 29, 2013

申 請 案 號: 102139029

Application No.

申 請 人: 大立光電股份有限公司

Applicant(s)

發明 人:陳緯彧

Inventor(s)



長

Director General

王美花

西元 <u>2013</u> 年 <u>11</u> 月 <u>11</u> 日



# 發明摘要

※申請案號:

※申請日:

※IPC 分類:

## 5 【發明名稱】(中文/英文)

影像拾取系統透鏡組、取像裝置及可攜裝置/ Image Capturing Lens System, Imaging Device and Mobile Terminal

# 10 【中文】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其像側面於近光軸處為凸面;及一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面。藉由上述結構,在滿足特定條件下,可有利於具備大視角及縮短系統總長度,並提升周邊解像力和照度。

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申請案號: 102139029

## 【英文】



This invention provides an image capturing lens system comprising from object-side to image-side: a first lens element with refractive power; a positive second lens element having a convex 5 image-side surface in a paraxial region; a negative third lens element having a concave object-side surface in a paraxial region and a convex image-side surface in a paraxial region; and a fourth lens element with refractive power having a concave image-side surface in a paraxial region, both of the object-side and image-side surfaces being aspheric, and the image-side surface has at least a convex shape at an off-axis region thereof. When particular relations are satisfied with the aforesaid structure configuration, wide field of view can be obtained, the total track length can be favorably reduced and the resolution for peripheral image and illumination can be improved.

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# 【代表圖】

【本案指定代表圖】: 第( -A)圖。

【本代表圖之符號簡單說明】:

5	光圈	100		
	第一透鏡	110		
	物側面	111	像側面	112
	第二透鏡	120		,
	物側面	121	像側面	122
10	第三透鏡	130		
	物側面	131	像側面	132
	第四透鏡	140		
	物側面	141	像側面	142
	紅外線濾除濾	光元件	150	
15	成像面	160		
	電子感光元件	= 170	•	

# 【本案若有化學式時,請揭示最能顯示發明特徵的化學式】:

20 無

申請案號: 102139029

# 發明專利說明書



(本說明督格式、順序,請勿任意更動)

## 【發明名稱】(中文/英文)

影像拾取系統透鏡組、取像裝置及可攜裝置/ Image Capturing Lens System, Imaging Device and Mobile Terminal

### 【技術領域】

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本發明係關於一種影像拾取系統透鏡組,特別是關於一種應 10 用於可攜式電子產品的影像拾取系統透鏡組。

### 【先前技術】

隨著個人電子產品逐漸輕薄化,電子產品內部各零組件被要求具有更小的尺寸。攝影鏡頭的尺寸在這個趨勢下同樣面臨著小型化的要求。除了小型化的要求之外,因為半導體製程技術的進步使得感光元件的畫素面積縮小,攝影鏡頭逐漸往高畫素領域發展,因此,對成像品質的要求也日益增加。

傳統搭載於可攜式電子產品上的小型化光學系統,多採用三 片式透鏡結構為主,但由於智慧型手機(Smart Phone)、平板電腦 (Tablet PC)與可穿戴式設備(Wearable Apparatus)等高規格可攜裝 置(Mobile Terminal)的盛行,使得攝影鏡頭在畫素與成像品質上 的迅速攀升,習知的三片式攝影鏡頭已無法滿足更高階的攝影需 求。

領域中亦提出四片式透鏡組,期能提供更優異的成像品質。 然而,習用四片式透鏡組往往未能在大視角及鏡頭總長度之間取 得良好的平衡,且對於周邊影像的解像力與照度也不甚理想,尚 未能滿足領域中所要求的高階成像品質。

因此,領域中急需一種在滿足小型化的條件下,具有良好之

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申請案號: 102139029



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### 【發明內容】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其像側面於近光軸處為凹面,其物側面及像側面皆為非球面,且其像側面於近光軸處為凹面,其物側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組的無距為 f,該第四透鏡的焦距為 f4,該第二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係式:0.5 mm < Td < 3.2 mm;1.0 mm < Td / tan(HFOV) < 3.75 mm;|f/f4| < 1.20;及 f2 / f3 < -0.65。

另一方面,本發明提供一種影像拾取系統透鏡組,由物側至像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近光軸處為凸面;及一具屈折力的第四透鏡,其像側面於近光軸處為凸面;及一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第三透鏡的焦距為f3,係滿足下列關係式:0.5 mm < Td < 3.2 mm;1.0 mm < Td / tan(HFOV) < 3.75 mm;|f/f4| < 1.20;及-2.0 < f/f3 < -0.95。

又一方面,本發明提供一種影像拾取系統透鏡組,由物側至像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近光軸處為凸面;及一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物側面及像側面皆為非球面,且其像側面於雖軸處具有至少一凸面;其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該影像拾取系統透鏡組的光圈值為 Fno,係滿足下列關係式:0.5 mm < Td < 3.2 mm;1.0 mm < Td / tan(HFOV) < 3.75 mm;|f/f4| < 1.20;及 1.40 < Fno < 2.25。

再一方面,本發明提供一種取像裝置,包含如前述的影像拾 取系統透鏡組及一電子感光元件。

更一方面,本發明提供一種可攜裝置,包含如前述的取像裝置。

當 Td 滿足上述條件時,有利於維持系統的小型化。

當 Td / tan(HFOV)滿足上述條件時,有助於使該影像拾取系統透鏡組同時具備大視角及短總長的特性。

當|f / f4|滿足上述條件時,可使系統的主點更遠離成像面, 有利於縮短系統的光學總長度,以維持鏡頭的小型化。

當 f2 / f3 滿足上述條件時,該第二透鏡與該第三透鏡的屈折力配置較為平衡,可有助於像差的修正與敏感度的降低。

當 f / f3 滿足上述條件時,該第三透鏡的作用如同補正透鏡, 其功能為平衡及修正系統所產生的各項像差,進而可使系統獲得 更高的成像品質。

當 Fno 滿足上述條件時,有助於提升系統的周邊照度。

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### 【圖式簡單說明】

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第一 A 圖係本發明第一實施例的取像裝置示意圖。

第一B圖係本發明第一實施例的像差曲線圖。

第二 A 圖係本發明第二實施例的取像裝置示意圖。

第二B圖係本發明第二實施例的像差曲線圖。

第三 A 圖係本發明第三實施例的取像裝置示意圖。

第三 B 圖係本發明第三實施例的像差曲線圖。

第四A圖係本發明第四實施例的取像裝置示意圖。

第四 B 圖係本發明第四實施例的像差曲線圖。

第五 A 圖係本發明第五實施例的取像裝置示意圖。

第五 B 圖係本發明第五實施例的像差曲線圖。

第六 A 圖係本發明第六實施例的取像裝置示意圖。

第六 B 圖係本發明第六實施例的像差曲線圖。

第七A圖係本發明第七實施例的取像裝置示意圖。

第七 B 圖係本發明第七實施例的像差曲線圖。

第八 A 圖係本發明第八實施例的取像裝置示意圖。

第八 B 圖係本發明第八實施例的像差曲線圖。

第九 A 圖係本發明第九實施例的取像裝置示意圖。

第九 B 圖係本發明第九實施例的像差曲線圖。

第十A圖係本發明第十實施例的取像裝置示意圖。

第十B圖係本發明第十實施例的像差曲線圖。

第十一 A 圖係示意裝設有本發明之取像裝置的智慧型手機。

第十一B圖係示意裝設有本發明之取像裝置的平板電腦。

第十一 C 圖係示意裝設有本發明之取像裝置的可穿戴式設

25 備。

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# 【實施方式】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包 含具屈折力的第一透鏡、第二透鏡、第三透鏡、及第四透鏡。 該第一透鏡可具有正屈折力,可提供系統所需的正屈折力, 有助於縮短系統的總長度。該第一透鏡物側面可為凸面,可有效 加強縮短光學總長度的功效。

該第二透鏡具正屈折力,有助於利用第二透鏡調和第一透鏡的匯聚能力。該第二透鏡的像側面於近光軸處為凸面,有助於修正系統的像散。

該第三透鏡具負屈折力,有助於系統的像差修正。該第三透鏡物側面近光軸處為凹面,其像側面近光軸處為凸面,可有助於修正系統的像散。

該第四透鏡物側面近光軸處可為凸面,其像側面近光軸處為凹面,且其像側面於離軸處具有至少一凸面,有助於修正系統非點收差(Astigmatism),並可有效修正離軸像差。

該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,當影像拾取系統透鏡組滿足下列關係式: 0.5 mm < Td < 3.2 mm 時,有利於維持系統的小型化;較佳地,滿足下列關係式: 0.8 mm < Td < 2.5 mm。

該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,當影像 拾取系統透鏡組滿足下列關係式:1.0 mm < Td / tan(HFOV) < 3.75 mm 時,有助於使該影像拾取系統透鏡組同時具備大視角及 短總長的特性;較佳地,滿足下列關係式:1.2 mm < Td / tan(HFOV) < 2.75 mm。

該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,當影像拾取系統透鏡組滿足下列關係式: |f/f4| < 1.20 時,可使系統的主點更遠離成像面,有利於縮短系統的光學總長度,以維持鏡頭的小型化。

該第二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,當影像拾取系統透鏡組滿足下列關係式:f2/f3<-0.65 時,該第二透鏡與該第三透鏡的屈折力配置較為平衡,可有助於像差的修正與敏感

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度的降低;較佳地,滿足下列關係式:f2/f3<-0.75。

該影像拾取系統透鏡組的焦距為 f,該第三透鏡的焦距為f3,當影像拾取系統透鏡組滿足下列關係式:-2.0 < f/f3 <-0.95時,該第三透鏡的作用如同補正透鏡,其功能為平衡及修正系統所產生的各項像差,進而可使系統獲得更高的成像品質。

該影像拾取系統透鏡組的光圈值為 Fno, 當影像拾取系統透鏡組滿足下列關係式: 1.40 < Fno ≤ 2.25 時, 有助於提升系統的周邊照度。

該影像拾取系統透鏡組的焦距為 f, 該第一透鏡的焦距為 fl, 10 當影像拾取系統透鏡組滿足下列關係式: -0.25 < f/fl < 0.75 時, 該第一透鏡的屈折力較為合適,避免敏感度過高;較佳地,滿足 下列關係式: 0.25 < f/fl < 0.75。

該第二透鏡物側面的曲率半徑為 R3,該第二透鏡像側面的曲率半徑為 R4。當影像拾取系統透鏡組滿足下列關係式: 0.5 < (R3+R4)/(R3-R4)<2.5 時,有助於加強像差的修正。

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該影像拾取系統透鏡組的焦距為 f, 當影像拾取系統透鏡組滿足下列關係式: 0.5 mm < f < 2.0 mm 時, 有助於提供適當的光學總長度。

該第一透鏡、該第二透鏡、該第三透鏡、及該第四透鏡於光軸上之厚度的總合為ΣCT,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,當影像拾取系統透鏡組滿足下列關係式:0.80 < ΣCT / Td < 0.95 時,有利於該影像拾取系統透鏡組的組裝,並降低敏感度。

該第一透鏡的色散係數為 V1, 當影像拾取系統透鏡組滿足下列關係式: 45 < V1 時, 可有效修正系統色差。

該第二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於光軸上的厚度為 CT4,當影像拾取系統透鏡組滿足下列關係式: 0.65 < CT2 / (CT1+CT3+CT4) < 2.0 時,各透鏡的厚度較為合適,

有助於鏡片的製作及組裝。

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該影像拾取系統透鏡組的最大視角為 FOV, 當影像拾取系統透鏡組滿足下列關係式: 80 度 < FOV < 110 度時, 有利於取得足夠的視場角。

本發明的影像拾取系統透鏡組中,透鏡的材質可為玻璃或塑膠,若透鏡的材質為玻璃,則可以增加該影像拾取系統透鏡組屈折力配置的自由度,若透鏡材質為塑膠,則可以有效降低生產成本。此外,可於鏡面上設置非球面(ASP),非球面可以容易製作成球面以外的形狀,獲得較多的控制變數,用以消減像差,進而縮減透鏡使用的數目,因此可以有效降低本發明的影像拾取系統透鏡組的總長度。

本發明的影像拾取系統透鏡組中,可至少設置一光闌,如孔徑光闌(Aperture Stop)、耀光光闌(Glare Stop)或視場光闌(Field Stop)等。

本發明影像拾取系統透鏡組中,光圈配置可為前置或中置,其中前置光圈意即光圈設置於被攝物與第一透鏡間,中置光圈則表示光圈設置於第一透鏡與成像面間,前置光圈可使影像拾取系統透鏡組的出射瞳(Exit Pupil)與成像面產生較長的距離,使之具有遠心(Telecentric)效果,可增加電子感光元件如 CCD 或 CMOS 接收影像的效率;中置光圈則有助於擴大系統的視場角,使影像拾取系統透鏡組具有廣角鏡頭之優勢。

本發明影像拾取系統透鏡組中,就以具有屈折力的透鏡而言,若透鏡表面係為凸面且未界定該凸面位置時,則表示該透鏡表面於近光軸處為凸面;若透鏡表面係為凹面且未界定該凹面位置時,則表示該透鏡表面於近光軸處為凹面。

本發明的影像拾取系統透鏡組更可視需求應用於變焦的光學系統中,並兼具優良像差修正與良好成像品質的特色可多方面應用於 3D(三維)影像擷取、數位相機、行動裝置、數位平板與可穿戴式設備等可攜裝置中。

本發明更提供一種取像裝置,其包含前述影像拾取系統透鏡組以及電子感光元件,其中該電子感光元件設置於該影像拾取系統透鏡組的成像面,因此取像裝置可藉由影像拾取系統透鏡組的系統設計,有利於縮短大視角的系統總長,並提升周邊解像力與照度,進而達到最佳成像效果。較佳地,該取像裝置可進一步包含鏡筒(Barrel Member)、支持裝置(Holder Member)或其組合。

請參第十一 A 圖、第十一 B 圖、第十一 C 圖,該取像裝置 (1101)可搭載於可攜裝置,其包括,但不限於:智慧型手機(1110)、平板電腦(1120)、或可穿戴式設備(1130)。前揭可攜裝置僅是示範性地說明本發明之取像裝置的實際運用例子,並非限制本發明之取像裝置的運用範圍。較佳地,該可攜裝置可進一步包含控制單元(Control Unit)、顯示單元(Display)、儲存單元(ROM)、暫儲存單元(RAM)或其組合。

本發明的取像裝置及影像拾取系統透鏡組將藉由以下具體 實施例配合所附圖式予以詳細說明。

# 《第一實施例》

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本發明第一實施例請參閱第一 A 圖,第一實施例的像差曲線請參閱第一 B 圖。第一實施例的取像裝置包含影像拾取系統透鏡組與一電子感光元件(170),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

- 一具正屈折力的第一透鏡(110),其材質為塑膠,其物側面(111)於近光軸處為凸面,其像側面(112)於近光軸處為凹面,且其兩面皆為非球面;
- 25 一具正屈折力的第二透鏡(120),其材質為塑膠,其物側面 (121)於近光軸處為凸面,其像側面(122)於近光軸處為凸面,且 其兩面皆為非球面;

- 一具負屈折力的第三透鏡(130),其材質為塑膠,其物側面(131)於近光軸處為凹面,其像側面(132)於近光軸處為凸面,且 其兩面皆為非球面;及
- 一具正屈折力的第四透鏡(140),其材質為塑膠,其物側面(141)於近光軸處為凸面,其像側面(142)於近光軸處為凹面,其兩面皆為非球面,且其像側面(142)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(100),置於該第一透鏡(110)與該第二透鏡(120)間;另包含有一紅外線濾除濾光元件(IR-cut filter)(150)置於該第四透鏡(140)與一成像面(160)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(170)設置於該成像面(160)上。

第一實施例詳細的光學數據如表一所示,其非球面數據如表 二所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV定義 為最大視角的一半。

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		** Filtrations of	表					
			(第一)	矿施例)				
		<u>f=1.J7 m</u>	m, Fno = 2.	20. HFOV =	= 46.7 deg,			
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.666	ASP	0.256	塑膠	1.650	21.4	9.56
2		2.139	ASP	0.031				
3	光圈	平面	,	0.019				
4	第二透鏡	5.712	ASP	0.671	塑膠	1.544	55.9	0.82
5		-0.464	ASP	0.130				
6	第三透鏡	-0.228	ASP	0.230	塑膠	1.634	23.8	-1.06
7		-0.480	ASP	0.030				
8	第四透鏡	0.679	ASP	0.483	塑膠	1.535	55.7	1.52
9		3.062	ASP	0.300				
10	红外線膨除	平面		0.145	玻璃	1.517	64.2	-
11	<b>泡光</b> 片	平面		0.204				
12	成像面	平面						
注:参考	波長為 d-line	587.6 nm						

	·	装二	•					
	非球面係數							
表面 #	1	2	4	5				
k =	1.2237E+00	1.7244E+01	9.0000E+01	-6.9311E-01				
A4 =	3.1416E-01	1.1703E+00	-4.1498E-01	-6.9345E-01				
A6 =	-1.0010E+00	-2.0080E+01	. 3.6416E+00	1.3202E+00				
A8 =	4.5872E+01	5.2569E+02	4.3035E+01	1.0955E+01				
A10 =	-5.9339E+02	-3.0044E+03	-7.4996E+03	-3.8285E+02				
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0040E+03				
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04				
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04				
表面 #	6 ·.	7	8	. 9				
k =	-9.8477E-01	-3.2669E+00	-6.1619E-01	-1.4636E+01				
A4 =	3.5682E+00	-1.8915E+00	-1.2870E+00	1.2883E+00				
A6 =	-3.7958E+00	8.7075E+00	3.1244E+00	-3.7603E+00				
A8 =	-1.1135E+02	-3.6761E+01	-9.1933E+00	5.9040E+00				
A10 =	1.5862E+03	1.7257E+02	1.7146E+01	-5.8521E+00				
A12 =	-8.7685E+03	-4.8146E+02	-1.9850E+01	3.5356E+00				
A14 =	2.3054E+04	6.7728E+02	1.2752E+01	-1.1759E+00				
_ A16 =	-2.3557E+04	-3.6747E+02	-3.5165E+00	1.6169E-01				

上述的非球面曲線的方程式表示如下:

$$X(Y)=(Y^2/R)/(1+sqrt(1-(1+k)*(Y/R)^2))+\sum_i (Ai)*(Y^i)$$

其中:

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X: 非球面上距離光軸為Y的點,其與相切於非球面光軸上 頂點之切面的相對距離;

Y:非球面曲線上的點與光軸的垂直距離;

R: 曲率半徑;

k:錐面係數;

10 Ai:第i階非球面係數。

影像拾取系統透鏡組的焦距為 f,影像拾取系統透鏡組的光圈 值為 Fno,影像拾取系統透鏡組中最大視角的一半為 HFOV,其數值為:f=1.17 (毫米),Fno=2.20,HFOV=46.7 (度)。

該第一透鏡(110)的色散係數為 V1,其關係式為: V1 = 21.4。

該第二透鏡(120)於光軸上的厚度為 CT2, 該第一透鏡(110)於 光軸上的厚度為 CT1, 該第三透鏡(130)於光軸上的厚度為 CT3, 該第四透鏡(140)於光軸上的厚度為 CT4, 其關係式為: CT2/ (CT1+CT3+CT4) = 0.69。

該第二透鏡物側面(121)的曲率半徑為 R3, 該第二透鏡像側面(122)的曲率半徑為 R4, 其關係式為:(R3+R4)/(R3-R4)=0.85。

該影像拾取系統透鏡組的焦距為 f,該第一透鏡(110)的焦距為 fl,其關係式為: f/fl=0.12。

該第二透鏡(120)的焦距為 f2,該第三透鏡(130)的焦距為 f3, 10 其關係式為:f2/f3 = -0.77。

該影像拾取系統透鏡組的焦距為 f,該第四透鏡(140)的焦距為 f4,其關係式為: |f/f4| = 0.77。

該影像拾取系統透鏡組的焦距為 f, 該第三透鏡(130)的焦距為 f3, 其關係式為:f/ f3 = -1.10。

15 該第一透鏡物側面(111)至該第四透鏡像側面(142)於光軸上的距離為 Td, 其關係式為: Td = 1.850(毫米)。

該第一透鏡(110)、該第二透鏡(120)、該第三透鏡(130)、及該第四透鏡(140)於光軸上之厚度的總合為 $\Sigma$ CT,該第一透鏡物側面(111)至該第四透鏡像側面(142)於光軸上的距離為 Td,其關係式為: $\Sigma$ CT / Td = 0.89。

該第一透鏡物側面(111)至該第四透鏡像側面(142)於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為HFOV,其關係式為: Td/tan(HFOV) = 1.74(毫米)。

該影像拾取系統透鏡組的最大視角為 FOV, 其關係式為: FOV 25 = 93.4(度)。

## 《第二實施例》

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本發明第二實施例請參閱第二 A 圖,第二實施例的像差曲線請參閱第二 B 圖。第二實施例的取像裝置包含影像拾取系統透鏡

組與一電子感光元件(270),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

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- 一具正屈折力的第一透鏡(210),其材質為塑膠,其物側面(211)於近光軸處為凸面,其像側面(212)於近光軸處為凹面,且其兩面皆為非球面;
- 一具正屈折力的第二透鏡(220),其材質為塑膠,其物側面(221)於近光軸處為凸面,其像側面(222)於近光軸處為凸面,且 其兩面皆為非球面;
- 一具負屈折力的第三透鏡(230),其材質為塑膠,其物側面 10 (231)於近光軸處為凹面,其像側面(232)於近光軸處為凸面,且 其兩面皆為非球面;及
  - 一具正屈折力的第四透鏡(240),其材質為塑膠,其物側面(241)於近光軸處為凸面,其像側面(242)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(242)於離軸處具有至少一凸面;
  - 其中,該影像拾取系統透鏡組另設置有一光圈(200),置於該第一透鏡(210)與該第二透鏡(220)間;另包含有一紅外線濾除濾光元件(250)置於該第四透鏡(240)與一成像面(260)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(270)設置於該成像面(260)上。

20 第二實施例詳細的光學數據如表三所示,其非球面數據如表 四所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義 為最大視角的一半。

			农	E .				
			(第二)	實施例)				
		<u>f = 1.23</u>	mm, Fno = 2.	45, HFOV =	= 45.6 deg.	_		
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.728	ASP	0.217	塑膠	1.640	22.0	1207.16
2		1.647	ASP	0.041				
3	光圈	平面		0.020			1	

4	第二透鏡	2.201	ASP	0.685	塑膠	1.544	55.9	0.78
5		-0.465	ASP	0.138		<del>"</del> .		
6	第三透鏡	-0.213	ASP	0.222	塑膠	1.634	23.8	-0.90
7		-0.479	ASP	0.030				
8	第四透鏡	0.691	ASP	0.430	塑膠	1.535	55.7	1.40
9		7.112	ASP	0.300	•			
10	紅外線液除	平面		0.300	玻璃	1.517	64.2	-
11	<b>適光</b> 片	平面		0.171				
12	成像面	平面		-				

		表四							
	非球面係數								
表面#	1	2	4	5					
k =	-7.8611E-01	2.2256E+01	4.4287E+01	-6.8249E-01					
A4 =	2.7433E-01	3.5449E-01	-1.1581E+00	-5.9944E-01					
A6 =	-1.5466E+00	-2:9377E+01	8.9406E-01	3.6061E-01					
A8 =	4.7455E+01	6.4129E+02	4.1870E+01	1.6896E+01					
A10 =	-6.0092E+02	-3.8207E+03	-7.3180E+03	-3.8194E+02					
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0043E+03					
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04					
A16=	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04					
表面#	6	7	8	9					
k =	-1.0107E÷00	-3.0532E+00	-7.4231E-01	2.2155E+01					
A4 =	3.8803E+00	-1.7079E+00	-1.1152E+00	1.6267E+00					
A6 =	-4.2860E÷00	8.7245E+00	2.9613E+00	-4.5228E+00					
A8 =	-1.1314E+02	-3.7291E+01	-9.2058E+00	6.4630E+00					
A 10 =	1.5859E+03	1.7181E+02	1.7048E+01	-5.8730E+00					
A12 =	-8.7686E+03	-4.8143E+02	-1.9563E+01	3.4083E+00					
A14=	2.3054E+04	6.7878E+02	1.3110E+01	-1.1920E+00					
A16 =	-2.3557E+04	-3.6776E+02	-4.1607E+00	1.9105E-01					

第二實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表五中所列。

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	表五		
	第二實施	<b></b> 色例	
f (mm)	1.23	f2/f3	-0.87
Fno	2.45	6764	0.88
HFOV [deg.]	45.6	98	-1.37

VI	22.0	Td [mm]	1.783
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.87
(R3+R4)/(R3-R4)	0.65	Td/tan(HFOV) [mm]	1.75
€fi.	0.00	FOV [deg.]	91.2

#### 《第三實施例》

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本發明第三實施例請參閱第三 A 圖,第三實施例的像差曲線請參閱第三 B 圖。第三實施例的取像裝置包含影像拾取系統透鏡組與一電子感光元件(370),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

- 一具正屈折力的第一透鏡(310),其材質為塑膠,其物側面(311)於近光軸處為凸面,其像側面(312)於近光軸處為凹面,且其兩面皆為非球面;
- 10 一具正屈折力的第二透鏡(320),其材質為塑膠,其物側面 (321)於近光軸處為凹面,其像側面(322)於近光軸處為凸面,且 其兩面皆為非球面;
  - 一具負屈折力的第三透鏡(330),其材質為塑膠,其物側面(331)於近光軸處為凹面,其像側面(332)於近光軸處為凸面,且 其兩面皆為非球面:及
  - 一具正屈折力的第四透鏡(340),其材質為塑膠,其物側面(341)於近光軸處為凸面,其像側面(342)於近光軸處為凹面,其兩面皆為非球面,且其像側面(342)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(300),置於該 20 第一透鏡(310)與該第二透鏡(320)間;另包含有一紅外線濾除濾 光元件(350)置於該第四透鏡(340)與一成像面(360)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(370)設置於該成像面(360)上。

第三實施例詳細的光學數據如表六所示,其非球面數據如表 25 七所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV定義 為最大視角的一半。

				·六			<del></del>	
			(第三)	實施例)			<del></del>	
		f = 1.66 m	m, Fno = 2.	15, HFOV =	= 46.8 deg.			
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.333	ASP	0.286	塑膠	1.544	55.9	2.50
2		59.851	ASP	0.005				
3	光圈	平面		0.195				
4	第二透鏡	-1.920	ASP	0.409	塑膠	1.544	55.9	1.60
5		-0.644	ASP	0.156				
6	第三透鏡	-0.263	ASP	0.200	塑膠	1.650	21.4	-1.49
7		-0.470	ASP	0.030				
8	第四透鏡	0.677	ASP	0.363	塑膠	1.535	55.7	.2.33
9		1.206	ASP	0.400				
10	紅外線泡除	平面		0.175	玻璃	1.517	64.2	
11	遮光片	平面		0.431				
12	成像面	平面		-				
主:参考	波長為 d-line	587.6 nm		******	•	<u> </u>	***************************************	
	第1面有效	半徑為 0.510 mm						

		表七						
	非球面係數							
表面#	1	2	4	5				
k =	-2.4704E+00	9.0000E+01	5.8947E+00	-3.7972E-01				
A4 =	-3.4848E-02	-3.8775E-01	-9.3075E-01	-3.3741E-01				
A6 =	-4.4471E-01	-2.8417E+00	3.6516E+00	9.2277E-01				
A8 =	-4.9925E-01	1.8185E+01	-4.0769E+01	-3.9461E+00				
A10 =	-1.2166E+01	-2.0954E+01	-4.4351E+00	-1.9037E+01				
A12 =	3.9114E+01	-1.4998E+03	1.2130E+03	4.9148E+01				
A14 =	-1.7950E+02	1.2389E+04	-4.4615E+03	1.0076E+02				
A16=	3.3572E+02	-2.9058E+04	6.2425E+03	8.0489E+01				
表面#	6	7	8	9				
k =	-1.1491E+00	-2.3808E+00	-1.7649E+00	-1.0689E+01				
A4 =	4.2079E+00	2.1562E-01	-6.9591E-01	9.1971E-01				
A6 =	-2.8310E+01	-4.4239E+00	1.2041E+00	-3.0958E+00				
A8 =	1.2287E+02	1.8790E+01	-2.9023E÷00	4.8713E+00				
A10 =	-3.9035E+02	-4.1840E+01	4.4195E+00	-4.6279E+00				
A12 =	8.5064E+02	5.5883E+01	-3.7857E+00	2.6418E+00				
A14 =	-9.7331E+02	-4.0255E+01	1.6532E+00	-8.3581E-01				
A16=	4.7213E+02	1.4428E+01	-2.8192E-01	1.1204E-01				

第三實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表八中所列。

	₹	八	
	第三	實施例	· · · · · · · · · · · · · · · · · · ·
f [mm]	1.66	f2/B	-1.07
Fno	2.15	f/f4	0.71
HFOV [deg.]	46.8	f/f3	-1.11
VI	55.9	Td [mm]	1.644
CT2/(CT1+CT3+CT4)	0.48	ΣCT/Τα	0.77
(R3+R4)/(R3-R4)	2.01	Td/tan(HFOV) [mm]	1.54
f/fi	0.66	FOV [deg.]	93.6

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#### 《第四實施例》

本發明第四實施例請參閱第四 A 圖,第四實施例的像差曲線請參閱第四 B 圖。第四實施例的取像裝置包含影像拾取系統透鏡組與一電子感光元件(470),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

- 一具負屈折力的第一透鏡(410),其材質為塑膠,其物側面(411)於近光軸處為凸面,其像側面(412)於近光軸處為凹面,且其兩面皆為非球面;
- 一具正屈折力的第二透鏡(420),其材質為塑膠,其物側面 (421)於近光軸處為凸面,其像側面(422)於近光軸處為凸面,且 其兩面皆為非球面;
  - 一具負屈折力的第三透鏡(430),其材質為塑膠,其物側面(431)於近光軸處為凹面,其像側面(432)於近光軸處為凸面,且 其兩面皆為非球面;及
- 20 一具正屈折力的第四透鏡(440),其材質為塑膠,其物側面 (441)於近光軸處為凸面,其像側面(442)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(442)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(400),置於該第一透鏡(410)與該第二透鏡(420)間;另包含有一紅外線濾除濾光元件(450)置於該第四透鏡(440)與一成像面(460)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(470)設置於該成像面(460)上。

第四實施例詳細的光學數據如表九所示,其非球面數據如表十所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV定義為最大視角的一半。

			- 表	九				· · · · · · · · · · · · · · · · · · ·
			(第四)	了施例)				
		<u>f = 1.15</u>	mm, Fno = 2.	22, HFOV =	= 48.5 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.999	ASP	0.200	塑膠	1.544	55.9	-46.83
2		1.789	ASP	0.021				
3	光图	平面		0.037				
4	第二透鏡	1.606	ASP	0.471	塑膠	,1.544	55.9	0.81
5		-0.543	ASP	0.184				
6	第三透鏡	-0.207	ASP	0.209	塑膠	1.634	23.8	-1.22
7		-0.393	ASP	0.030				
8	第四透鏡	0.747	ASP	0.319	塑膠	1.535	55.7	1.62
9		4.607	ASP	0.300				
10	紅外線遮除	平面		0.300	玻璃	1.517	64.2	-
11	滤光片	平面		0.130				
12	成像面	平面		-				
主:参考	波長為 d-line:	587.6 nm						

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	•	表十	•	
		非球面係數		
表面#	1	2	4	5
k =	-2.2996E+01	3.4247E+01	9.8701E+00	-4.2975E-01
A4 =	-2.1353E-01	-2.0670E+00	-2.2221E+00	-6.3795E-01
A6 =	-3.6880E+00	-3.6063E+01	-8.7081E+00	-6.5092E+00
A8 =	5.2789E+01	6.9201E+02	1.4888E÷02	4.6114E+01
A10 =	-6.4083E+02	-4.8238E+03	-8.2602E+03	-4.7532E+02
A12 =	4.0983E+03	-1.6432E+05	1.3290E+05	3.0044E+03

A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0679E+04
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3828E+04
表面#	6 .	7	8	9
k =	-1.0439E+00	-2.0056E+00	-6.4024E-01	-3.3636E+00
A4 =	4.2327E+00	-9.7476E-01	-8.3147E-01	1.0958E+00
A6 =	-3.4551E+00	1.0236E+01	2.1761E+00	-1.7086E+00
A8 =	-1.0303E+02	-3.7610E+01	-4.8336E+00	1.3575E+00
A10 =	1.5970E+03	1.6620E+02	5.0397E+00	-2.6285E+00
A12 =	-8.9315E+03	-4.9093E+02	-4.1411E+00	4.3863E+00
A14 =	2.3054E+04	6.8046E+02	3.4069E+00	-3.3963E+00
A16=	-2.3558E+04	-3.4010E+02	-1.6576E+00	9.5967E-01

第四實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表十一中所列。

	表	<del></del>					
第四實施例							
f [mm]	1.15	f2/f3	-0.66				
Fno	2.22	[E/f4]	0.71				
HFOV (deg.)	48.5	f/f3	-0.94				
VI	55.9	Td (mm)	1.471				
CT2/(CT1+CT3+CT4)	0.65	ΣCT/Td	0.82				
(R3+R4)/(R3-R4)	0.49	Td/tan(HFOV) [mm]	1.30				
ฮก	-0.02	FOV [deg.]	97.0				

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申請案號:102139029

#### 《第五實施例》

本發明第五實施例請參閱第五 A 圖,第五實施例的像差曲線請參閱第五 B 圖。第五實施例的取像裝置包含該影像拾取系統透鏡組與一電子感光元件(570),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

- 一具負屈折力的第一透鏡(510),其材質為玻璃,其物側面(511)於近光軸處為凸面,其像側面(512)於近光軸處為凹面,且其兩面皆為非球面;
- 一具正屈折力的第二透鏡(520),其材質為玻璃,其物側面 15 (521)於近光軸處為凸面,其像側面(522)於近光軸處為凸面,且

#### 其兩面皆為非球面;

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- 一具負屈折力的第三透鏡(530),其材質為塑膠,其物側面 (531)於近光軸處為凹面,其像側面(532)於近光軸處為凸面,且 其兩面皆為非球面;及
- 一具正屈折力的第四透鏡(540),其材質為塑膠,其物側面 (541)於近光軸處為凸面,其像側面(542)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(542)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(500),置於該 第一透鏡(510)與該第二透鏡(520)間;另包含有一紅外線瀨除瀨 光元件(550)置於該第四透鏡(540)與一成像面(560)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(570)設置於該成像面(560)上。

第五實施例詳細的光學數據如表十二所示,其非球面數據如 表十三所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義為最大視角的一半。

			表-	<b>-</b> =				,
			(第五1	質施例)			-	
	· ·	<u>f = 2.24 m</u>	m, Fno = 2.	51, HFOV =	= 44.2 deg.			
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.367	ASP	0.300	玻璃	2.144	17.8	-13.68
2		1.110	ASP	0.144				
3	光圈	平面		-0.015				
4	第二透鏡	3.909	ASP	1.483	玻璃	1.525	70.3	1.60
5		-0.932	ASP	0.325				
6	第三透鏡	-0.341	ASP	0.277	塑膠	1.639	23.5	-1.72
7		-0.651	ASP	0.030				
8	第四透鏡	0.897	ASP	0.606	塑膠	1.565	57.0	2.00
9		3.302	ASP	0.800				
10	红外缐遊除	平面		0.300	玻璃	1.517	64.2	-
11	遊光片	平面		0.342				
12	成像面	平面		-				
注:参考	波長為 d-line	587.6 nm		•				

		表十三							
非球面係數									
表面#		2	4	5					
k =	1.1992E+00	1.9195E+00	2.1734E+01	-7.2786E-01					
A4 =	5.8324E-02	1.2422E-01	-9.9032E-02	-1.2252E-01					
A6 =	-1.4402E-01	-5.2189E-01	5.9983E+00	5.2990E-01					
A8 =	1.0028E+00	4.2713E÷00	-1.1966E+02	-3.0301E+00					
A10 =	-4.0021E+00	1.8016E+01	1.4083E+03	7.9248E+00					
A12 =	8.9035E+00	-4.2193E+02	-9.4428E+03	-1.0795E+01					
A14 =	-9.8479E+00	2.2697E+03	3.3923E+04	6.3429E+00					
A16 =	3.0263E+00	-4.1004E+03	-5.0610E+04	-8.0066E-01					
表面#	. 6	7	8	9.					
k =	-9.8774E-01	-3.1767E+00	-8.3817E-01	-2.4331E+01					
A4 =	2.5606E÷00	-1.2881E-01	-4.2259E-01	3.5717E-01					
A6 =	-7.9740E+00	-6.6170E-01	4.3675E-01	-4.5759E-01					
A8 =	1.4853E+01	1.1888E+00	-4.6275E-01	2.9937E-01					
A10 =	-1.1480E+01	-4.2607E-01	3.1380E-01	-1.1921E-01					
A12 =	-4.4740E+00	-5.1720E-01	-1.2912E-01	2.8364E-02					
A14 =	1.2594E÷01	5.0722E-01	2.9275E-02	-3.7104E-03					
A16 =	-5.4160E+00	-1.2485E-01	-2.8533E-03	2.0238E-04					

第五實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表十四中所列。

	表	十四						
第五實施例								
f [mm]	2.24	12/13	-0.93					
Fno	2.51	[5][4]	1.12					
HFOV [deg.]	44.2	<b>7/</b> 13	-1.30					
VI	17.8	Td [mm]	3.150					
CT2/(CT1+CT3+CT4)	1.25	ΣCT/Td	0.85					
(R3+R4)/(R3-R4)	0.61	Td/tan(HFOV) [mm]	3.24					
Øfi –	-0.16	FOV [deg.]	88.4					

# 《第六實施例》

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申請案號: 102139029

本發明第六實施例請參閱第六 A 圖,第六實施例的像差曲線請參閱第六 B 圖。第六實施例的取像裝置包含影像拾取系統透鏡

組與一電子感光元件(670),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(610),其材質為塑膠,其物側面(611)於近光軸處為凸面,其像側面(612)於近光軸處為凸面,且其兩面皆為非球面;

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- 一具正屈折力的第二透鏡(620),其材質為塑膠,其物側面(621)於近光軸處為凹面,其像側面(622)於近光軸處為凸面,且 其兩面皆為非球面;
- 一具負屈折力的第三透鏡(630),其材質為塑膠,其物側面(631)於近光軸處為凹面,其像側面(632)於近光軸處為凸面,且 其兩面皆為非球面;及
- 一具正屈折力的第四透鏡(640),其材質為塑膠,其物側面(641)於近光軸處為凸面,其像側面(642)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(642)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(600),置於該第一透鏡(610)與該第二透鏡(620)間;另包含有一紅外線濾除濾光元件(650)置於該第四透鏡(640)與一成像面(660)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(670)設置於該成像面(660)上。

第六實施例詳細的光學數據如表十五所示,其非球面數據如表十六所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV定義為最大視角的一半。

			表-	<b>十五</b>		,		
			(第六)	了施例)				
		<u>f = 1.27 n</u>	nm, Fno = 2.	10, HFOV =	= 44.4 deg.			
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	2.393	ASP	0.280	塑膠	1.544	55.9	3.85
2		-16.057	ASP	0.017				
3	光圈	平面		0.044				



12	成像面	平面						
11	<b>適光</b> 片	平面		0.073				
10	紅外線濾除	平面		0.175	玻璃	1.517	64.2	-
9		2.521	ASP	0.400				
8	第四透鏡	0.639	ASP	0.522	塑膠	1.530	55.8	1.47
7	·	-0.594	ASP	0.030				
6	第三透鏡	-0.246	ASP	0.240	塑膠	1.639	23.5	-0.90
5		-0.468	ASP	0.121				
4	第二透鏡	-30.373	ASP	0.755	塑膠	1.544	55.9	0.87

		<b>表</b> 十六								
	非球面係數									
表面 #	. 1	2	4	5						
k =	1.7241E+00	-8.9754E+01	-9.0000E+01	-7.5923E-01						
A4 =	2.1410E-01	1.4516E+00	1.5168E-01	-5.4982E-01						
A6 =	-2.3810E-01	-1.0826E+01	4.8929E+00	2.0791E+00						
A8 =	2.3555E+01	1.9495E+02	-3.2116E+01	8.2787E-01						
A10 =	-2.5034E+02	-5.1780E+02	-2.6801E+03	-1.4893E+02						
A12 =	1.4357E+03	-5.7593E+04	4.6579E+04	1.0534E+03						
A14 =	-4.2381E+03	9.2351E+05	-3.3256E+05	-3.0936E+03						
A16 =	4.9589E+03	-4.2045E+06	9.0327E+05	3.3098E+03						
表面 #	6	7	8	9						
k =	-9.9704E-01	-3.7851E+00	-7.3474E-01	-2.0751E+00						
A4 =	2.9255E+00	-1.3600E+00	-1.2133E+00	1.8260E+00						
A6 =	-2.4852E+00	5.5927E+00	3.0817E+00	-5.9653E+00						
A8 =	-5.7718E+01	-1.8755E+01	-1.0034E+01	9.6816E+00						
A10 =	6.7135E+02	7.3016E+01	1.9498E+01	-9.2466E+00						
A12 =	-3.0733E+03	-1.6937E+02	-2.1549E+01	5.1894E+00						
A14=	6.6780E+03	1.9522E+02	1.2590E+01	-1.5760E+00						
A16=	-5.6393E+03	-8.6932E+01	-3.0510E+00	1.9769E-01						

第六實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表十七中所列。

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	表十t		
	第六實別	<b></b>	
f (mm)	1.27	f2/f3	-0.97
Fno	2.10	f/f4	0.86
HFOV [deg.]	44.4	f/f3	-1.41

VI	55.9	Td [mm]	2.009
CT2/(CT1+CT3+CT4)	0.72	ΣCT/Td	0.89
(R3+R4)/(R3-R4)	1.03	Td/tan(HFOV) [mm]	2.05
ฮก	0.33	FOV [deg.]	88.8

#### 《第七實施例》

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申請案號:102139029

本發明第七實施例請參閱第七 A 圖,第一實施例的像差曲線請參閱第七 B 圖。第七實施例的取像裝置包含影像拾取系統透鏡組與一電子感光元件(770),該影像拾取系統透鏡組主要由四片具屈折力的透鏡構成,由物側至像側依序包含:

- 一具正屈折力的第一透鏡(710),其材質為塑膠,其物側面(711)於近光軸處為凸面,其像側面(712)於近光軸處為凹面,且其兩面皆為非球面;
- 一具正屈折力的第二透鏡(720),其材質為塑膠,其物側面 (721)於近光軸處為凹面,其像側面(722)於近光軸處為凸面,且 其兩面皆為非球面;
  - 一具負屈折力的第三透鏡(730),其材質為塑膠,其物側面(731)於近光軸處為凹面,其像側面(732)於近光軸處為凸面,且 其兩面皆為非球面;及
  - 一具正屈折力的第四透鏡(740),其材質為塑膠,其物側面(741)於近光軸處為凸面,其像側面(742)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(742)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(700),置於一 20 被攝物與該第一透鏡(710)間:另包含有一紅外線濾除濾光元件 (750)置於該第四透鏡(740)與一成像面(760)間,其材質為玻璃且 不影響焦距。

其中,該電子感光元件(770)設置於該成像面(760)上。

第七實施例詳細的光學數據如表十八所示,其非球面數據如 25 表十九所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義為最大視角的一半。

			<del>稷</del> ·	十八				
			(第七)	度施例)				,
		<u>f = 1.57 i</u>	mm, Fno = 2	.05, HFOV =	= 48,5 deg.			<del></del>
<b>表面</b> #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				****
1	光图	平面		-0.052			·	
2	第一透鏡	1.142	ASP	0.279	塑膠	1.544	55.9	2.84
3		4.008	ASP	0.159				
4	第二透鏡	-4.075	ASP	0.614	塑膠	1.544	55.9	1.24
5		-0.608	ASP	0.142		7		
6	第三透鏡	-0.255	ASP	0.230	塑膠	1.634	23.8	-1.37
7		-0.487	ASP	0.030				
8	第四透鏡	0.636	ASP	0.414	塑膠	1.535	55.7	2.35
9		0.998	ASP	0.500				
10	紅外線遊除	平面		0.175	玻璃	1.517	64.2	_
11	濾光片	平面		0.141				
12	成像面	平面		•				

		表十九								
	非球面係數									
表面 #	2	3	4	5						
k =	-5.4318E-01	6.9324E+01	6.0179E+01	-4.8138E-01						
A4 =	1.1275E-01	-3.4138E-01	-6.6571E-01	-8.5384E-02						
A6 =	-1.4350E+00	-2.7321E+00	4.9846E-01	-6.6518E-01						
A8 =	6.0529E+00	2.0740E+01	-4.5807E+00	-2.1554E-01						
A10 =	4.7148E+01	-7.0776E+01	-1.7027E+02	-7.9977E+00						
A12 =	-1.4571E+02	-1.4998E+03	1.2130E+03	2.5638E+01						
A14=	-3.8164E+03	1.2389E+04	-4.4615E+03	-4.3167E+01						
A16=	1.5882E+04	-2.9058E+04	6.2425E+03	7.2938E+01						
表面#	6	7	8	9						
k =	-1.1103E+00	-3.0258E+00	-9.3042E-01	-5.1455E+00						
A4 =	5.4423E+00	4.5345E-01	-7.7223E-01	7.0200E-01						
A6 =	-3.5666E+01	-4.9768E÷00	9.4468E-01	-1.5850E+00						
A8 =	1.3446E+02	1.9752E+01	-1.3669E+00	1.7028E+00						
A10 =	-2.5131E+02	-4.2912E+01	1.1409E+00	-1.1082E+00						
A12 =	-7.3665E+01	5.3544E+01	-5.2307E-01	4.3302E-01						
A14=	1.1117E+03	-3.5702E+01	1.2365E-01	-9.2838E-02						
A16 =	-1.2600E+03	1.0063E+01	-1.1645E-02	8.3092E-03						

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第七實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表二十中所列。

	表	二十	
	第七	實施例	
f [mm]	1.57	f2/f3	-0.91
Fno	2.05	67f4	0.67
HFOV [deg.]	48.5	763	-1.15
VI	55.9	Td [mm]	1.868
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.82
(R3+R4)/(R3-R4)	1.35	Td/tan(HFOV) [mm]	1.65
<i>ប</i> ក	0.55	FOV [deg.]	97.0

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#### 《第八實施例》

本發明第八實施例請參閱第八 A 圖,第八實施例的像差曲線 請參閱第八 B 圖。第八實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(870),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

- 一具正屈折力的第一透鏡(810),其材質為塑膠,其物側面(811)於近光軸處為凸面,其像側面(812)於近光軸處為凹面,且其兩面皆為非球面;
- 一具正屈折力的第二透鏡(820),其材質為塑膠,其物側面 15 (821)於近光軸處為凹面,其像側面(822)於近光軸處為凸面,且 其兩面皆為非球面;
  - 一具負屈折力的第三透鏡(830),其材質為塑膠,其物側面(831)於近光軸處為凹面,其像側面(832)於近光軸處為凸面,且 其兩面皆為非球面;及
- 20 一具正屈折力的第四透鏡(840),其材質為塑膠,其物側面 (841)於近光軸處為凸面,其像側面(842)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(842)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(800),置於該第一透鏡(810)與該第二透鏡(820)間;另包含有一紅外線濾除濾光元件(850)置於該第四透鏡(840)與一成像面(860)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(870)設置於該成像面(860)上。

第八實施例詳細的光學數據如表二十一所示,其非球面數據如表二十二所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

				-+-				
			(第八)	實施例)				·
		<u>f= 1.68</u>	mm, Fno = 2	.10, HFOV :	= 46,0 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.787	ASP	0.278	塑膠	1.544	55.9	3.81
2		12.133	ASP	0.022		,		
3	光图	平面		0.145				·····
4	第二透鏡	-3.839	ASP	0.668	塑膠	1.544	55.9	1.38
5		-0.668	ASP	0.194				······································
6	第三透鏡	-0.273	ASP	0.230	塑膠	1.639	23.5	-1.18
7		-0.569	ASP	0.030				***
8	第四透鏡	0.784	ASP	0.496	塑膠	1.530	55.8	1.65
9		5.992	ASP	0.400				
10	紅外線遮除	平面		0.175	玻璃	1.517	64.2	-
11	<b>適光</b> 片	平面		0.472				
12	成像面	平面		•				

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<b>表二十二</b>										
	非球面係數									
表面#	1	2	4	5						
k =	-1.3232E+00	5.3151E+01	5.1693E+01	-5.9308E-01						
A4 =	1.6281E-02	-1.2122E-02	-2.5602E-01	-1.1508E-01						
A6 =	1.5823E-01	-1.1940E+00	-1.0332E+00	-6.8787E-01						
A8 =	5.9941E-01	1.2093E+01	1.0464E+01	-9.7964E-02						
A10 =	-1.3812E+01	-2.0003E+01	-1.9940E+02	-6.2734E+00						
A12 =	4.5317E+01	-1.4998E+03	1.2130E+03	2.8529E+01						

A14 =	-4.4460E+01	1.2389E+04	-4.4615E+03	-4.4589E+01
A16 =	-4.7734E+01	-2.9058E+04	6.2425E+03	2.7908E+01
表面#	6	7	8	9
k =	-1.0578E+00	-3.0032E+00	-8.6121E-01	5.6610E+00
A4 =	4.0391E+00	9.4553E-02	-6.6716E-01	7.7788E-01
A6 =	-2.6571E+01	-4.4170E+00	1.1395E+00	-1.2944E+00
A8 =	1.2417E+02	1.9085E+01	-1.7698E+00	1.0967E÷00
A10 =	-3.9394E+02 .	-4.1568E+01	1.6239E÷00	-5.7605E-01
A12 =	8.2748E+02	5.5376E+01	-8.6944E-01	1.8609E-01
A14 =	-9.7331E+02	-4.1902E+01	2.5418E-01	-3.3617E-02
A16=	4.7213E+02	1.3653E+01	-3.1838E-02	2.5144E-03

第八實施例非球面曲線方程式的表示如同第一實施例的形 式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十三中所列。

·	表二	十三							
	第八實施例								
f [mm]	1.68	f2/f3	-1.17						
Fno	2.10	E/f4	1.02						
HFOV [deg.]	46.0	f/f3	-1.42						
VI	55.9	Td [mm]	2.063						
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.81						
(R3+R4)/(R3-R4)	1.42	Td/tan(HFOV) [mm]	1.99						
ชก	0.44	FOV [deg.]	92.0						

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#### 《第九實施例》

本發明第九實施例請參閱第九A圖,第九實施例的像差曲線 請參閱第九B圖。第一實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(970),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

- 一具正屈折力的第一透鏡(910),其材質為塑膠,其物側面 (911)於近光軸處為凸面,其像側面(912)於近光軸處為凸面,且其 兩面皆為非球面;
- 一具正屈折力的第二透鏡(920),其材質為塑膠,其物側面 15 (921)於近光軸處為凸面,其像側面(922)於近光軸處為凸面,且

#### 其兩面皆為非球面;

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一具負屈折力的第三透鏡(930),其材質為塑膠,其物側面(931)於近光軸處為凹面,其像側面(932)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(940),其材質為塑膠,其物側面(941)於近光軸處為凸面,其像側面(942)於近光軸處為凹面,其兩面皆為非球面,且其像側面(942)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(900),置於該第一透鏡(910)與該第二透鏡(920)間;另包含有一紅外線濾除濾光元件(950)置於該第四透鏡(940)與一成像面(960)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(970)設置於該成像面(960)上。

第九實施例詳細的光學數據如表二十四所示,其非球面數據如表二十五所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

			表二	十四		······································	·	
			(第九)	實施例)	······································			
		<u>f = 0.92 m</u>	m, Fno = 2	45, HFOV	= 43.9 deg.			
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				<b>V</b>
1	第一透鏡	100.000	ASP	0.205	塑膠	1.633	23.4	13.12
2		-9.046	ASP	0.017				
3	光圈	平面		0.024				
4	第二透鏡	1.695	ASP	0.475	塑膠	1.544	55.9	0.54
5		-0.319	ASP	0.100				
6	第三透鏡	-0.148	ASP	0.160	塑膠	1.634	23.8	-0.65
7	•	-0.329	ASP	0.030				
8	第四透鏡	0.595	ASP	0.239	塑膠	1.530	55.8	1.28
9		4.109	ASP	0.300				
10	紅外線濾除	平面		0.145	玻璃	1.517	64.2	-
11	<b>適光片</b>	平面		0.151				···········
12	成像面	平面		-				
主:参考	波長為 d-line	587.6 nm	····	<u> </u>	1		<u> </u>	····

		表二十五		-					
	非球面係數								
表面 #	1	2	4	5					
k =	-9.0000E+01	9.0000E+01	3.3243E+01	-6.6437E-01					
A4 =	2.5656E-01	2.4894E+00	-1.9077E+00	-1.5093E+00					
A6 =	-1.0613E+00	-9.5530E+01	-1.3506E+01	4.3096E+00					
A8 =	1.6769E+02	3.0126E+03	1.0928E+01	1.6065E+02					
A10 =	-3.7307E+03	-2.3016E+04	-4.4021E+04	-2.9203E+03					
A12=	3.9786E+04	-1.5960E+06	1.2908E+06	2.9181E+04					
A14=	-2.1485E+05	4.6819E+07	-1.6860E+07	-1.5683E+05					
A16=	4.5990E+05	-3.8994E+08	8.3772E+07	3.0696E+05					
表面#	6	7	8	9					
k =	-1.0921E+00	-2.4247E+00	-6.0015E-01	3.3921E+01					
A4 =	8.8579E+00	-1.7457E+00	-1.8642E+00	3.4965E+00					
A6 =	-9.7201E+00	2.7059E+01	4.2816E+00	-1.7965E+01					
A8 =	-4.6210E+02	-1.6609E+02	-3.6842E+01	3.3243E+01					
A10=	1.0079E+04	1.0699E+03	9.4802E+01	-3.1178E+01					
A12=	-8.5169E+04	-4.7330E+03	-1.9140E+02	1.8452E+01					
A14=	3.3855E+05	1.0605E+04	3.6755E+02	-3.7397E+01					
A16=	-5.2300E+05	-7.7191E+03	-9.3365E+02	3.7762E+01					

第九實施例非球面曲線方程式的表示如同第一實施例的形 式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十六中所列。

	表二	十六						
第九質施例								
f [mm]	0.92	12/13	-0.83					
Fno	2.45	[f/f4]	0.72					
HFOV [deg.]	43.9	f/t3	-1.42					
Vì	23.4	Td (mm)	1.250					
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.86					
(R3+R4)/(R3-R4)	0.68	Td/tan(HFOV) [mm]	1.30					
<b>7/</b> 1	0.07	FOV [deg.]	87.8					

# 《第十實施例》

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本發明第十實施例請參閱第十A圖,第十實施例的像差曲線 請參閱第十B圖·第一實施例的取像裝置包含影像拾取系統透鏡

- 組與一電子感光元件(1070),該影像拾取系統透鏡組主要由四片 具屈折力的透鏡構成,由物側至像側依序包含:
- 一具正屈折力的第一透鏡(1010),其材質為塑膠,其物側面(1011)於近光軸處為凸面,其像側面(1012)於近光軸處為凹面,且 其兩面皆為非球面;

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- 一具正屈折力的第二透鏡(1020),其材質為塑膠,其物側面(1021)於近光軸處為凹面,其像側面(1022)於近光軸處為凸面, 且其兩面皆為非球面;
- 一具負屈折力的第三透鏡(1030),其材質為塑膠,其物側面 10 (1031)於近光軸處為凹面,其像側面(1032)於近光軸處為凸面, 且其兩面皆為非球面;及
  - 一具正屈折力的第四透鏡(1040),其材質為塑膠,其物側面(1041)於近光軸處為凸面,其像側面(1042)於近光軸處為凹面, 其兩面皆為非球面,且其像側面(1042)於離軸處具有至少一凸面;
  - 其中,該影像拾取系統透鏡組另設置有一光圈(1000),置於一被攝物與該第一透鏡(1010)間;另包含有一紅外線濾除濾光元件(1050)置於該第四透鏡(1040)與一成像面(1060)間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(1070)設置於該成像面(1060)上。

第十實施例詳細的光學數據如表二十七所示,其非球面數據如表二十八所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

			表二	十七				
			(第十)	官施例)				
		<u>f = 1.80</u> ;	mm, Fno = 2	.12, HFOV =	47.2 deg.	•		***************************************
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限		1		
1	光圈	平面		-0.060				
2	第一透鏡	1.246	ASP	0.289	塑膠	1.544	55.9	2.97
3		5.018	ASP	0.191				

4	第二透鏡	-3.749	ASP	0.593	塑膠	1.544	55.9	1.57
5		-0.733	ASP	0.156				·
6	第三透鏡	-0.288	ASP	0.248	塑膠	1.634	23.8	-1.33
7		-0.584	ASP	0.030				
8	第四透鏡	0.704	ASP	0.601	塑膠	1.535	55.7	2.05
9		1.382	ASP	0.500				
10	紅外線遊除	平面		0.210	玻璃	1.517	64.2	-
11	<b>泡光</b> 片	平面		0.198				
12	成像面	平面		-				

第9面有效半徑為 1.676 mm

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		表二十八								
	非球面係數									
表面#	2	3	4	5						
k =	-5.0585E-01	9.0000E+01	3.6143E+01 ·	-3.9805E-01						
A4 =	8.6099E-02	-2.2970E-01	-4.8540E-01	-1.5034E-01						
A6 =	-9.1382E-01	-1.8900E+00	2.7508E-01	-5.1276E-01						
A8 =	1.9706E+00	1.1233E+01	-2.0152E+00	-1.5742E-01						
A10 =	1.9492E+01	-3.0654E+01	-6.3534E+01	-3.0117E+00						
A12 =	-3.5519E+01	-4.4967E+02	3.6120E+02	7.3424E+00						
A14 =	-8.0910E+02	2.9681E+03	-1.0702E+03	-1.0241E+01						
A16 =	2.4600E+03	-5.5960E+03	1.2022E+03	1.7746E+01						
表面#	6	7	8	9						
k = .	-1.1070E+00	-2.9894E+00	-9.3316E-01	-5.2865E+00						
A3 =			-1.4739E-01	5.0831E-01						
A4 =	4.3809E+00	4.3352E-01	-3.5412E+00	2.6512E+00						
A5 =			2.4672E-02	1.3099E-01						
A6 =	-2.6437E+01	-3.7903E+00	1.0303E+01	-3.1255E+01						
A7 =			3.7082E-02	2.0652E-01						
A8 =	9.1296E+01	1.0965E+01	-3.1616E+01	. 1.1148E+02						
A9 =			-2.2687E-03	-9.0797E-01						
A10 =	-1.5853E+02	-1.4675E+01	6.3626E+01	-2.2327E+02						
A11 =			-2.3794E-03	3.6058E-01						
A12 =	8.3141E+00	7.7310E+00 .	-7.5604E+01	2.6201E+02						
A13 =			8.0966E-03	1.7201E-01						
A14 =	3.8963E+02	1.2159E+00	4.7652E+01	-1.7041E+02						
A15 =			-5.5857E-02	1.0396E-01						
A16=	-3.9976E+02	-1.8447E+00	-1.2153E+01	4.7523E÷01						
		1	I	<u> </u>						

第十實施例非球面曲線方程式的表示如同第一實施例的形

式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個關係式的數值係如表二十六中所列。

	表二	<b>二十九</b>	
	第十	實施例	
f (mm)	1.80	f2/f3	-1.18
Fno	2.12	[6/f4]	0.88
HFOV [deg.]	47.2	f/f3	-1.35
VI	55.9	Td [mm]	2.108
CT2/(CT1+CT3+CT4)	0.52	ΣCT/Td	0.82
(R3+R4)/(R3-R4)	1.49	Td/tan(HFOV) [mm]	1.95
ชก	0.61	FOV [deg.]	94.4

表一至表二十九所示為本發明的影像拾取系統透鏡組實 施例的不同數值變化表,然本發明各個實施例的數值變化皆屬 實驗所得,即使使用不同數值,相同結構的產品仍應屬於本發 明的保護範疇,故以上的說明所描述的及圖式僅做為例示性, 非用以限制本發明的申請專利範圍。

### 10 【符號說明】

光圈 100、200、300、400、500、600、700、800、900、 1000

第一透鏡 110、210、310、410、510、610、710、810、910、1010

15 物側面 111、211、311、411、511、611、711、811、911、

像側面 112、212、312、412、512、612、712、812、912、 1012

第二透鏡 120、220、320、420、520、620、720、820、920、.

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1011

物側面 121、221、321、421、521、621、721、821、921、

1021

像側面 122、222、322、422、522、622、722、822、922、

1022

第三透鏡 130、230、330、430、530、630、730、830、930、

5 1030

> 物側面 131 · 231 · 331 · 431 · 531 · 631 · 731 · 831 · 931 ·

1031

像側面 132 \ 322 \ 332 \ 432 \ 532 \ 632 \ 732 \ 832 \ 932 \

1032

10 第四透鏡 140、240、340、440、540、640、740、840、940、

1040

物側面 141 · 241 · 341 · 441 · 541 · 641 · 741 · 841 · 941 ·

1041

像側面 142、422、342、442、542、642、742、842、942、

15 1042

> 紅外線濾除濾光元件 150、250、350、450、550、650、 750 \ 850 \ 950 \ 1050

> 成像面 160、260、360、460、560、660、760、860、960、 1060

20 電子感光元件 170、270、370、470、570、670、770、870、 970 - 1070

> 取像裝置 1101

> 智慧型手機 1110

> 平板電腦 1120

25 可穿戴式設備 1130

申請案號:102139029

影像拾取系統透鏡組的焦距為f 第一诱鏡的焦距為 fl

第二透鏡的焦距為 f2

第三透鏡的焦距為 的

第四透鏡的焦距為 f4

第一透鏡的色散係數為 VI

第一透鏡物側面至第四透鏡像側面於光軸上的距離為 Td

第一透鏡於光軸上的厚度為 CT1

第二透鏡於光軸上的厚度為 CT2

第三透鏡於光軸上的厚度為 CT3

第四透鏡於光軸上的厚度為 CT4

10 第一透鏡、第二透鏡、第三透鏡、及第四透鏡於光軸上的厚度 的總和為∑CT

第二透鏡物側面的曲率半徑為 R3

第二透鏡像側面的曲率半徑為 R4

影像拾取系統透鏡組的光圈值為 Fno

15 影像拾取系統透鏡組的最大視角為 FOV

影像拾取系統透鏡組中最大視角的一半為 HFOV

# 【生物材料寄存】

國內寄存資訊【請依寄存機構、日期、號碼順序註記】

20 無

申請案號:102139029

國外寄存資訊【請依寄存國家、機構、日期、號碼順序註記】

無

# 申請專利範圍

- 1. 一種影像拾取系統透鏡組,由物側至像側依序包含:
  - 一具屈折力的第一透鏡;

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- 一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;
- 一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其 像側面於近光軸處為凸面;及
- 一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係式:

0.5 mm < Td < 3.2 mm;

-1.0 mm < Td / tan(HFOV) < 3.75 mm;

|f / f4| < 1.20; 及

f2 / f3 < -0.65 •

- 2. 如申請專利範圍第 1 項所述的影像拾取系統透鏡組,其中該第20 四透鏡的物側面於近光軸處為凸面。
  - 3. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 fl,係滿足下列關係式:

-0.25 < f / f1 < 0.75

25 4. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,係滿足下列關係式:

 $0.8 \text{ mm} < \text{Td} < 2.5 \text{ mm} \cdot$ 

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- 5. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的光圈值為 Fno,係滿足下列關係式:
  - $1.4 < Fno \le 2.25 \circ$
- 6. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,該第二透鏡物側面的曲率半徑為 R3,該第二透鏡像側面的曲率半徑為 R4,係滿足下列關係式:
  - 0.5 < (R3+R4) / (R3-R4) < 2.5
- 7. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的焦距為 f,係滿足下列關係式:
- 10  $0.5 \text{ mm} < f < 2.0 \text{ mm} \circ$

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- 8. 如申請專利範圍第 1 項所述的影像拾取系統透鏡組,其中該第 一透鏡物側面於近光軸處為凸面。
- 9. 如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,係滿足下列關係式:
  - 1.2 mm < Td / tan(HFOV) < 2.75 mm
- 10.如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第一透鏡、該第二透鏡、該第三透鏡、及該第四透鏡於光軸上之厚度的總合為∑CT,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,係滿足下列關係式:
  - $0.80 < \sum CT / Td < 0.95$ .
- 11.如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第 一透鏡的色散係數為 V1,係滿足下列關係式:
- 25 45 < V1

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12.如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於光軸上

的厚度為 CT4, 係滿足下列關係式:

0.65 < CT2 / (CT1+CT3+CT4) < 2.0

- 13.一種取像裝置,包含如申請專利範圍第 1 項所述的影像拾取系統透鏡組及一電子感光元件。
- 5 14.一種可攜裝置,包含如申請專利範圍第 13 項所述的取像裝置。
  - 15.一種影像拾取系統透鏡組,由物側至像側依序包含:
    - 一具屈折力的第一透鏡:
      - 一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;
    - 一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其 像側面於近光軸處為凸面;及
  - 一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離 5 為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第三透鏡的焦距為 f3,係滿足下列關係式:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td / tan(HFOV) < 3.75 mm;

|f / f4| < 1.20; 及

-2.0 < f / f3 < -0.95

16.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該第一透鏡的色散係數為 V1,係滿足下列關係式:

45 < V1 •

25 17.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 fl,係滿足下列關係式:

-0.25 < f/f1 < 0.75 •

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- 18.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的最大視角為 FOV,係滿足下列關係式:
  - 80 度 < FOV < 110 度。
- 19.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,係滿足下列關係式:
  - 0.8 mm < Td < 2.5 mm •
- 20.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該第二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係式:

 $f2 / f3 < -0.75 \circ$ 

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- 21.一種影像拾取系統透鏡組,由物側至像側依序包含:
  - 一具屈折力的第一透鏡:
  - 一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;
- 15 一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其 像側面於近光軸處為凸面;及
  - 一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該影像拾取系統透鏡組的光圈值為 Fno,係滿足下列關係式:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td / tan(HFOV) < 3.75 mm;

|f / f4| < 1.20; 及

 $1.40 < Fno \le 2.25$ 

22.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第

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二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係式:

 $f2 / f3 < -0.65 \circ$ 

23. 如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第一透鏡的色散係數為 VI,係滿足下列關係式:

45 < V1 •

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24.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第一透鏡具正屈折力,該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 fl,係滿足下列關係式:

0.25 < f / f1 < 0.75

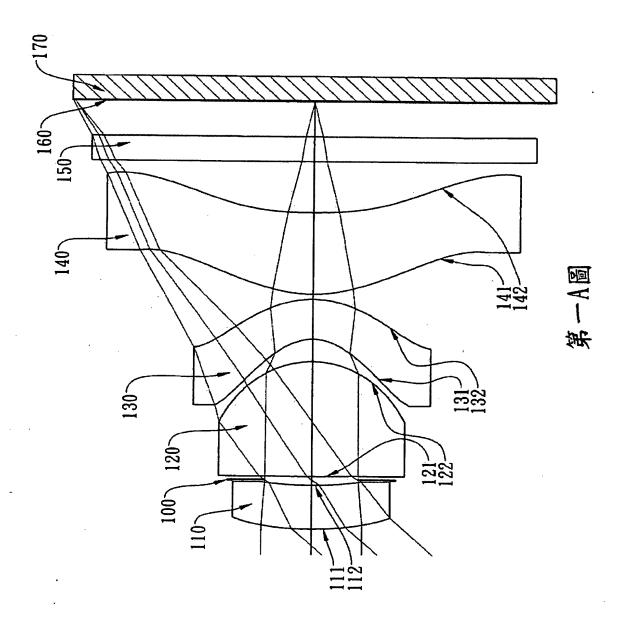
25.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的最大視角為 FOV,係滿足下列關係式:

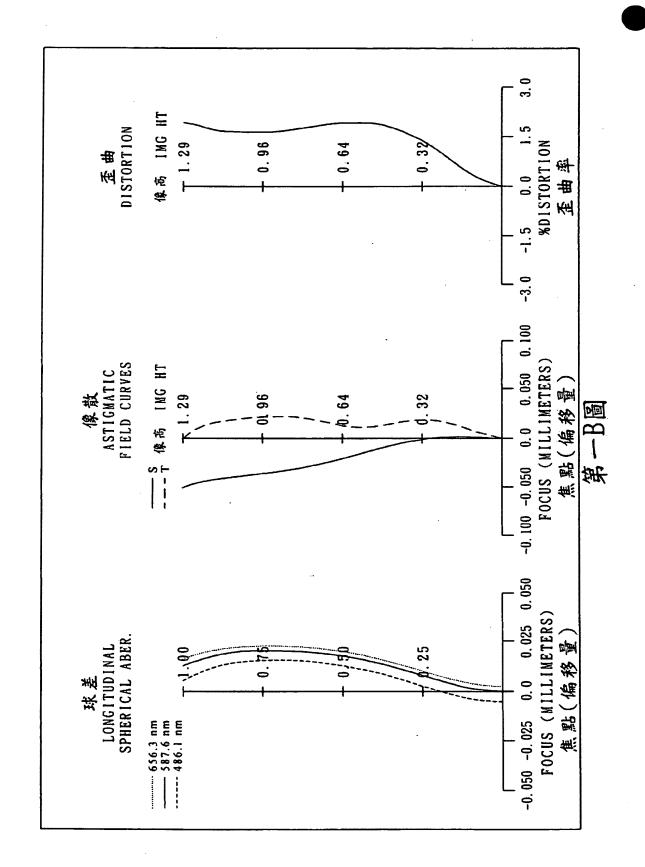
80度 < FOV < 110度。

26.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於光軸上的厚度為 CT4,係滿足下列關係式:

0.65 < CT2 / (CT1+CT3+CT4) < 2.0

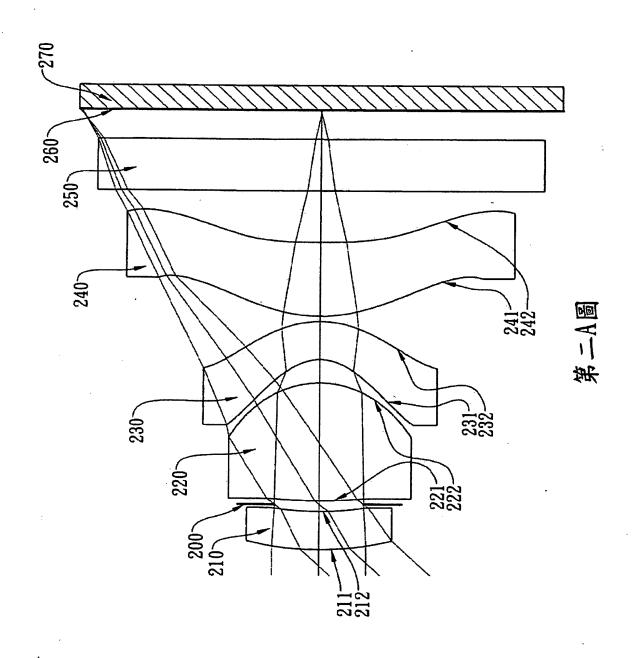
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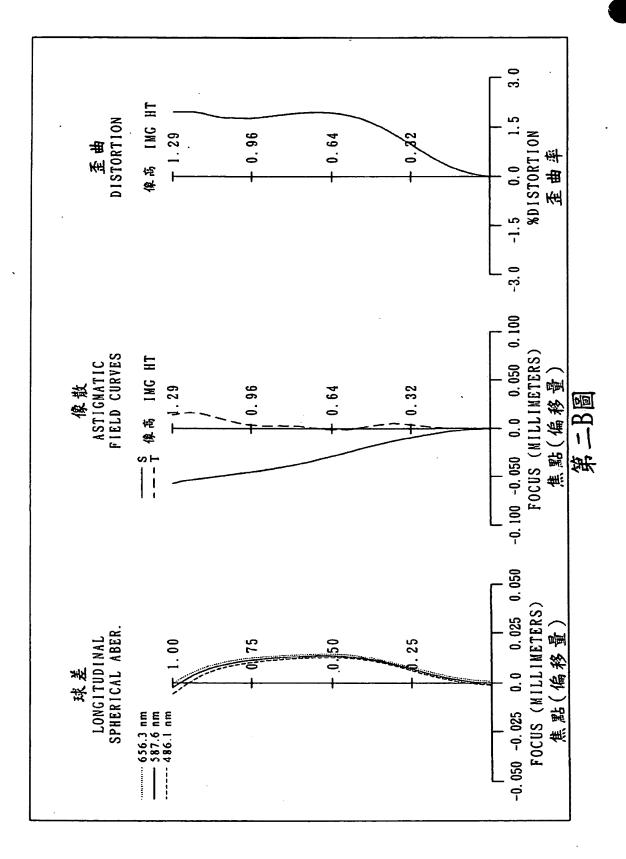




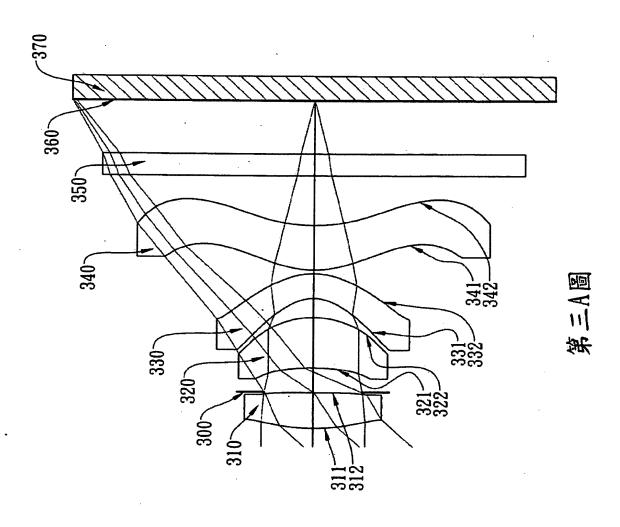
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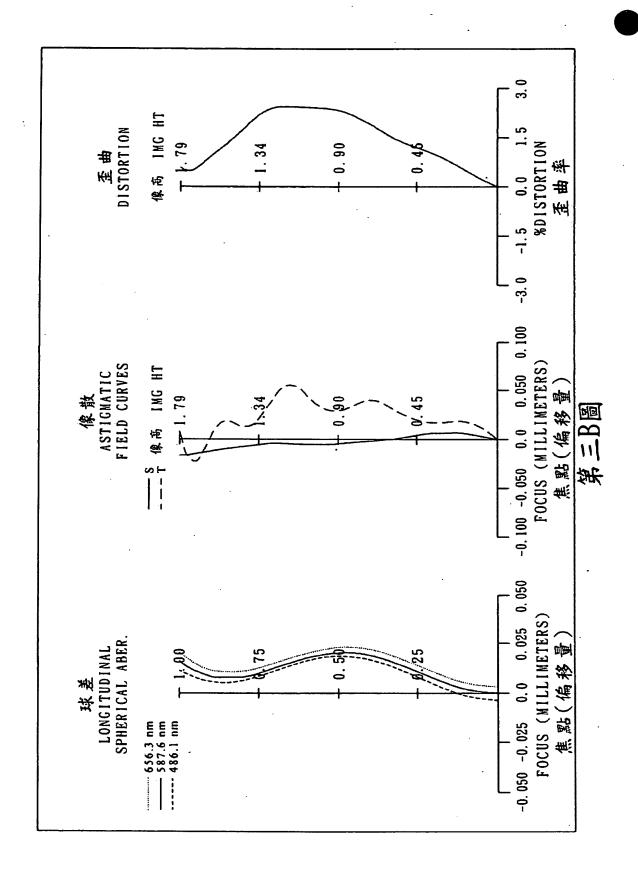
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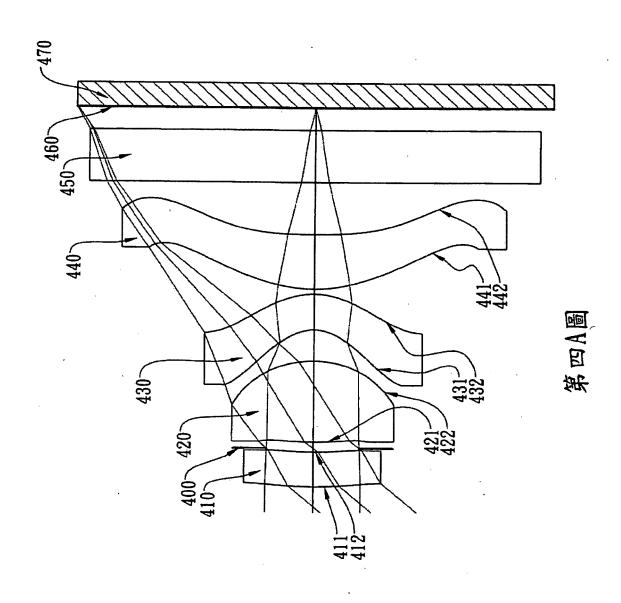


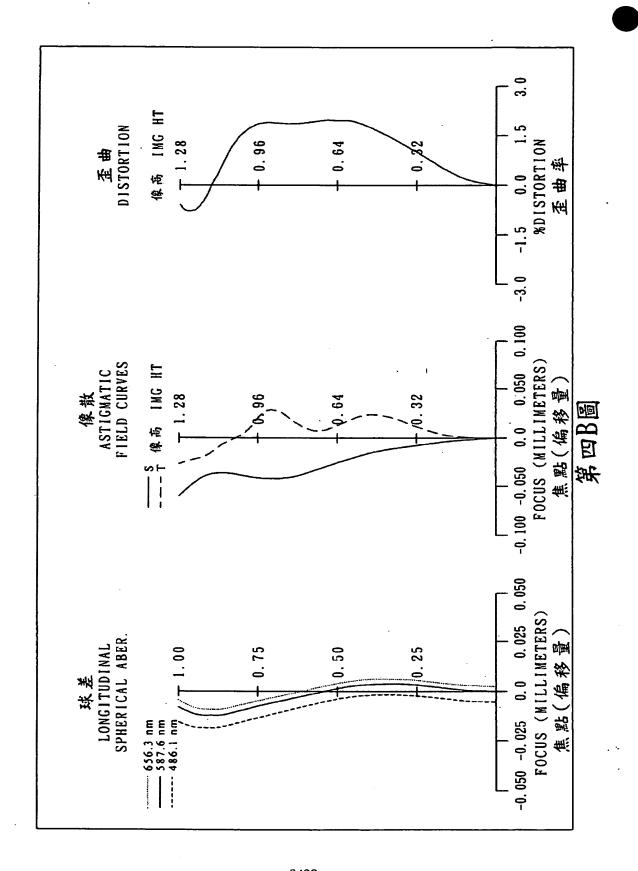
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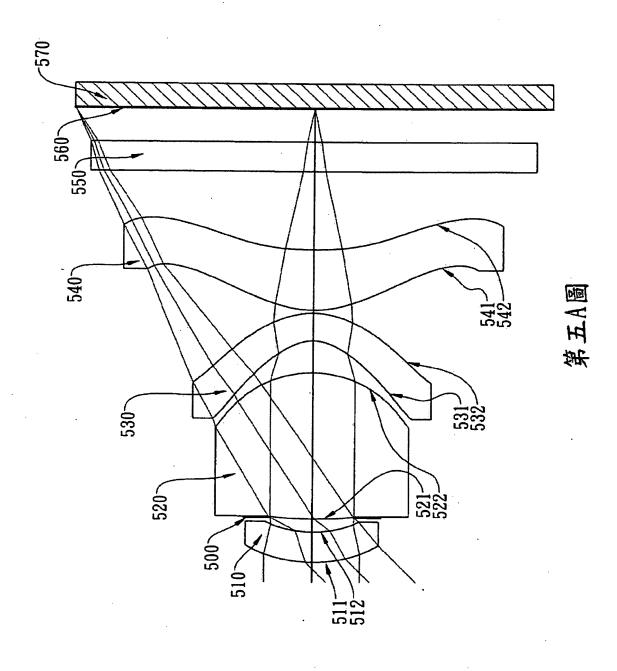


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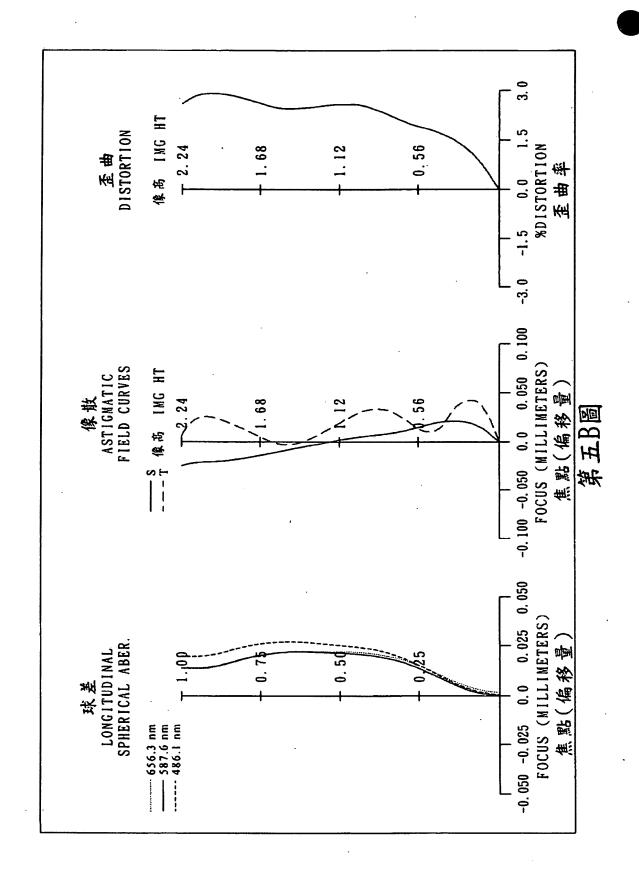


8/23



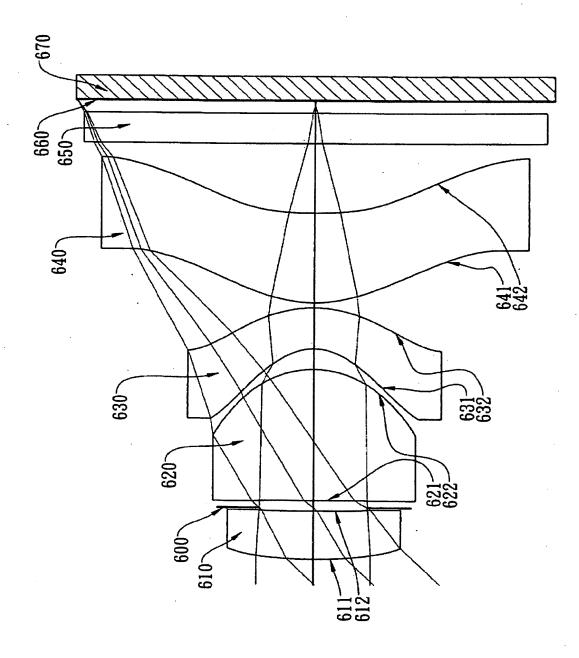
9/23

申請案號: 102139029



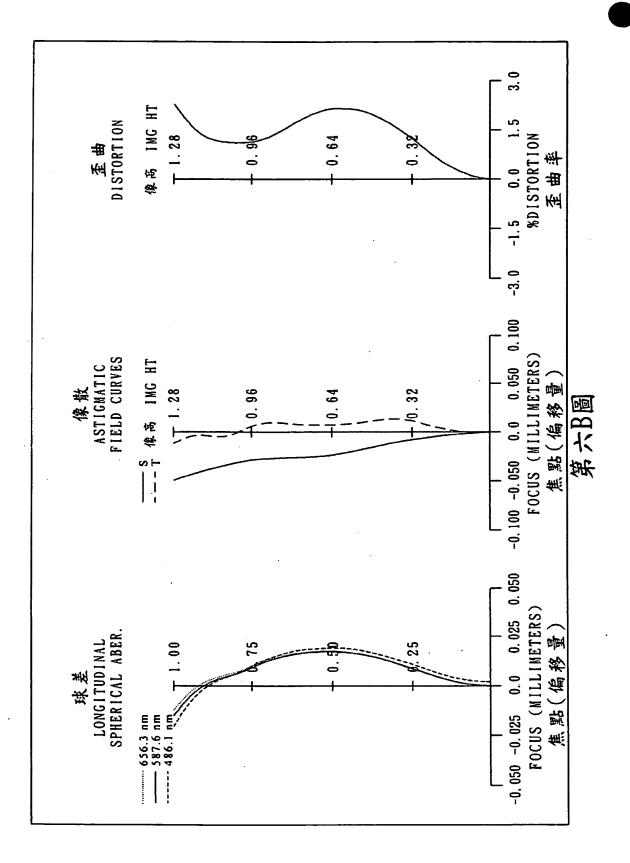
10/23

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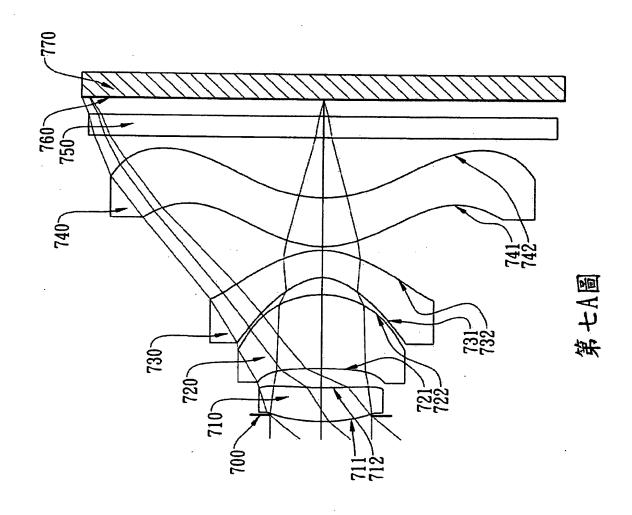
第六人圖

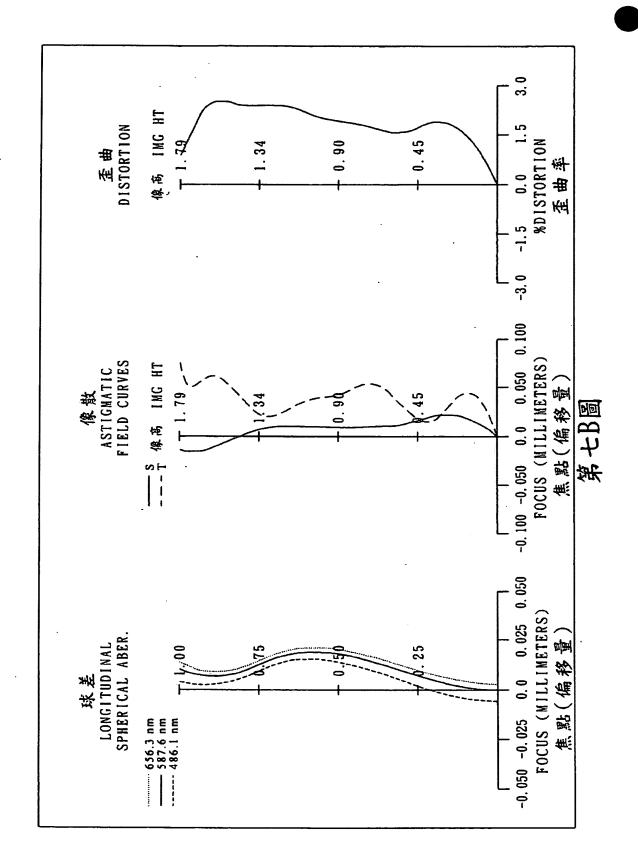
申請案號: 102139029



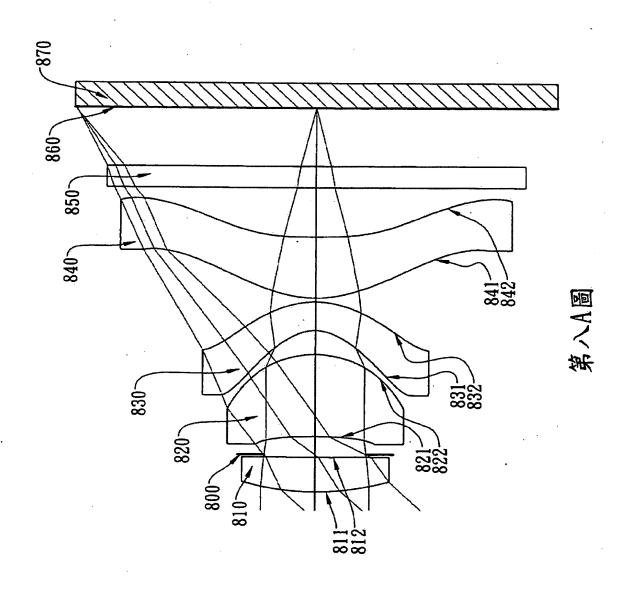
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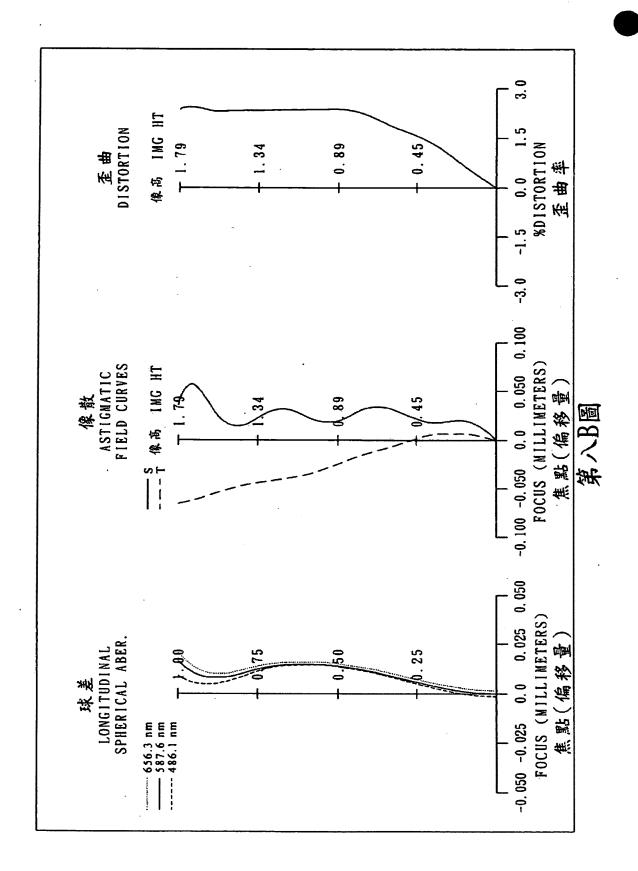
ز. پ



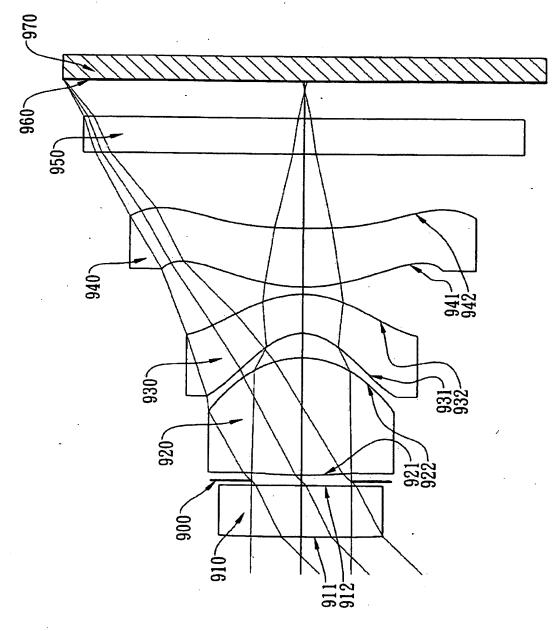


14/23

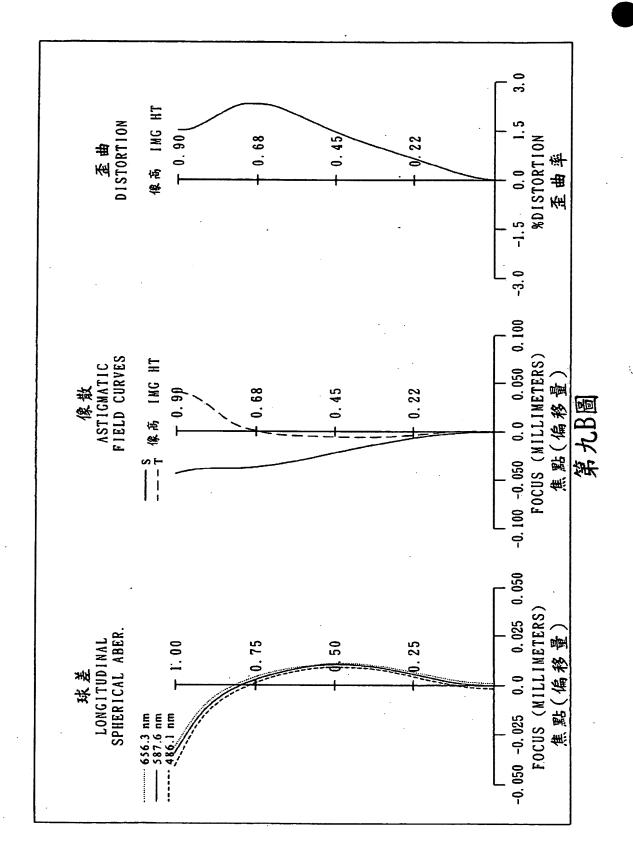


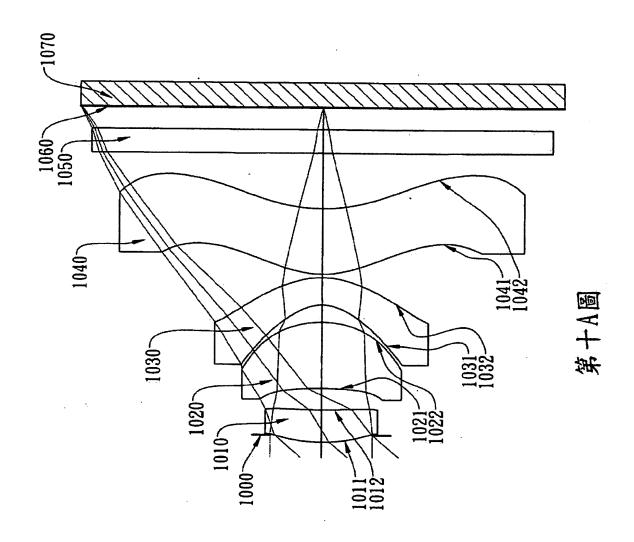


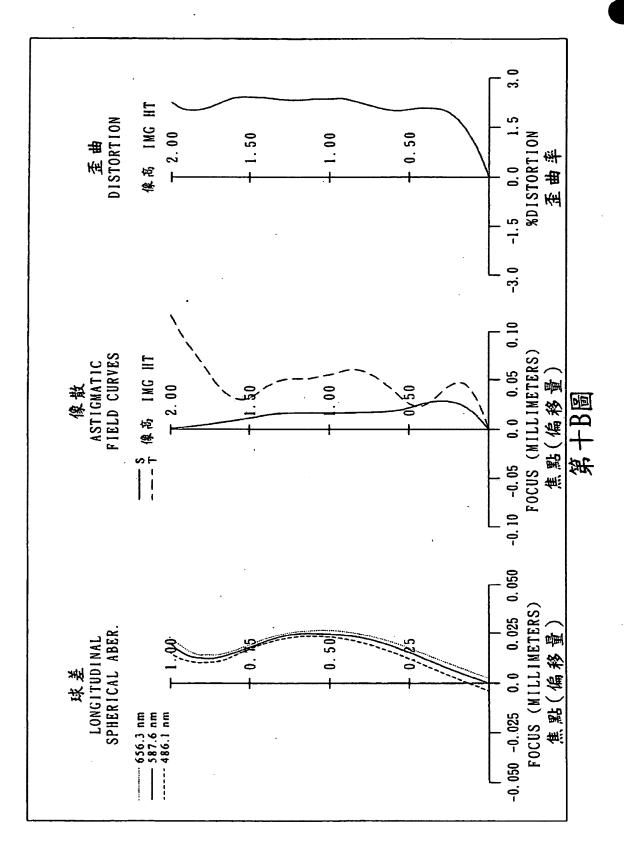
16/23



第九A區

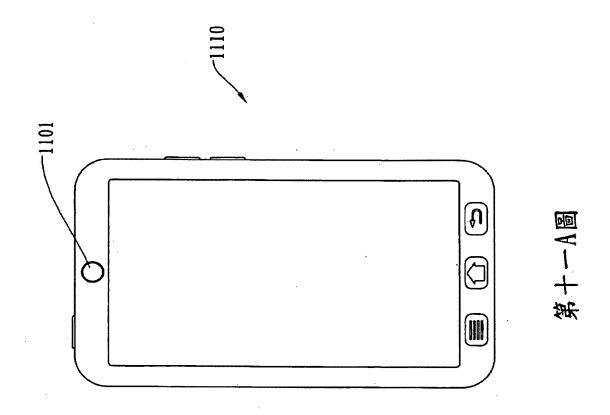






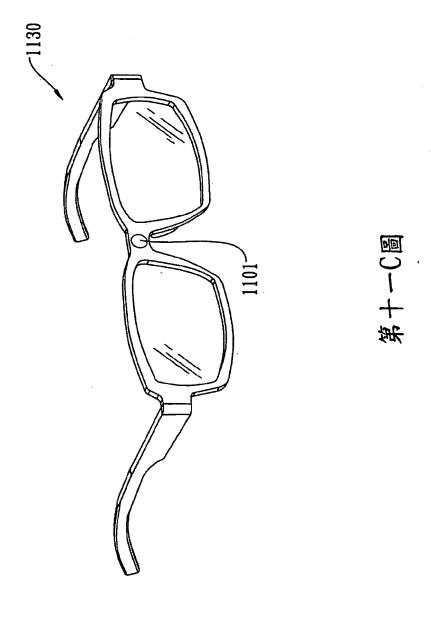
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<u>(</u>.



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申請案號:102139029



23/23

S/N: 14/105,811 PATENT
Confirmation No. 5836



# IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Wei-Yu Chen

Examiner:

Unassigned

Serial No.:

14/105,811

Group Art Unit:

Unassigned

Filed:

December 13, 2013

Docket No.:

14970-94702

Title:

IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE

**TERMINAL** 

**CERTIFICATE UNDER 37 CFR 1.8:** 

I hereby certify that this correspondence is being deposited on January 6, 2014 with the United States Postal Service as first class mail, with sufficient postage, in an envelope addressed to: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

By: Name: Tim Tingkang Xia

# **TRANSMITTAL**

Commissioner for Patents P.O. Box 1450 Alexandria, VA 22313-1450 January 6, 2014

Customer No. 24728

Sir:

We are transmitting herewith the attached:

Transmittal Sheet containing Certificate of Mailing (1 page)

Submission of Priority Document (1 page)

Certified Copy of Priority Document Taiwan Patent Application 102139029, filed October 29, 2013 (66 pages)

Return Postcard

MORRIS, MANNING & MARTIN, LLP 1600 Atlanta Financial Center 3343 Peachtree Road NE Atlanta, Georgia 30326 404.495.3678

Customer No. 24728

By: Name: Tim Tingkang Xia

Reg. No.: 45,242

TTX

17,1

S/N: 14/105,811

PATENT Confirmation No. 5836



# IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Wei-Yu Chen

Examiner:

Unassigned

Serial No.:

14/105,811

Group Art Unit:

Unassigned

Filed:

December 13, 2013

Docket No.:

14970-94702

Title:

IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE

TERMIAL

**CERTIFICATE UNDER 37 CFR 1.8:** 

I hereby certify that this correspondence is being deposited on January 6, 2014 with the United States Postal Service as first class mail, with sufficient postage, in an envelope addressed to: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

By: Name: Tim Tingkang Xia

# **SUBMISSION OF PRIORITY DOCUMENT**

Commissioner for Patents P.O. Box 1450 Alexandria, VA 22313-1450 January 6, 2014

**CUSTOMER NO. 24728** 

Dear Sir:

The certified copy of Taiwan Patent Application No. 102139029, from which this application claims priority is hereby submitted as the priority document.

If there are any questions regarding this matter, please call the undersigned at 404-495-3678.

Respectfully submitted,

MORRIS, MANNING & MARTIN, LLP

January 6, 2014

Tim Tingkang Xia Reg. No. 45,242

Attorney for the Assignee and Applicants on Record

MORRIS, MANNING & MARTIN, L.L.P. 1600 Atlanta Financial Center 3343 Peachtree Road, N.E. Atlanta, Georgia 30326 404-495-3678 Direct Customer No. 24728



# UNITED STATES PATENT AND TRADEMARK OFFICE

UNITED STATES DEPARTMENT OF COMME United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov UNITED STATES DEPARTMENT OF COMMERCE

APPLICATION NUMBER PATENT NUMBER GROUP ART UNIT FILE WRAPPER LOCATION

14/105,811 2872



# Correspondence Address/Fee Address Change

The following fields have been set to Customer Number 24728 on 06/10/2014

- Correspondence Address
- Maintenance Fee Address

The address of record for Customer Number 24728 is:

24728 MORRIS MANNING MARTIN LLP 3343 PEACHTREE ROAD, NE **1600 ATLANTA FINANCIAL CENTER** ATLANTA, GA 30326

PTO/SB/08a (01-10)

Approved for use through 07/31/2012. OMB 0651-0031

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	Application Number		14105811	
INFORMATION BIOGLOGUES	Filing Date		2013-12-13	
INFORMATION DISCLOSURE	First Named Inventor	ventor WEI-YU CHEN		
STATEMENT BY APPLICANT (Not for submission under 37 CFR 1.99)	Art Unit		2872	
( Not for Submission under or or it 1.00)	Examiner Name			
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Application Number		14105811				
Filing Date		2013-12-13				
First Named Inventor	WEI-Y	YU CHEN				
Art Unit		2872				
Examiner Name						
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# English Translation of Abstract of JP2014-178623

This invention provides a wide-angle lens system 10 from an object-side to an image-side in order including a first lens element 11 with negative refractive power, a second lens element 12 with positive refractive power, a third lens element 13 with negative refractive power and a fourth lens element 14 with positive refractive power. The first lens element 11 has negative refractive power and a concave surface and the second lens element 12 has positive refractive power and convex surfaces such that a total track length of the lens system with more than 65-degree view of angle is controlled within about 5mm. An image surface 14b of the fourth lens element 14 is provided with inflection points so as to control a direction of the light coming from the wide-angle lens system 10.

(19) 日本国特許厅(JP)

02)公開特許公報(A)

(11)特許出願公開番号

####2014-178623

(P2014-178823A)

(43) 公司日 平成26年9月25日(2014.9.25)

(S1) Int.Ci.

(20)

F I GO2B 13/00 テーマコード (参考)

GO28 13/00 GO28 13/18 (2006, 01) (2006, 01)

GO2B 13/18

2H087

審査請求 未請求 請求項の数 7 OL (全 31 頁)

(21) 出願報号 (22) 出願日 特第2013-53990 (P2013-53990)

平成25年3月15日(2013.3.15)

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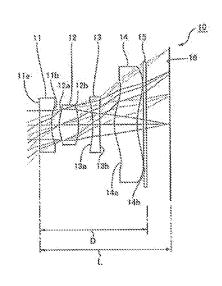
(54) (発明の名称) 広角レンズおよび振像装置

## (57) 【要約】

【課題】レンズ系の全長を短く抑え、結像而に対する主 光線入射角度を小さく抑制できる広角レンズを提供する こと。

【解決手段】広角レンズ10は、物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ11、正のパワーを有する第2レンズ12、負のパワーを有する第3レンズ13、および正のパワーを有する第4レンズ14からなる。第1レンズ11に凹形状を備える負のパワーのレンズを配置し、第2レンズ12に凸形状を備える正のパワーを有するレンズを配置したので、65、以上の調角を備えるレンズ系の全長を5mm程度に抑えることができる。第4レンズ14の像側レンズ面14bは、変曲点を有しているので、広角レンズ10からの射出光線の方向を制御できる。

(BRE) MI



# [特許請求の範囲]

# [請求項1]

物体側から像側に向かって順に配置された、負のパワーを有する第 1 レンズ。正のパワーを有する第 2 レンズ、負のパワーを有する第 3 レンズおよび正のパワーを有する第 4 レンズからなり、

前記第1レンズの像側レンズ面は、凹形状を備え、

前記第2レンズの物体側レンズ面は、凸形状を備え。

前記第4レンズの像側レンズ面は、変曲点を備える非球面であり、光軸を含む中央部分が囲形状をしており。

新記録 4 レンズの像側レンズ面を含む少なくとも2つのレンズ面が非球面とされている ことを特徴とする広角レンズ。

#### 【翻求項2】

讃潔項1において、

レンズ系全体の焦点距離を f 、前記第 2 レンズの焦点距離を f 2 としたときに、以下の 条件式 (1)を満たすことを特徴とする広角レンズ。

 $0.4 \le f2/f \le 0.7 \cdot (1)$ 

#### 【請求項3】

請求項1または2において、

前記第3レンズの焦点距離を (3としたときに、以下の条件式 (2)を満たすことを特徴とする広角レンズ。

 $-1 \le f2/f3 \le -0.25 \cdot \cdot (2)$ 

#### [諸隶項4]

蠶束項1ないし3のうちのいずれかの項において、

前記第1レンズの物体側レンズ面の物体側の端から第4レンズの像側レンズ面の像側の端までの距離をDとしたときに、以下の条件式(3)を満たすことを特徴とする広角レンズ。

1.  $0 \le D/t \le 2.0 - (3)$ 

# [請求項5]

讃遠項1ないしょのうちのいずれかの項において、

前記第1レンズの無点距離を f 1 としたときに、以下の条件式 (4) を満たすことを特 微とする広角レンズ。

 $-30 \le fi/f \le -0.5 \cdot \cdot (4)$ 

# [請求項6]

請求項1ないし5のうちのいずれかの項において。

画角が65°以上であることを特徴とする広角レンズ。

# 【辦求項7】

請求項1ないし8のうちのいずれかの項に配載の広角レンズと、

前記広角レンズの焦点位置に配置された操像素子と、を有することを特徴とする操像装置。

# [発明の詳細な説明]

## 【技術分野】

[0001]

本発明は、4枚のレンズからなる小型の広角レンズおよび当該広角レンズを搭載する撮像装置に関する。

# (背景技術)

# [00003]

携帯電話などの情報端末や小型のデジタルカメラに搭載される撮像レンズは特許文献 1 に記載されている。同文献の撮影レンズは物体側から像側に向かって順に配置された、正 のパワーを備える第 1 レンズ、負のパワーを備える第 2 レンズ、正のパワーを備える第 3 レンズ、像側が凸のメニスカス形状の第 4 レンズ、および、像側レンズ面が変曲点を備え

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る非球菌形状とされた第5レンズを備えている。筒文献の撮像レンズの最大顔角は60°である。

【先行技術文献】

[特許文献]

[0003]

【特許文献1】特關2009-14947号公報

[発明の概要]

[発明が解決しようとする課題]

[0004]

情報端末や小型のデジタルカメラなどの機器に搭載される撮像レンズにおいては、使い 勝手を考慮して両角を広くする場合がある。すなわち、これらの小型の機器においては、 標準両角の撮像レンズを、60°以上の両角の広角レンズに置き換えることが要求される 場合がある。

[0005]

ここで、標準レンズを広角レンズに置き換えるためには、広角レンズのレンズ系の全長 (第1レンズの物体側レンズ面の物体側の端から結像菌までの距離)を短く抑え、広角レ ンズを標準レンズの配置スペースに設置可能としなければならない。また、これらの機器 において、振像レンズの無点位置に配置される撮像業子には、そのセンサ面に斜めから入 射する光に対して感度が低下する特性を有するものがあるので、センサ面(撮像レンズの 結像菌)に対する主光線入射角度を小さく抑制して、画質の劣化を抑制しなければならな い。

[0006]

さらに、情報端末や小型のデジタルカメラなどの機器に搭載される機像レンズには、経 圏化や製造コストの抑制が求められている。かかる要求に対応するためには、操像レンズ を構成しているレンズの枚数を減少させることが窒ましい。

[0007]

このような点に鑑みて、本発明の課題は、レンズ系の全長を短く抑え、結像面に対する 主光線入射角度を小さく抑制できるす故のレンズから構成された広角レンズを提供するこ とにある。また、このような広角レンズを搭載する提像装置を提供することにある。

【課題を解決するための手段】

[8000]

上記課題を解決するために、本発明の広角レンズは、

物体側から像側に向かって順に配置された、蚤のパワーを有する第 1 レンズ、正のパワーを有する第 2 レンズ、魚のパワーを有する第 3 レンズおよび正のパワーを有する第 4 レンズからなり。

前記第1レンズの像側レンズ面は、凹形状を備え、

前記第2レンズの物体側レンズ面は、凸形状を備え、

前記第4レンズの像側レンズ面は、変曲点を備える非球面であり、光軸を含む中央部分が凹形状をしており、

簡記第4レンズの像側レンズ面を含む少なくとも2つのレンズ面が非球面とされていることを特徴とする。

[00009]

本発明によれば、第1レンズに凹形状を備える負のパワーのレンズを配置し、第2レンズに凸形状を備える正のパワーを有するレンズを配置したので、レンズ系の全長を抑えた広角レンズを構成できる。また、第4レンズの像側レンズ面を、変曲点を備える非球面としたので、広角レンズからの射出光線の方向を制御することが容易となり、結像面に入射する主光線入射角度を小さく抑制することができる。さらに、第4レンズの像側レンズ面を含む少なくとも2つのレンズ面が非球面とされているので、広角レンズを明るく構成することが容易である。これに加えて、4枚のレンズから広角レンズを構成したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの抑制を図ることが容

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器である。なお、広角レンズとは、一般的に、画角が60°以上の撮像レンズをいう。主 光線入射角度とは、結像面へ入射する光線と光軸が交差する角度である。

## [0010]

本発明において、レンズ系全体の焦点距離を f 、前記第 2 レンズの焦点距離を f 2 としたときに、以下の条件式 (1) を満たすことが望ましい。

 $0.4 \le 12/1 \le 0.7 + (1)$ 

## [0011]

条件式 (1) はレンズ系の全長の抑制を容易にするものであり、条件式 (1) の上限値を上回ると、レンズ系の全長の増大を招く。条件式 (1) の下限値を下回ると、パックフォーカスを確保することが困難となる。

3.0

#### [0012]

本発明において、前記第3レンズの焦点距離をf3としたときに、以下の条件式(2) を満たすことが望ましい。

 $-1 \le f/2/f/3 \le -0.25 \cdot (2)$ 

## [0013]

条件式(2)は軸上の色収差を抑制するものである。すなわち、軸上の色収差は隣接配置した正のパワーを有する第2レンズ12、負のパワーを有する第3レンズ13によって 抑制することが可能であるが、第2レンズのパワーと第3レンズのパワーのバランスによって、条件式(2)の上限値を上回ると色収差の補正が不足となり、条件式(2)の下限値を下回ると色収差に過剰補正が生じる。

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#### 400141

本発明において、前記第1レンズの物体側レンズ面の物体側の端から第4レンズの像側 レンズ面の像側の端までの距離 (レンズ系のレンズ厚)をDとしたときに、以下の条件式 (3)を満たすことが望ましい。

 $1.0 \leq D/f \leq 2.0 \cdot \cdot (3)$ 

# [0.015]

条件式 (3) はパックフォーカスを確保しながらレンズ系の全長を抑制することを容易にするものである。条件式 (3) の上限値を上回るとパックフォーカスを確保することが 困難となる。条件式 (3) の下限値を下回ると、各レンズの間の距離が短くなり、各レンズの配置に無理が生じやすい。すなわち、各レンズの中心厚やコパ厚によって、各レンズの配置が困難となる場合が発生する。

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## [0016]

本発明において、前記第1レンズの焦点距離をf1としたときに、以下の条件式(4) を満たすことが望ましい。

 $-30 \leq f1/f \leq -0.5 \cdot \cdot (4)$ 

#### [0017]

条件式(4)は断角の確保を容易にするものである。条件式(4)の上限値を上回ると第1レンズのパワーがレンズ系の中で大きくなりすぎて、全長の増大を招く。また、第1レンズのパワーがレンズ系の中で大きくなりすぎて、像面湾曲の補正が困難となる。条件式(2)の下限値を下回ると、第1レンズのパワーの低下により画角の確保が嫌しくなる

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#### [0018]

本発明において、脳角は65°以上とすることができる。すなわち、標準レンズよりも広い脳角を備えるものとすることができる。

#### [0019]

次に、本発明の撮像装置は、上記の広角レンズと、前記広角レンズの焦点位置に配置された撮像案子とを有することを特徴とする。

#### [0050]

本発明によれば、広角レンズのレンズ系の全長が短く抑えられている。従って、選像装 搬を小さく機成できる。また、広角レンズが明るく、結像面に対する主光線入射角度が小

さく抑制されている。従って、撮像レンズの焦点位置に配置される撮像業子がそのセンサ 面に斜めから入射する光に対して感度が低下する特性を有するものであっても、画質の劣 化を抑制することができる。さらに、4枚のレンズから広角レンズを構成したので、5枚 以上のレンズを備える撮像レンズを搭載する場合と比較して、撮像装置の軽量化や製造コ ストの抑制を図ることが容易である。

## 【発明の効果】

#### [[5003

本発明によれば、レンズ系の全長を短く抑え、結像面に対する主光線入射角度を小さく 抑制した明るい広角レンズを4枚のレンズから構成できる。

[図画の簡単な説明]

# [0052]

【図1】本発明を適用した実施側1の広角レンズの構成図である。

【図2】図1の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図3】本発明を適用した実施例2の広角レンズの構成図である。

【図4】図3の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図5】本発明を適用した実施例3の広角レンズの構成図である。

【図6】図5の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【器7】本発明を適用した実施側4の広角レンズの構成圏である。

【図8】図での広角レンズの綴収差図、横収差図、像面湾曲図、歪曲収差図である。

【図9】本発明を適用した実施例5の広角レンズの構成図である。

【図10】図9の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図11】広角レンズを搭載する撮像装置の説明図である。

【発明を実施するための形態】

#### [0023]

以下に図面を参照して、本発明を適用した広角レンズを説明する。

# [0024]

#### (実施例1)

図1は実施例1の広角レンズの光線図である。図1に示すように、広角レンズ10は、 物体側から像側に向かって順に配置された、魚のパワーを有する第1レンズ11、正のパ ワーを有する第2レンズ12、魚のパワーを有する第3レンズ13、および正のパワーを 有する第4レンズ14からなる。第1レンズ11と第2レンズ12の際には絞り(不顯示 ) が配置されている。第4レンズ14の像鋼にはカバーガラス15が配置されている。結 像簡16はカバーガラス15と圏隔を開けた位置にある。

#### 100251

第1レンズ11は、物体側レンズ面11aおよび像側レンズ面11bのそれぞれが非球 面とされている。物体側レンズ面11aは凸形状を備えており、像側レンズ面11bは凹 形状を備えている。物体側レンズ面11aは、凸形状をしているレンズ面部分の曲率半径 が大きく、平面形状に近い。

# [0026]

第2レンズ12は、物体側レンズ面12aおよび像側レンズ面12bのそれぞれが非球 面とされている。物体側レンズ面12aおよび像側レンズ面12bは、それぞれ凸形状を 備えている。

#### [0027]

第3レンズ13は、物体側レンズ面13a器よび像側レンズ面13bのそれぞれが非球 面とされている。物体側レンズ面13aおよび像側レンズ面13bは、それぞれ凹形状を 備えている。

#### [0028]

第4レンズ14は、物体側レンズ面14ョおよび像側レンズ面14日のそれぞれが非球 面とされている。物体側レンズ面14aは光軸を含む中央部分に凸形状を備えている。像 観レンズ面14 bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。

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従って、像側レンズ面14bは変曲点から内層側に向かって物体側に湾曲しており、変曲 点から外周側に向かって物体側に湾曲している。

#### [6200]

広角レンズ10の開口数をFno、半面角をn、および、レンズ系の全長(第1レンズ11の物体側レンズ面11aの物体側の端から結像面16までの距離)をL、レンズ系のレンズ準(第1レンズ11の物体側レンズ面11aの物体側の端から第4レンズ14の像側レンズ面14bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

Fno.  $\approx 2.8$ 

w ≈ 8 5 . 8°

 $L = 4.281 \, \text{mm}$ 

D = 3.212 mm

#### [0030]

また、全レンズ系の無点距離を f、第 1 レンズ 1 1 の焦点距離を f 1、第 2 レンズ 1 2 の焦点距離を f 2、第 3 レンズ 1 3 の焦点距離を f 3、第 4 レンズ 1 4 の焦点距離を f 4 とすると、これらの値は以下のとおりである。

f = 2.564

f1 = -3.390

f2 = 1.490

f3 = -3.241

f4 = 4.561

#### [0031]

ことで、本例の広角レンズ10は、以下の条件式(1)~(4)を満たす。

 $0.4 \le f2/f \le 0.7 \cdot (1)$ 

 $-1 \le f2/f3 = \le -0.25 \cdot \cdot (2)$ 

1.  $0 \le D/f \le 2.0 \cdots (3)$ 

 $-30 \le f1/f \le -0.5 \cdot \cdot (4)$ 

# [0032]

## [0033]

広角レンズIOは条件式(1)を満たすので、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。すなわち、条件式(1)の上限値を上回ると、全長の増大を招く。条件式(1)の下限値を下回ると、パックフォーカスを確保することが困難となる。

#### [0034]

広角レンズ10は条件式(2)を満たすので、軸上の色収差が抑制される。すなわち、軸上の色収差は隣接配置した正のパワーを有する第2レンズ12、負のパワーを有する第3レンズ13によって抑制することが可能となっているが、第2レンズ12のパワーと第3レンズ13のパワーのバランスによって、条件式(2)の上限値を上囲ると色収差の補正が不足となり、条件式(2)の下限値を下回ると色収差に過剰補正が生じる。

#### [0035]

広角レンズ10は条件式(3)を満たすので、パックフォーカスを確保しながらレンズ系の全長を抑制することが容易である。すなわち、条件式(3)の上限値を上回るとパックフォーカスを確保することが困難となる。条件式(3)の下限値を下回ると、各レンズの間の距離が短くなるので、各レンズの中心厚やコパ厚によって、各レンズの配置が困難となる場合が発生する。

## [0038]

広角レンズ10は条件式(4)を満たすので、画角の確保が容易である。すなわち、条件式(4)の上限値を上回ると第1レンズ11のパワーがレンズ系の中で大きくなりすぎ

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HP, Ex. 1002 Page 180 て、レンズ系の全長の増大を招く。また、条件式(4)の上機値を上回ると第1レンズ1 1のパワーがレンズ系の中で大きくなりすぎて、像面湾曲の補正が固難となる。一方、条件式(2)の下限値を下回ると、第1レンズ11のパワーの低下により画角の確保が難しくなる。

#### [0037]

また、広角レンズ10は、以下の条件式(5)、(6)を満たす。

 $-1.4 \le 13/1 \le -0.8 \cdot \cdot (5)$ 

1.3 \leq L/f \leq 2.5 \cdots \cdot (6)

#### [0038]

すなわち、 f 3 / f == -1、264であり、1 / f == 1.670である。

[0039]

広角レンズ10は条件式(5)を満たすので、色収差を良好に補正できる。すなわち、 条件式(5)の上級値を上回ると色収差の補正が過剰となり、下限値を下回ると色収差の 補正に不足が生じる。

#### [0040]

さらに、広角レンズ10は条件式(6)を満たすので、パックフォーカスを確保しながらレンズ系の全長を抑制することがより容易となる。すなわち、条件式(6)の上環値を上回るとパックフォーカスを確保することが困難となる。条件式(6)の下限値を下回ると、各レンズの間の距離が短くなるので、各レンズの中心厚やコバ厚によって、各レンズの配置が困難となる場合が発生する。

[0041]

以下の表1Aは広角レンズ10の各レンズ面のレンズデータを示す。表1Aでは物体側から数えた頻番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非球面である。なお、9面および10面はカバーガラス15のガラス面であり、11面は結像面16である。曲率半径および間隔の単位はミリメートルである。

#### [0042]

#### [表1A]

<b>100 285</b>	曲率半径		Nd(風折率)	Vd(アッペ数)	材料
1	18.988	0.400	1,53116	56.0	樹脂
2	1.639	0.259			
3	1.306	0.627	1,53116	58.0	樹脂
4	~1.693	0.477			
5	-2,153	0.226	1,63494	24.0	樹脂
6	61.884	0.479			
7	1.220	0.744	1,53118	56.0	樹脂
8	1.929	0.210			
9	infinity	0.100	1.51680	64.2	光学ガラス
10	infinity	8,781			
11	infinity	-0.022			<u> </u>

[0043]

次に、表1B、表1Cは非球面とされたレンズ面の非球面形状を規定するための非球面係数を示す。表1B、表1Cにおいても物体側から数えた順番で各レンズ面を特定している。

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### [表18]

F	第1面	第2面	<b>#3</b> iii	第4節	¥65₩	第6面
K	0.00000 E+00	1,96645 E+00	-3.24341 E+00	0,000000 E+0.0	~4,91958 E+01	3.84467 E+03
A4	-6,70903 E-02	~1,23090 E-01	1.05137 E-01	2.08266 E-01	-4,45527 E-02	2.10240 E-02
A6	1,43040 E-02	1.93268 E-01	2.60961 E-01	-7,07806 E-01	0,000000 E+00	0.00000 E+00
A8	0.000000 E+00	0.00000 E+00	-5.44654 E-01	1,00543 E+00	-1.05324 E-01	5.55869 E-02
A10	0.000000 E+00	0.000000 E+00	0.00000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00
A12	0.000000 E+00	0.00000 E+00	0.00000 E+00	0,000000 E+00	0.000000 E+00	0.00000 E+00
A14	0,00000 E+00	0.000000 E+00	0.000000 E+00	0,000000 E+00	0.000000 E+00	0.00000 E+00
A18	0.00000 E+00	0.000000 E+00	0.000000 E+00	0,000000 E+00	0.00000 E+00	0.00000 E+00

#### [X10]

********	第7面	第8面
K	-5.25406 E+00	0,000000 E+00
A4	-6.29015 E-02	-1.28252 E-01
A6	-2.28756 E-03	3,60116 E~02
A8	-8.15992 E-03	-3.97193E-02
01A	3.30573 E-04	3.02334 E-02
A12	7.78451 E-03	-1.38145 E-02
A14	-4.09359 E-03	3,33327 E-03
A16	4.32061 E-04	~3.35E-04

[0044]

なお、レンズ面に採用する非球面形状は、Yをサグ量、cを曲率半径の遊数、Kを円錐 係数、 h を光線高さ、 4 次、 6 次、 8 次、 1 0 次、 1 2 次、 1 4 次、 1 6 次の非球面係数 をそれぞれA4、A6、A8、A10、A12、A14、A16とすると、次式により表 わされる。

[0045]

[数1]

$$Y(h) = \frac{ch^2}{1 + \sqrt{1 - (K+1)c^2h^2}} + A_4h^4 + A_5h^6 + A_8h^8 + A_{10}h^{10} + A_{12}h^{12} + A_{14}h^{14} + A_{16}h^{16}$$

[0048]

(作用効果)

図2 (a)~(d)は広角レンズ10の縦収差図、横収差図、像面湾曲図、歪曲収差図 である。図2(a)の縦収差図では、横軸は光線が光軸しと交わる位置を示し、縦軸は光 線がレンズ系に入射する高さを示している。図2(b)の模収差割では機軸は入射膜底標 を示し、緩軸は収差量を示す。図2(a)、(b)では、波長の異なる複数の可視光線に ついてのシミュレーション結果を示してある。図2(c)の像面薄曲図では横軸は光軸方 向の距離を示し、機糖は像の高さを示す。図2 (c) において、Sはサジタル面における 像面湾曲収差を示し、Tはタンジェンシャル面における像面湾曲収差を示す。図2(d) の歪曲収差図では横軸は像の歪み盤を示し、縦軸は像の高さを示す。

[0047]

図2 (a) に示すように、広角レンズ10によれば、軸上の色収差が良好に矯正されて いる。また、図2(b)に示すように、色の滲みが抑制される。さらに、図2(c)、( d) に示すように、像面湾曲が良好に補正されている。従って、広角レンズ10が高解像 度となる。

[0048]

また、広角レンズ10では、第1レンズ11に凹形状を備える質のパワーのレンズを配 置し、第2レンズ12に凸形状を備える正のパワーを有するレンズを配置したので、65 以上の顕角を備えるレンズ系の全長を4.3mm以下に抑えることができる。さらに、 第4レンズ14の像側レンズ面14bを、変曲点を備える非球菌としたので、広角レンズ 20

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10からの射出光線の方向を制御することが容易となり、結像面16に入射する主光線入射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面としたので、広角レンズ10が明るく構成される。さらに、4枚のレンズから広角レンズ10を構成したので、5枚以上のレンズを備える機像レンズと比較して、軽量化や製造コストの抑制を図ることが容易である。

#### 100491

#### (寒施粥2)

図3は実施例2の広角レンズの光線図である。図3に示すように、広角レンズ20は、物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ21、圧のパワーを有する第2レンズ22、魚のパワーを有する第3レンズ23、および圧のパワーを有する第4レンズ24からなる。第1レンズ21と第2レンズ22の間には絞り(不図示)が配置されている。第4レンズ24の像側にはカバーガラス25が配置されている。結像面26はカバーガラス25と関係を開けた位置にある。

## [0050]

第1レンズ21は、物体側レンズ面21 a および像側レンズ面21 b のそれぞれが非球面とされている。物体側レンズ面21 a は凸形状を備えており、像側レンズ面21 b は凹形状を備えている。物体側レンズ面21 a は、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

#### [0051]

第2レンズ22は、物体側レンズ面22aおよび像側レンズ面22bのそれぞれが非球面とされている。物体側レンズ面22aおよび像側レンズ面22bは、それぞれ凸形状を備えている。

#### [0052]

第3レンズ23は、物体側レンズ面23aおよび像側レンズ面23bのそれぞれが非球面とされている。物体側レンズ面23aおよび像側レンズ面23bは、それぞれ凹形状を備えている。

#### [0053]

第4レンズ24は、物体側レンズ面24aおよび像側レンズ面24bのそれぞれが非球面とされている。物体側レンズ面24aは光軸を含む中央部分に凸形状を備えている。像側レンズ面24bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面24bは変曲点から内周側に向かって物体側に湾曲しており、変曲点から外周側に向かって物体側に湾曲している。

## [0054]

広角レンズ20の開口数をFno、、半頭角をの、および、レンズ系の金長(第1レンズ21の物体側レンズ面21aの物体側の端から結像面2-6までの距離)をL、レンズ系のレンズ厚(第1レンズ21の物体側レンズ面21aの物体側の端から第4レンズ24の像側レンズ面24bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

Pno. = 2.8

ω == 85. 8°

L = 4.983 mm

D = 3.935 mm

## [0055]

また、全レンズ系の無点距離を f、第 1 レンズ 2 1 の焦点距離を f 1、第 2 レンズ 2 2 の焦点距離を f 2、第 3 レンズ 2 3 の焦点距離を f 3、第 4 レンズ 2 4 の焦点距離を f 4 とすると、これらの値は以下のとおりである。

f = 2.563

f1 = -8.972

f2 = 1.529

13 = -2.479

ΙÜ

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f 4 = 7.890

#### [0056]

ここで、本側の広角レンズ20は、以下の条件式(1)~(4)を満たす。

- $0.4 \le f2/f = 0.596 \le 0.7 \cdot (1)$
- $-1 \le 12/13 = -0.617 \le -0.25 * (2)$
- 1.  $0 \le D/f = 1$ .  $535 \le 2$ .  $0 \longrightarrow (3)$
- $-30 \le f_1/f_2 2.720 \le -0.5 \cdot \cdot (4)$

#### 100571

広角レンズ20は、条件式 (1) ~ (4) を微たすので、65°以上の画角を確保しながら、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、軸上の色収差を抑制することができる。

1.0

## [0058]

また、広角レンズ20は、以下の条件式(5)、(6)を満たす。

- -1.  $4 \le f 3 / f = -0$ ,  $9 6 7 \le -0$ ,  $6 \cdot \cdot \cdot (5)$
- 1.  $3 \le L/f = 1.944 \le 2.5 \cdot \cdot (6)$

#### [0059]

広角レンズ20は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面26に入射する主光線入射角度を小さくできる。さらに、バックフォーカスを 確保しながらレンズ系の全長を抑制することが容易である。

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#### [0060]

以下の表2Aは広角レンズ20の各レンズ面のレンズデータを示す。表2Aでは物体制から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非球面である。なお、9面および10面はカバーガラス25のガラス面であり、11面は結像面26である。曲率半径および関隔の単位はミリメートルである。

#### [0 0 8 1]

#### (表2A)

W 28	曲率半径		Nd(屈折率)	Vd(アッベ数)	材料
1	18.988	0.400	1,53116	56.0	樹牆
2	3.087	1.067			
3	1.218	0.529	1,53116	56.0	樹牆
4	~2.093	0.215			
5	-2.030	0.383	1.6349.4	24.0	樹脂
6	7,868	0,601			
7	1.498	0.739	1.53116	56.0	樹脂
8	1.928	0.210			
9	infinity	0.100	1,51680	64.2	光学ガラス
10	infinity	0.762		ļ	
11	infinity	-0.024	<u>}</u>	<b></b>	<b>.</b>

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#### [0062]

次に、表2B、表2Cは非球面とされたレンズ面の非球面形状を規定するための非球面係数を示す。表2B、表2Cにおいても物体側から数えた順番で各レンズ面を特定している。

### [表28]

			***************************************	·	
第1面	第2面	第3面	第4面	第5面	第6面
***************************************	3,85318 E+00	-2,99208 E+00	2.54698 E+00	-4,46502 E+01	0.00000 E+00
		7.81867 E-02	1.02286 E-01	-7.96020 E-02	2.08047 E-01
		***************************************	-5.30883 E-01	0.000000 E+00	0.00000 E+00
			6.21259 E-01	-2.22084E-01	8,71866 E-02
	*****	~3,91407 E-01	-1.87758 E+00	-3.06686 E-01	-8.16509 E-02
***************************************		*************	0.000000 E+00	0.00000 E+00	0.000000 E+00
	*****	***************************************	0.00000 E+00	0.00000 E+00	0.000000 E+00
	F		***********	0,00000 E+00	0,000000 E+00
	0.00000 E+00 5.78055 E-03 -1.09778 E-02 0.00000 E+00 0.00000 E+00 0.00000 E+00	0.00000 E+00 3.85318 E+00 5.78055 E-03 5.21124 E-03 -1.09778 E-02 -4.44309 E-02 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00 0.00000 E+00	0.00000E+00 3.85318E+00 -2.99208E+00 5.78055E-03 5.21124E-03 7.81867E-02 -1.09778E-02 -4.44309E-02 3.32598E-02 0.00000E+00 0.00000E+00 -7.00411E-01 0.00000E+00 0.00000E+00 -3.91407E-01 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00	0.00000 E+00         3.85318 E+00         -2.99208 E+00         2.54698 E+00           5.78055 E-03         5.21124 E-03         7.81867 E-02         1.02266 E-01           -1.09778 E-02         -4.44309 E-02         3.32598 E-02         -5.30663 E-01           0.00000 E+00         0.00000 E+00         -7.00411 E-01         6.21259 E-01           0.00000 E+00         0.00000 E+00         -3.91407 E-01         -1.87758 E+00           0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00           0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00	0.00000 E+00         3.85318 E+00         -2.99208 E+00         2.54698 E+00         -4.46502 E+01           5.78055 E-03         5.21124 E-03         7.81867 E-02         1.02286 E-01         -7.96020 E-02           -1.09778 E-02         -4.44309 E-02         3.32598 E-02         -5.30863 E-01         0.00000 E+00           0.00000 E+00         0.00000 E+00         -7.00411 E-01         6.21259 E-01         -2.22084 E-01           0.00000 E+00         0.00000 E+00         -3.91407 E-01         -1.87758 E+00         -3.06686 E-01           0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00           0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00         0.00000 E+00

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#### [表20]

	第7面	第8第
K	-5.38920 E+00	8.00000 E+00
A4	-1,11271 E-01	~1.63845 E-01
AG	3.08045 E-02	4.93248 E-02
A8	-3.76929 E-03	-3.99351 E-02
A10	-3.21886 E-03	3.00214 E-02
A12	5.97323 E-03	1.39517E02
A14	-4.16558 E-03	3.30562 E-03
A18	9.01603 E-04	3.20E04

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#### [0063]

#### (作用効果)

圏 4 (a)  $\sim$  (d) は広角レンズ 2 0 の縦収差圏、横収差圏、像面薄曲圏、歪曲収差圏である。図 4 (a) に示すように、広角レンズ 2 0 によれば、軸上の色収差が良好に補正されている。また、図 4 (b) に示すように、色の滲みが抑制される。さらに、図 4 (c) (d) に示すように、像面湾曲が良好に補正されている。従って、広角レンズ 2 0 が高解像度となる。

### [0064]

また、広角レンズ20では、第1レンズ21に凹形状を備える負のパワーのレンズを配置し、第2レンズ22に凸形状を備える正のパワーを有するレンズを配置したので、65以上の画角を備えるレンズ系の全長を5mm以下に抑えることができる。さらに、第4レンズ24の像側レンズ面24bを、変曲点を備える非球面としたので、広角レンズ20からの射出光線の方向を制御することが容易となり、結像面26に入射する主光線入射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面としたので、広角レンズ20が明るく構成される。さらに、4枚のレンズから広角レンズを構えるで、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの抑制を図ることが容易である。

## [0055]

#### (実施例3)

図5は実施例3の広角レンズの光線図である。図5に示すように、広角レンズ30は、物体側か5像側に向かって順に配置された、負のパワーを有する第1レンズ31、正のパワーを有する第2レンズ32、気のパワーを有する第3レンズ33、および正のパワーを有する第4レンズ34からなる。第1レンズ31と第2レンズ32の際には絞り(不図示)が配置されている。第4レンズ34の像側にはカバーガラス35が配置されている。結像面36はカバーガラス35と間隔を開けた位置にある。

[0056]

第1レンズ31は、物体側レンズ面31aおよび像側レンズ面31bのそれぞれが非球面とされている。物体側レンズ面31aは凸形状を備えており、像側レンズ面31bは凹形状を備えている。物体側レンズ面31aは、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

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[0087]

第2レンズ32は、物体側レンズ面32aおよび像側レンズ面32bのそれぞれが非球面とされている。物体側レンズ面32aおよび像側レンズ面32bは、それぞれ凸形状を備えている。

[0068]

第3レンズ33は、物体側レンズ面33aおよび像側レンズ面33bのそれぞれが非球面とされている。物体側レンズ面33aは凹形状を備えており、像側レンズ面33bは凸形状を備えている。

[0069]

第4レンズ34は、物体側レンズ面34 a および像側レンズ面34 b のそれぞれが非球面とされている。物体側レンズ面34 a は光軸を含む中央部分に凸形状を備えている。像側レンズ面34 b は、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。後のて、像側レンズ面34 b は変曲点から内角側に向かって物体側に湾曲しており、変曲点から外角側に向かって物体側に湾曲している。

[0070]

広角レンズ30の開口数をFno、、半瀬角をn、および、レンズ系の全長(第1レンズ31の物体側レンズ面31aの物体側の端から結像面36までの距離)をL、レンズ系のレンズ厚(第1レンズ31の物体側レンズ面31aの物体側の端から第4レンズ34の像側レンズ面34bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

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Fno. = 2.8

 $w = 8.5.8^{\circ}$ 

L = 3.838 mm

D = 2.783 mm

[0071]

また、全レンズ系の焦点距離を f、第1レンズ31の焦点距離を f1、第2レンズ32 の焦点距離を f2、第3レンズ33の焦点距離を f3、第4レンズ34の焦点距離を f4 とすると、これらの値は以下のとおりである。

f == 2. 563

fl == -4. 824

f 2 = 1.340

f3 = -2.259

f4 = 4.190

[0072]

ここで、本例の広角レンズ30は、以下の条件式(1)~(4)を満たす。

0.  $4 \le f 2 / f = 0$ ,  $5 2 3 \le 0$ ,  $7 \rightarrow (1)$ 

 $-1 \le f2/f3 = -0.593 \le -0.25 \cdot \cdot (2)$ 

1.  $0 \le D/f = 1.086 \le 2.0 \cdot \cdot (3)$ 

 $-30 \le f1/f = -1.882 \le -0.5 \cdot \cdot (4)$ 

[0073]

広角レンズ30は、条件式(1)~(4)を満たすので、65°以上の顕角を確保しながら、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、軸上の色収差を抑制することができる。

100741

また、広角レンズ30は、以下の条件式(5)、(6)を満たす。

 $-1.4 \le f3/f = -0.881 \le -0.8 \cdot \cdot (5)$ 

1.  $3 \le L/f = 1$ .  $498 \le 2$ .  $5 \cdot \cdot \cdot (6)$ 

[0075]

広角レンズ30は条件式(5)、(6)を満たすので、色収差を度好に補正できる。また、結像菌36に入射する主光線入射角度を小さくできる。さらに、バックフォーカスを

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HP, Ex. 1002 Page 186 確保しながらレンズ系の全長を抑制することが容易である。

## [0076]

以下の表3Aは広角レンズ30の各レンズ面のレンズデータを示す。表3Aでは物体側から数えた頻番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非球面である。なお、9面および10面はカバーガラス35のガラス面であり、11面は結像面36である。曲率半径および開隔の単位はミリメートルである。

## [0077]

## [表3 A]

(S) 35	曲率半径		Nd(屈折率)	Va(アッペ数)	材料
1	150,000	0,400	1,53116	56.0	樹鵬
2	2.527	0.068	***************************************		
3	8.974	0.479	1.53116	58.0	樹脂
4	-2.225	0.289			16.1.864
5	-0.678	0.322	1.6349.4	24.0	掛龍
8	-1.512	0.301	<b></b>		. X4X 2064
7	1.218	0.923	1.5311.6	56.0	樹脂
8	1.971	0.210		<u> </u>	30 306 35°
9	infinity	f	1.51680	64.2	光学ガラス
10	infinity	***************************************			
11	infinity	-0.028			ł

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## [0078]

次に、表3B、表3Cは非球面とされたレンズ面の非球面形状を規定するための非球面 係数を示す。表3B、表3Cにおいても物体側から数えた順番で各レンズ面を特定している。

## [養38]

	第1面	第2面	第3面	364 m	第5面	第6 <b>m</b>
K	0.000000 E+00		-3.83881 E+00	5,33538 E+00	-4.54098 E+00	0.00000 E+00
A4	-1.74521 E-02		5,90588 E-02	8,27775 E-02	-4.37925 E-01	1,43565 E-01
A8	-1.70578 E-01	-1,70011 E-01	8.54668 E-02	-2,36439 E-01	0.000000 E+00	0,00000 E+00
A8	0.00000 E+00	0.00000 E+00	-5.37071 E-01	~1,38356 E+00	1.01643 E+00	6,87456 E-01
A10	0.00000 E+00	0.00000 E+00	-3.10124 E+00	9.66727 E-01	1.18549 E+00	-1.66451 E-01
A12	0.00000 E+00	0.00000 E+00	0.000000 E+00	0.000000 E+00	0.000000 E+00	0.000000 E+00
A14	0,00000 E+00	0,00000 E+00	0.000000 E+00	0.000000 E+00	0.00000 E+08	0.000000 E+000
A16	0.00000 E+00	3	0.00000 E+00	0.000000 E+00	0.000000 E+00	0.00000 E+00

#### [衰3C]

	******	***************
	第7面	第8面
X	-7.24393 E+00	0.000000 E+00
A4	-1.40591 E-01	-1.80857 E-01
A6	4.71327 E-02	6,52796 E-02
A8	-5.32562 E-03	-4.48510 E-02
A10	~5.36876 E~03	2.97256 E-02
A12	5,96681 E-03	-1.34959 E-02
A14	-4.45794 E-03	3.25636 E-03
A18	1.08896 E-03	-3.23E-04

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## [0 0 7 9]

#### (作用効果)

図 6 (a) ~ (d) は広角レンズ 3 0 の継収差図、模収差図、像面湾曲図、歪曲収差図である。図 6 (a) に示すように、広角レンズ 3 0 によれば、軸上の色収差が良好に補正されている。また、図 6 (b) に示すように、色の参みが抑制される。さらに、図 6 (c)、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レンズ 3 0 が

高解像度となる。

#### 10801

また。広角レンズ30では、第1レンズ31に凹形状を備える負のパワーのレンズを配置し、第2レンズ32に凸形状を備える正のパワーを有するレンズを配置したので、65%以上の画角を備えるレンズ系の全長を4mm以下に抑えることができる。さらに、第4レンズ34の像側レンズ面34bを、変曲点を備える非球面としたので、広角レンズ30からの射出光線の方向を制御することが容易となり、結像面36に入射する主光線入射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面としたので、広角レンズ30が明るく構成される。さらに、4枚のレンズから広角レンズ10を構成したので、5枚以上のレンズを備える据像レンズと比較して、軽量化や製造コストの抑制を図ることが容易である。

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#### [0081]

#### (実施例4)

図7は実施例4の広角レンズの光線図である。図7に示すように、広角レンズ40は、物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ41、正のパワーを有する第2レンズ42、負のパワーを有する第3レンズ43、および正のパワーを有する第4レンズ44からなる。第1レンズ41と第2レンズ42の間には絞り(不図示)が配置されている。第4レンズ44の像側にはカバーガラス45が配置されている。結像面46はカバーガラス45を配置されている。結

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#### [0082]

第1レンズ41は、物体側レンズ面41aおよび像側レンズ面41bのそれぞれが非球面とされている。物体側レンズ面41aは凸形状を備えており、像側レンズ面41bは凹形状を備えている。物体側レンズ面41aは、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

#### [0083]

第2レンズ42は、物体側レンズ面42aおよび像側レンズ面42bのそれぞれが非球面とされている。物体側レンズ面42aおよび像側レンズ面42bは、それぞれ凸形状を備えている。

#### [0084]

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第3レンズ43は、物体側レンズ面43aおよび像側レンズ面43bのそれぞれが非球面とされている。物体側レンズ面43aは凹形状を備えており、像側レンズ面43bは凸形状を備えている。

#### [0085]

第4レンズ44は、物体側レンズ面44aおよび像側レンズ面44bのそれぞれが非球 固とされている。物体側レンズ面44aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面44bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面44bは変曲点から内局側に向かって物体側に湾曲しており、変曲 点から外層側に向かって物体側に湾曲している。

[0086]

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広角レンズ40の開口数をFno、 半面角をω、および、レンズ系の全長(第1レンズ41の物体側レンズ面41aの物体側の端から結像面46までの距離)をし、レンズ系のレンズ厚(第1レンズ41の物体側レンズ面41aの物体側の端から第4レンズ44の像側レンズ面44bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

Fno. = 2.8

w = 8 5 . 8 °

L=3.932mm

D = 2.895 mm

#### [0087]

また、全レンズ系の焦点距離をよ、第1レンズ41の焦点距離をよ1、第2レンズ42

HP, Ex. 1002 Page 188 の焦点距離を f 2、第 3 レンズ 4 3 の焦点距離を f 3、第 4 レンズ 4 4 の焦点距離を f 4 とすると、これらの値は以下のとおりである。

f = 2.563

f1 = - 1 4 . 4 5 6

fz = 1.595

f3 == -2. 032

f4 = 3.607

#### [0088]

ここで、本例の広角レンズ40は、以下の条件式(1)~(4)を満たす。

 $0.4 \le f2/f = 0.622 \le 0.7 \cdot (1)$ 

-15 f2/f3=-0.785 5-0.25 · · (2)

1.  $0 \le D/t = 1$ , 129  $\le 2$ ,  $0 \cdot \cdot \cdot (3)$ 

 $-30 \le [1/f=-5.840 \le -0.5 \cdot \cdot (4)]$ 

#### [0089]

広角レンズ40は、条件式(1)~(4)を満たすので、65°以上の画角を確保しながら、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。

#### [0090]

また、広角レンズ40は、以下の条件式(5)、(6)を満たす。

 $-1:4 \le 13/1 = -0.793 \le -0.6 + \cdot (5)$ 

1.  $3 \le 1/f = 1$ ,  $534 \le 2$ ,  $5 \times (6)$ 

## [0091]

広角レンズ40は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面46に入射する主光線入射角度を小さくできる。さらに、バックフォーカスを 確保しながらレンズ系の全長を抑制することが容易である。

## [0092]

以下の表4Aは広角レンズ40の各レンズ面のレンズデータを示す。表4Aでは物体側から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非球面である。なお、9面および10面はカバーガラス45のガラス面であり、11面は結像面46である。曲率半径および関係の単位はミリメートルである。

100931

## [数4A]

逐發	曲率半径		Nd(開折率)	Vd(アッペ数)	材料
1	150,000	0.400	1,53116	56.0	横淵
2	7,327	0,099			
3	1,413	0,558	1.53116	56.0	被胎
4	-1.846	0,338			
5	-0.578	0,361	1,63494	24.0	187 HB
6	-1.285	0,146			
7	1.147	0.995	1,53116	56.0	樹脂
8	1.986	0.210			
9	infinity	0.100	1,51680	64.2	光学ガラス
10	infinity	0.753			
11	infinity	-0.026			

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#### 100941

次に、義4B、表4Cは非球面とされたレンズ面の非球面形状を規定するための非球面係数を示す。接4B、表4Cにおいても物体側から数えた順番で各レンズ面を特定している。

#### [赛48]

	第1面	<b>%2</b> 10	第3面	\$\$4[8]	第5面	第6面
K	0,000000 E+00	9.96692 E+01	~4.55267 E+00	5.20287 E+00	-3.51020 E+00	0.00000 E+00
A4	-2,50823 E-03	-3.83857 E-02	3.83770 E-02	-1.33640 E-01	-5.16180 E-01	1,22505 E-0.1
A6	-8,07761 E-02	-6.22535 E-02	-1.17843 E-01	7.52591 E-02	0.00000 E+00	0.00000 E+00
A8	0,000000 E+00	-3.63324 E-01	~7.96090 E-01	-1.60850 E+00	8,70251 E-01	6,90508 E-01
A10	0,000000 E+00	0.000000 E+00	~4.16550E+00	5.85779 E-01	8.59858 E-01	-3.11595 E-01
A12	0,000000 E+00	0.000000 E+00	6.20707 E+00	1.85436 E+00	-3.35126 E-01	-4.39279 E-02
A14	0.000000 E+00	0,00000 E+00	0.000000 E+00	0.000000 E+00	0.00000 E+00	0.000000 E+00
A16	0.00000 E+00	0.00000 E÷00	0.00000 E+00	0.000000 €+00	0.000000 E+00	0.000000 E+00

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#### [表40]

************	第7面	第8節
K	~8.11925 E+00	0.00000 E+00
44	-1.95885 E-01	-1.93101 E-01
A6	1.03146 E-01	7.12000 E-02
A8	-3,61144 E-02	-4.41820 E-02
A10	2.84718 E-03	2.85423 E-02
A12	6.32241 E-03	-1.35319 E-02
A14	~6.95948 E-03	3.43603 E-03
A18	1.89193 E-03	-3.56E-04

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#### 100961

#### (作用効果)

図8(a)~(d)は広角レンズ40の縦収差図、機収差図、像面薄曲図、歪曲収差図である。図8(a)に示すように、広角レンズ40によれば、軸上の色収差が良好に補正されている。また、図8(b)に示すように、色の滲みが抑制される。さらに、図8(c)、(d)に示すように、像面密曲が良好に補正されている。従って、広角レンズ40が高解像度となる。

#### [0096]

また、広角レンズ40では、第1レンズ41に凹形状を備える魚のパワーのレンズを配置し、第2レンズ42に凸形状を備える正のパワーを有するレンズを配置したので、65%以上の画角を備えるレンズ系の全長を4.0mm以下に抑えることができる。さらに、第4レンズ44の像側レンズ面44bを、変曲点を備える非球面としたので、広角レンズ40からの射出光線の方向を制御することが容易となり、結像面46に入射する主光線入射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面としたので、広角レンズ40が弱るく構成される。さらに、4枚のレンズから広角レンズを構成したので、5枚以上のレンズを構える撮像レンズと比較して、軽量化や製造コストの抑制を図ることが容易である。

#### [0097]

#### (実施例5)

図9は実施例5の広角レンズの光線図である。図9に示すように、広角レンズ50は、物体側から像側に向かって順に配置された、食のパワーを有する第1レンズ51、正のパワーを有する第2レンズ52、食のパワーを有する第3レンズ53、および正のパワーを有する第4レンズ54からなる。第1レンズ51と第2レンズ52の間には絞り(不図示)が配置されている。第4レンズ54の像側にはカバーガラス55が配置されている。結像面56はカバーガラス55と間隔を開けた位置にある。

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#### [0098]

第1レンズ51は、物体側レンズ面51aおよび像側レンズ面51bのそれぞれが非球面とされている。物体側レンズ面51aは凸形状を備えており、像側レンズ面51bは凹形状を備えている。物体側レンズ面51aは、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

#### [0099]

第2レンズ52は、物体側レンズ面52aおよび像側レンズ面52bのそれぞれが非球面とされている。物体側レンズ面52aおよび像側レンズ面52bは、それぞれ凸形状を備えている。

#### [0010]

第3レンズ53は、物体側レンズ面53aおよび像側レンズ面53bのそれぞれが非球面とされている。物体側レンズ面53aは凹形状を備えており、像側レンズ面53bは凸形状を備えている。

#### [0101]

第4レンズ54は、物体側レンズ面54aおよび像側レンズ面54bのそれぞれが非球面とされている。物体側レンズ面54aは光軸を含む中央部分に凸形状を備えている。像側レンズ面54bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。従って、像側レンズ面54bは変曲点から内周側に向かって物体側に湾曲しており、変曲点から外周側に向かって物体側に湾曲している。

#### [0102]

広角レンズ50の開口数をFno、、半面角をω、および、レンズ系の全長(第1レンズ51の物体側レンズ面51aの物体側の端から結像面56までの距離)をL、レンズ系のレンズ厚(第1レンズ51の物体側レンズ面51aの物体側の端から第4レンズ54の像側レンズ面54bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

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Fno. = 2.8

 $\omega = 8.5.7^{\circ}$ 

 $L = 4.107 \, \text{mm}$ 

D = 3.031 mm

#### [0103]

また、全レンズ系の焦点距離を f 、第 1 レンズ 5 1 の焦点距離を f 1 、第 2 レンズ 5 2 の焦点距離を f 2 、第 3 レンズ 5 3 の焦点距離を f 3 、第 4 レンズ 5 4 の焦点距離を f 4 とすると、これらの値は以下のとおりである。

£=2.563

f1 = -62.580

f2 = 1.715

f3 = -1.832

f4 = 3.091

## [0104]

ここで、本例の広角レンズ50は、以下の条件式(1)~(4)を満たす。

0.  $4 \le f2/f = 0$ .  $669 \le 0$ .  $7 \cdot (1)$ 

 $-1 \le f2/f3 = -0.936 \le -0.25 \cdot \cdot (2)$ 

1.  $0 \le D/f = 1$ ,  $182 \le 2$ ,  $0 \cdot \cdot \cdot (3)$ 

 $-30 \le f1/f = -24.417 \le -0.5 \cdot \cdot (4)$ 

## [0105]

広角レンズ50は、条件式(1)~(4)を満たすので、65°以上の顕角を確保しなが5、レンズ系の全長を抑制し、バックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。

#### [0106]

また、広角レンズ50は、以下の条件式(5)、(6)を満たす。

 $-1.4 \le f3/f = -0.715 \le -0.6 \cdot \cdot (5)$ 

1.  $3 \le 1/f = 1$ ,  $602 \le 2$ .  $6 \cdot \cdot \cdot (6)$ 

#### [0107]

広角レンズ50は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面56に入射する主光線入射角度を小さくできる。さらに、バックフォーカスを

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確保しながらレンズ系の全長を抑制することが容易である。

## [0108]

以下の表 5 A は広角レンズ 5 O の各レンズ面のレンズデータを示す。表 5 A では物体側から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非球面である。なお、 9 面および 1 O 面はカバーガラス 5 5 のガラス面であり、 1 1 面は結像面 5 6 である。由率半径および網路の単位はミリメートルである。

## [0109]

#### 【表 5 A】

<b>6</b>	曲率半径		Nd(屈折率)	Vd(アッベ数)	材料
1	150,000	0,400	1,53116	56.0	樹龍
2	27.279	0.298			
3	1.796	0.549	1,53116	56.0	樹脂
4	-1.887	0.352			
5	-0.536	0.331	1,8349.4	24.0	<b>一樹脂</b>
6	-1.225	0.109			
7	1.053	0.992	1,53116	56.0	
8	1.960	0.210			
9	infinity	0,100	1.51680	64.2	光学ガラス
10	infinity	0,791	ļ		
11	infinity	-0.025	<u></u>		<b></b>

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#### [0110]

次に、表5B、表5Cは非球面とされたレンズ面の非球面形状を規定するための非球面係数を示す。表5B、表5Cにおいても物体側から数えた順番で各レンズ面を特定している。

## [袭5B]

	第1面	第2面	第3個	第4面	第5 <b>函</b>	第6面
K	0.00000 E+00	1,68169 E+03	-7.82206 E-01	4.95063 E+00	-3.52793 E+00	0,00000 E+00
A4	1,35856 8-01	4,80109 E-01	1.56539 E-01	-1.62437 E-01	-7.43230 E-01	1.06681 E-01
A6	-2.24346 E-02	-6.34433 E-01	-2.72463 E-02	4,51584 E-01	0.00000 E+00	0.00000 E+00
A8	0.00000 E+00	1.41506 E+00	-7.42170E-01	-1.63061 E+00	9.47084 E-01	7.11233 E-01
A10	0.00000 E+00	0,00000 E+00	~3,96390 E+00	-7.77874 E-02	7,17913 E-01	-3.14780 E-01
A12	0.00000 E+00	0,00000 E+00	7,84072 E+00	2.79269 E÷00	-3.48348 E+00	-6.16063 E-02
A14	0.00000 E+00	0,000000 E+00	0,000000 E+00	0.00000 E÷00	0.000000 E+00	0.00000 E+00
A16	0.00000 E+00	0.000000 E+00	0.000000 E+00	0.00000 E+00	0.000000 E+00	0.00000 E+00

#### [表5C]

	第7面	第8節
K	-8.73455 E+00	0.000000 E+00
A4	-1.85191 E-01	-1,98948 E-01
A6	9.59854 E-02	7,50201 E-02
A8	-3.21706 E-02	~4,53006 E-02
A10	2.48962 E-03	2.82001 E-02
A12	6.31466 E-03	-1.34263 E-02
A14	-7.56292 E-03	3,48357 E-03
A16	2.27749 E-03	-3,70E-04

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## [0111]

#### (作用効果)

図10(a)~(d)は広角レンズ50の緩収差図、機収差図、像面湾曲図、歪曲収差図である。図10(a)に示すように、広角レンズ50によれば、軸上の色収差が良好に補正されている。また、図10(b)に示すように、色の滲みが抑制される。さらに、図10(c)、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レン

ズ50が高解像度となる。

#### [0112]

また、広角レンズ50では、第1レンズ51に凹形状を備える負のパワーのレンズを配置し、第2レンズ52に凸形状を備える正のパワーを有するレンズを配置したので、65%以上の画角を備えるレンズ系の全長を4.1mm程度に抑えることができる。さらに、第4レンズ54の像側レンズ面54bを、変曲点を備える非球面としたので、広角レンズ50からの射出光線の方向を制御することが容易となり、結像面56に入射する主光線入射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面としたので、広角レンズ50が明るく構成される。さらに、4枚のレンズから広角レンズを構成したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの抑制を図ることが容易である。

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## [0113]

#### (摄像装器)

図11は本発明の広角レンズ10を搭載する撮像装置100の説明図である。図11に 元すように、撮像装置100は広角レンズ10の結像面16(焦点位置)にセンサ面10 1aを配置した撮像素子101を備えるものである。撮像素子101は、CCDセンサ或 いはCMOSセンサである。

## [0114]

本例によれば、広角レンズ10のレンズ系の全長しが短いので、撮像装置100を小型化することができる。さらに、広角レンズ10から撮像業子101に入射する主光線入射角度が小さく抑えられるので、撮像装置100における画質の劣化を抑制できる。すなわち、これらの撮像素子101ではセンサ面101aに斜めから入射する光に対して感度が低下する特性を有するので、主光線入射角度が大きくなると画質の劣化を招いてしまうが、本例の広角レンズ10によれば結像面に対する主光線入射角度を小さくすることができるので、センサ面への光線の入射角度に起因する画質の劣化を抑制できる。また、広角レンズ10の解像度が高いので、撮像素子101として顕素数の多い撮像素子101を採用することにより、撮像装置100には、広角レンズ20~50を広角レンズ10と間様に搭載することができ、この場合にも間様の効果を得ることができる。

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#### [0115]

なお、上記の例では、全てのレンズ面が非球面とされているが、第4レンズの像側レンズ面を含む少なくとも2つのレンズ面を非球面とすれば、広角レンズを明るく構成することが容易となる。

## 【符号の説明】

## [0116]

10-20-30-40-50- 、広角レンズ

11-21-31-41-51-- 第1レンズ

12・22・32・42・52・・・第2レンズ

13・23,33・43:53・・・第3レンズ

14,24,34、44.54.,・第4レンズ

14日・24日・34日・44日・54日・・・第4レンズの物体網レンズ面

15 - 25 - 35 - 45 - 55 - - - カバーガラス

16、26、36、46、56、、結像匯

100・・・摄像装置

101 · · · 摄像案子

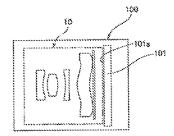
101a・・・撮像素子のセンサ節

D・・・レンズ系のレンズ厚

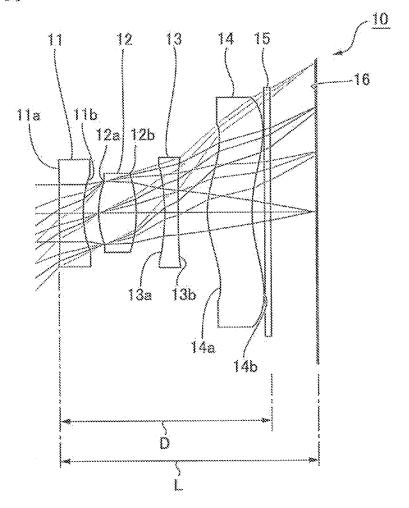
し・・・レンズ系の全長

30.

[211]

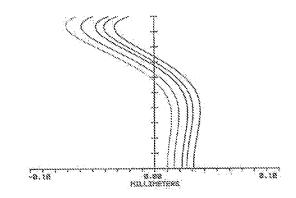


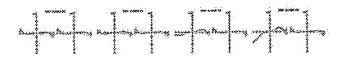
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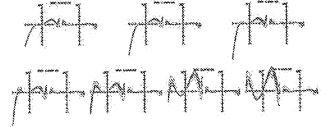
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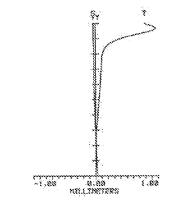


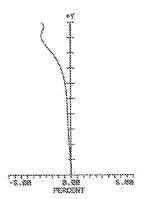


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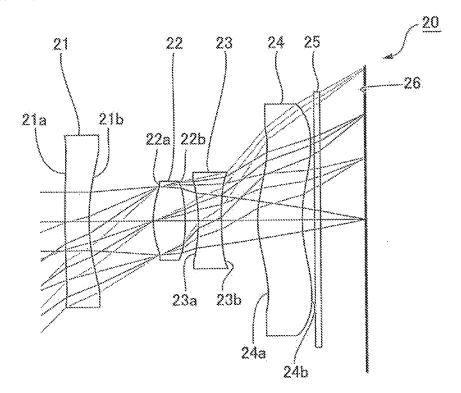


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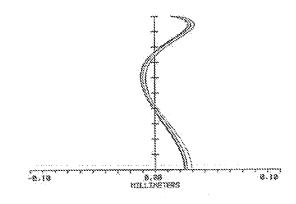


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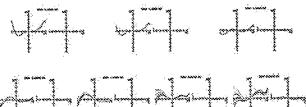
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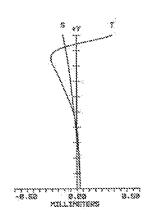


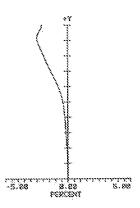


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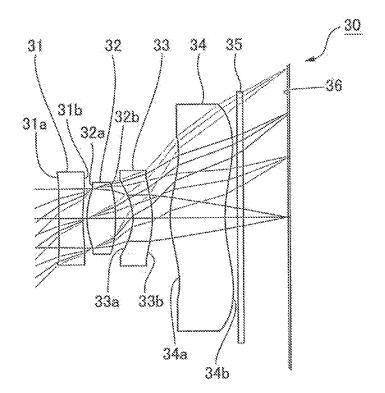


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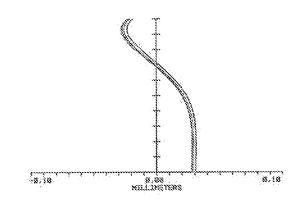


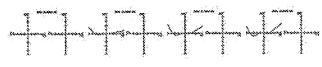
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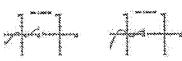
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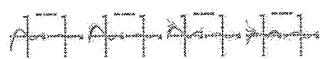
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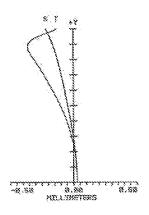


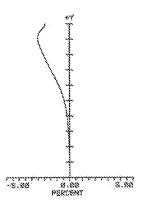




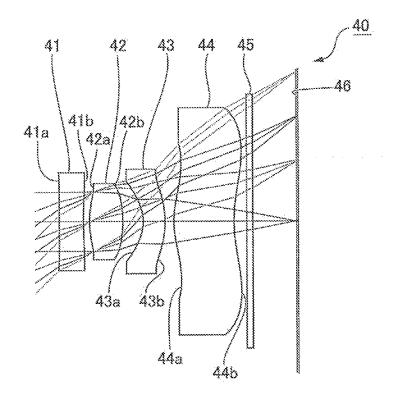


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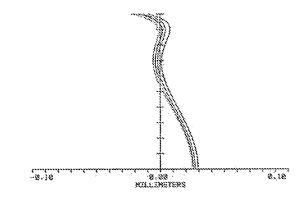


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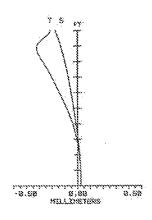


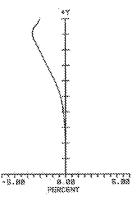
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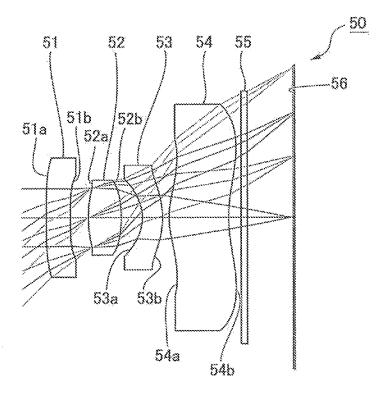


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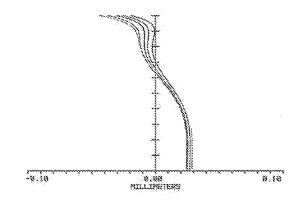


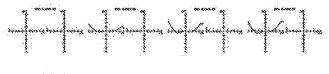
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[810]

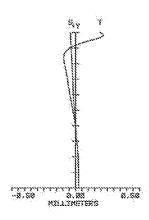
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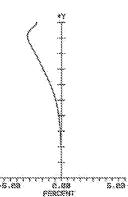






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Fターム(参考) 2H087 KA01 LA01 PA04 PA17 PH04 QA02 QA06 QA17 QA21 QA26 QA32 QA42 QA45 RA04 RA05 RA12 RA13 RA32 RA42 RA44 0401

Electronic Ack	knowledgement Receipt
EFS ID:	20824379
Application Number:	14105811
International Application Number:	
Confirmation Number:	5836
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL
First Named Inventor/Applicant Name:	WEI-YU CHEN
Customer Number:	24728
Filer:	Tim Tingkang Xia/Chenae Byrd
Filer Authorized By:	Tim Tingkang Xia
Attorney Docket Number:	14970-94702
Receipt Date:	01-DEC-2014
Filing Date:	13-DEC-2013
Time Stamp:	12:35:20
Application Type:	Utility under 35 USC 111(a)

# **Payment information:**

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ART UNIT	PAPER NUMBER		
2.872	<u> </u>		

DATE MAILED: 01/27/2015

	APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
_	14/105,811	12/13/2013	WEI-YU CHEN	14970-94702	5836

TITLE OF INVENTION: IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

APPLN. TYPE	ENTITY STATUS	ISSUE FEE DUE	PUBLICATION FEE DUE	PREV. PAID ISSUE FEE	TOTAL FEE(S) DUE	DATE DUE
nonprovisional	UNDISCOUNTED	\$960	\$0	\$0	\$960	04/27/2015

THE APPLICATION IDENTIFIED ABOVE HAS BEEN EXAMINED AND IS ALLOWED FOR ISSUANCE AS A PATENT. PROSECUTION ON THE MERITS IS CLOSED. THIS NOTICE OF ALLOWANCE IS NOT A GRANT OF PATENT RIGHTS. THIS APPLICATION IS SUBJECT TO WITHDRAWAL FROM ISSUE AT THE INITIATIVE OF THE OFFICE OR UPON PETITION BY THE APPLICANT. SEE 37 CFR 1.313 AND MPEP 1308.

THE ISSUE FEE AND PUBLICATION FEE (IF REQUIRED) MUST BE PAID WITHIN <u>THREE MONTHS</u> FROM THE MAILING DATE OF THIS NOTICE OR THIS APPLICATION SHALL BE REGARDED AS ABANDONED. <u>THIS STATUTORY PERIOD CANNOT BE EXTENDED.</u> SEE 35 U.S.C. 151. THE ISSUE FEE DUE INDICATED ABOVE DOES NOT REFLECT A CREDIT FOR ANY PREVIOUSLY PAID ISSUE FEE IN THIS APPLICATION. IF AN ISSUE FEE HAS PREVIOUSLY BEEN PAID IN THIS APPLICATION (AS SHOWN ABOVE), THE RETURN OF PART B OF THIS FORM WILL BE CONSIDERED A REQUEST TO REAPPLY THE PREVIOUSLY PAID ISSUE FEE TOWARD THE ISSUE FEE NOW DUE.

#### HOW TO REPLY TO THIS NOTICE:

I. Review the ENTITY STATUS shown above. If the ENTITY STATUS is shown as SMALL or MICRO, verify whether entitlement to that entity status still applies.

If the ENTITY STATUS is the same as shown above, pay the TOTAL FEE(S) DUE shown above.

If the ENTITY STATUS is changed from that shown above, on PART B - FEE(S) TRANSMITTAL, complete section number 5 titled "Change in Entity Status (from status indicated above)".

For purposes of this notice, small entity fees are 1/2 the amount of undiscounted fees, and micro entity fees are 1/2 the amount of small entity fees

II. PART B - FEE(S) TRANSMITTAL, or its equivalent, must be completed and returned to the United States Patent and Trademark Office (USPTO) with your ISSUE FEE and PUBLICATION FEE (if required). If you are charging the fee(s) to your deposit account, section "4b" of Part B - Fee(s) Transmittal should be completed and an extra copy of the form should be submitted. If an equivalent of Part B is filed, a request to reapply a previously paid issue fee must be clearly made, and delays in processing may occur due to the difficulty in recognizing the paper as an equivalent of Part B.

III. All communications regarding this application must give the application number. Please direct all communications prior to issuance to Mail Stop ISSUE FEE unless advised to the contrary.

IMPORTANT REMINDER: Utility patents issuing on applications filed on or after Dec. 12, 1980 may require payment of maintenance fees. It is patentee's responsibility to ensure timely payment of maintenance fees when due.

#### PART B - FEE(S) TRANSMITTAL

## Complete and send this form, together with applicable fee(s), to: Mail Mail Stop ISSUE FEE

Mail Stop ISSUE FEE Commissioner for Patents P.O. Box 1450

Alexandria, Virginia 22313-1450

or <u>Fax</u> (571)-273-2885

INSTRUCTIONS: This form should be used for transmitting the ISSUE FEE and PUBLICATION FEE (if required). Blocks 1 through 5 should be completed where appropriate. All further correspondence including the Patent, advance orders and notification of maintenance fees will be mailed to the current correspondence address as indicated unless corrected below or directed otherwise in Block 1, by (a) specifying a new correspondence address; and/or (b) indicating a separate "FEE ADDRESS" for maintenance fee notifications.

maintenance fee notifications. Note: A certificate of mailing can only be used for domestic mailings of the Fee(s) Transmittal. This certificate cannot be used for any other accompanying papers. Each additional paper, such as an assignment or formal drawing, must have its own certificate of mailing or transmission. CURRENT CORRESPONDENCE ADDRESS (Note: Use Block 1 for any change of address) Certificate of Mailing or Transmission 24728 7590 01/27/2015 I hereby certify that this Fee(s) Transmittal is being deposited with the United States Postal Service with sufficient postage for first class mail in an envelope addressed to the Mail Stop ISSUE FEE address above, or being facsimile transmitted to the USPTO (571) 273-2885, on the date indicated below. MORRIS MANNING MARTIN LLP **IP** Department 3343 PEACHTREE ROAD, NE (Depositor's name 1600 ATLANTA FINANCIAL CENTER (Signature ATLANTA, GA 30326 (Date APPLICATION NO. FILING DATE FIRST NAMED INVENTOR ATTORNEY DOCKET NO. CONFIRMATION NO. 14/105.811 12/13/2013 WEI-YU CHEN 14970-94702 5836 TITLE OF INVENTION: IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL APPLN. TYPE ISSUE FEE DUE PUBLICATION FEE DUE PREV. PAID ISSUE FEE TOTAL FEE(S) DUE **ENTITY STATUS** DATE DUE UNDISCOUNTED \$0 \$0 04/27/2015 \$960 \$960 nonprovisional **EXAMINER** ART UNIT CLASS-SUBCLASS DINH, JACK 2872 359-779000 1. Change of correspondence address or indication of "Fee Address" (37 CFR 1.363). 2. For printing on the patent front page, list (1) The names of up to 3 registered patent attorneys ☐ Change of correspondence address (or Change of Correspondence Address form PTO/SB/122) attached. or agents OR, alternatively, (2) The name of a single firm (having as a member a registered attorney or agent) and the names of up to 2 registered patent attorneys or agents. If no name is listed, no name will be printed. ☐ "Fee Address" indication (or "Fee Address" Indication form PTO/SB/47; Rev 03-02 or more recent) attached. Use of a Customer Number is required. 3. ASSIGNEE NAME AND RESIDENCE DATA TO BE PRINTED ON THE PATENT (print or type) PLEASE NOTE: Unless an assignee is identified below, no assignee data will appear on the patent. If an assignee is identified below, the document has been filed for recordation as set forth in 37 CFR 3.11. Completion of this form is NOT a substitute for filing an assignment. (A) NAME OF ASSIGNEE (B) RESIDENCE: (CITY and STATE OR COUNTRY) Please check the appropriate assignee category or categories (will not be printed on the patent): 🔲 Individual 📮 Corporation or other private group entity 🖵 Government 4a. The following fee(s) are submitted: 4b. Payment of Fee(s): (Please first reapply any previously paid issue fee shown above) ☐ Issue Fee A check is enclosed. ☐ Publication Fee (No small entity discount permitted) Payment by credit card. Form PTO-2038 is attached. Advance Order - # of Copies \_ The director is hereby authorized to charge the required fee(s), any deficiency, or credits any overpayment, to Deposit Account Number 5. Change in Entity Status (from status indicated above) NOTE: Absent a valid certification of Micro Entity Status (see forms PTO/SB/15A and 15B), issue fee payment in the micro entity amount will not be accepted at the risk of application abandonment. Applicant certifying micro entity status. See 37 CFR 1.29 ☐ Applicant asserting small entity status. See 37 CFR 1.27  $\underline{NOTE}$ : If the application was previously under micro entity status, checking this box will be taken to be a notification of loss of entitlement to micro entity status. ☐ Applicant changing to regular undiscounted fee status. NOTE: Checking this box will be taken to be a notification of loss of entitlement to small or micro entity status, as applicable. NOTE: This form must be signed in accordance with 37 CFR 1.31 and 1.33. See 37 CFR 1.4 for signature requirements and certifications. Authorized Signature \_ Date

> HP, Ex. 1002 Page 209

Typed or printed name \_

Registration No. \_



## UNITED STATES PATENT AND TRADEMARK OFFICE

UNITED STATES DEPARTMENT OF COMMERCE United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS

P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov

APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
14/105,811	12/13/2013	WEI-YU CHEN	14970-94702	5836
24728 75	90 01/27/2015		EXAM	INER
	IING MARTIN LLP	DINH, JACK		
IP Department				
3343 PEACHTREI	E ROAD, NE		ART UNIT	PAPER NUMBER
	INANCIAL CENTER	2872		
ATLANTA, GA 30	)326	DATE MAILED: 01/27/201	5	

## Determination of Patent Term Adjustment under 35 U.S.C. 154 (b)

(Applications filed on or after May 29, 2000)

The Office has discontinued providing a Patent Term Adjustment (PTA) calculation with the Notice of Allowance.

Section 1(h)(2) of the AIA Technical Corrections Act amended 35 U.S.C. 154(b)(3)(B)(i) to eliminate the requirement that the Office provide a patent term adjustment determination with the notice of allowance. See Revisions to Patent Term Adjustment, 78 Fed. Reg. 19416, 19417 (Apr. 1, 2013). Therefore, the Office is no longer providing an initial patent term adjustment determination with the notice of allowance. The Office will continue to provide a patent term adjustment determination with the Issue Notification Letter that is mailed to applicant approximately three weeks prior to the issue date of the patent, and will include the patent term adjustment on the patent. Any request for reconsideration of the patent term adjustment determination (or reinstatement of patent term adjustment) should follow the process outlined in 37 CFR 1.705.

Any questions regarding the Patent Term Extension or Adjustment determination should be directed to the Office of Patent Legal Administration at (571)-272-7702. Questions relating to issue and publication fee payments should be directed to the Customer Service Center of the Office of Patent Publication at 1-(888)-786-0101 or (571)-272-4200.

#### OMB Clearance and PRA Burden Statement for PTOL-85 Part B

The Paperwork Reduction Act (PRA) of 1995 requires Federal agencies to obtain Office of Management and Budget approval before requesting most types of information from the public. When OMB approves an agency request to collect information from the public, OMB (i) provides a valid OMB Control Number and expiration date for the agency to display on the instrument that will be used to collect the information and (ii) requires the agency to inform the public about the OMB Control Number's legal significance in accordance with 5 CFR 1320.5(b).

The information collected by PTOL-85 Part B is required by 37 CFR 1.311. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 12 minutes to complete, including gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, Virginia 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, Virginia 22313-1450. Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

#### **Privacy Act Statement**

The Privacy Act of 1974 (P.L. 93-579) requires that you be given certain information in connection with your submission of the attached form related to a patent application or patent. Accordingly, pursuant to the requirements of the Act, please be advised that: (1) the general authority for the collection of this information is 35 U.S.C. 2(b)(2); (2) furnishing of the information solicited is voluntary; and (3) the principal purpose for which the information is used by the U.S. Patent and Trademark Office is to process and/or examine your submission related to a patent application or patent. If you do not furnish the requested information, the U.S. Patent and Trademark Office may not be able to process and/or examine your submission, which may result in termination of proceedings or abandonment of the application or expiration of the patent.

The information provided by you in this form will be subject to the following routine uses:

- 1. The information on this form will be treated confidentially to the extent allowed under the Freedom of Information Act (5 U.S.C. 552) and the Privacy Act (5 U.S.C 552a). Records from this system of records may be disclosed to the Department of Justice to determine whether disclosure of these records is required by the Freedom of Information Act.
- 2. A record from this system of records may be disclosed, as a routine use, in the course of presenting evidence to a court, magistrate, or administrative tribunal, including disclosures to opposing counsel in the course of settlement negotiations.
- 3. A record in this system of records may be disclosed, as a routine use, to a Member of Congress submitting a request involving an individual, to whom the record pertains, when the individual has requested assistance from the Member with respect to the subject matter of the record.
- 4. A record in this system of records may be disclosed, as a routine use, to a contractor of the Agency having need for the information in order to perform a contract. Recipients of information shall be required to comply with the requirements of the Privacy Act of 1974, as amended, pursuant to 5 U.S.C. 552a(m).
- 5. A record related to an International Application filed under the Patent Cooperation Treaty in this system of records may be disclosed, as a routine use, to the International Bureau of the World Intellectual Property Organization, pursuant to the Patent Cooperation Treaty.
- 6. A record in this system of records may be disclosed, as a routine use, to another federal agency for purposes of National Security review (35 U.S.C. 181) and for review pursuant to the Atomic Energy Act (42 U.S.C. 218(c)).
- 7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
- 8. A record from this system of records may be disclosed, as a routine use, to the public after either publication of the application pursuant to 35 U.S.C. 122(b) or issuance of a patent pursuant to 35 U.S.C. 151. Further, a record may be disclosed, subject to the limitations of 37 CFR 1.14, as a routine use, to the public if the record was filed in an application which became abandoned or in which the proceedings were terminated and which application is referenced by either a published application, an application open to public inspection or an issued patent.

	Application No. 14/105,811	Applicant(s) CHEN, WEI-YU		
Notice of Allowability	Examiner JACK DINH	Art Unit 2872	AIA (First Inventor to File) Status Yes	
The MAILING DATE of this communication appearable communication appearable claims being allowable, PROSECUTION ON THE MERITS IS (herewith (or previously mailed), a Notice of Allowance (PTOL-85) of NOTICE OF ALLOWABILITY IS NOT A GRANT OF PATENT RICE of the Office or upon petition by the applicant. See 37 CFR 1.313	OR REMAINS) CLOSED in this app or other appropriate communication GHTS. This application is subject to	lication. If not will be mailed i	e address included in due course. THIS	
1. This communication is responsive to the communication filed A declaration(s)/affidavit(s) under 37 CFR 1.130(b) was/				
<ol> <li>An election was made by the applicant in response to a restr requirement and election have been incorporated into this ac</li> </ol>		ne interview on	; the restriction	
<ol> <li>The allowed claim(s) is/are <u>1-26</u>. As a result of the allowed c Highway program at a participating intellectual property offic <a href="http://www.uspto.gov/patents/init_events/pph/index.jsp">http://www.uspto.gov/patents/init_events/pph/index.jsp</a> or ser</li> </ol>	e for the corresponding application.	For more inform		
4. Acknowledgment is made of a claim for foreign priority under Certified copies:	r 35 U.S.C. § 119(a)-(d) or (f).			
a) ☑ All b) ☐ Some *c) ☐ None of the:  1. ☑ Certified copies of the priority documents have 2. ☐ Certified copies of the priority documents have 3. ☐ Copies of the certified copies of the priority doc International Bureau (PCT Rule 17.2(a)).  * Certified copies not received:	been received in Application No		application from the	
Applicant has THREE MONTHS FROM THE "MAILING DATE" of noted below. Failure to timely comply will result in ABANDONMI THIS THREE-MONTH PERIOD IS NOT EXTENDABLE.		complying with	the requirements	
5. CORRECTED DRAWINGS ( as "replacement sheets") must	be submitted.			
including changes required by the attached Examiner's Paper No./Mail Date	Amendment / Comment or in the Of	ffice action of		
Identifying indicia such as the application number (see 37 CFR 1.6 each sheet. Replacement sheet(s) should be labeled as such in the			not the back) of	
<ol> <li>DEPOSIT OF and/or INFORMATION about the deposit of BI attached Examiner's comment regarding REQUIREMENT FO</li> </ol>			ne	
Attachment(s)  1. ☐ Notice of References Cited (PTO-892)  2. ☑ Information Disclosure Statements (PTO/SB/08), Paper No./Mail Date 20141201  3. ☐ Examiner's Comment Regarding Requirement for Deposit of Biological Material  4. ☐ Interview Summary (PTO-413), Paper No./Mail Date	5. ☐ Examiner's Amendn 6. ☑ Examiner's Stateme 7. ☐ Other			
/JACK DINH/ Primary Examiner, Art Unit 2872				

U.S. Patent and Trademark Office PTOL-37 (Rev. 08-13) Application/Control Number: 14/105,811 Page 2

Art Unit: 2872

**REASONS FOR ALLOWANCE** 

1. Claims 1-26 are allowed. The following is an examiner's statement of reasons for

allowance. Regarding claims 1, 15 and 21, the prior art fails to satisfy the conditions as claimed.

2. The prior art taken either singly or in combination fails to anticipate or fairly suggest the

limitations of the independent claims, in such a manner that a rejection under 35 USC 102 or 103

would be improper. Any comments considered necessary by applicant must be submitted no

later than the payment of the issue fee and, to avoid processing delays, should preferably

accompany the issue fee. Such submissions should be clearly labeled "Comments on Statement

of Reasons for Allowance."

Other Information/Remarks

3. Any inquiry concerning this communication or earlier communications from the

examiner should be directed to JACK DINH whose telephone number is (571)272-2327. The

examiner can normally be reached on M-F (7:30 AM - 4:00 PM).

If attempts to reach the examiner by telephone are unsuccessful, the examiner's

supervisor, Thomas K. Pham can be reached on 571-272-3689. The fax phone number for the

organization where this application or proceeding is assigned is 571-273-8300.

HP, Ex. 1002 Page 213 Application/Control Number: 14/105,811 Page 3

Art Unit: 2872

Information regarding the status of an application may be obtained from the Patent Application Information Retrieval (PAIR) system. Status information for published applications may be obtained from either Private PAIR or Public PAIR. Status information for unpublished applications is available through Private PAIR only. For more information about the PAIR system, see http://pair-direct.uspto.gov. Should you have questions on access to the Private PAIR system, contact the Electronic Business Center (EBC) at 866-217-9197 (toll-free). If you would like assistance from a USPTO Customer Service Representative or access to the automated information system, call 800-786-9199 (IN USA OR CANADA) or 571-272-1000.

/Jack Dinh/ Primary Examiner, Art Unit 2872 01/12/15

	Application/Control No.	Applicant(s)/Patent Under Reexamination
Index of Claims	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

<b>✓</b>	Rejected	[-	Cancelled	N	N Non-Elected		A	Appeal	
=	Allowed	÷	Restricted	I	I Interference		0	Objected	
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☐ Claims r	renumbered	in the same o	order as pre	esented by a	applicant		□ СРА	□ т.с	D. 🗆	R.1.47
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U.S. Patent and Trademark Office Part of Paper No.: 20150112

# **EAST Search History**

# **EAST Search History (Prior Art)**

Ref #	Hits	Search Query	DBs	Default Operator	Plurals	Time Stamp
L1	0	"14105811"	US-PGPUB; USPAT	OR	OFF	2015/01/12 06:50
L2	1	("8842379").PN.	USPAT; USOCR	OR	OFF	2015/01/12 07:09
L3	2	"20100165485"	US-PGPUB; USPAT	OR	OFF	2015/01/12 07:12
L4	10323	lens\$2 same (first) same (second near6 positive) same (third near6 negative) same (fourth)	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L5	396	(359/771).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L6	308	(359/772).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L7	186	(359/779).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L8	284	(359/781).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L9	1059	(359/771,772,779,781).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:16
L10	265	L9 and L4	US-PGPUB; USPAT;	OR	:1	2015/01/12 07:16

HP, Ex. 1002

			USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB			
L11	636	lens\$2 same (first) same ((second near6 positive) with convex with image) same ((third near6 negative) with concave with object with convex with image) same (fourth with concave with image)	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L12	889	(359/715).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L13	1714	(359/715,771,772,779,781).OCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L14	86	L11 and L13	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18

#### **EAST Search History (Interference)**

Ref #	Hits	Search Query	DBs	Default Operator	Plurals	Time Stamp
L15		(lens\$2 and (first) and ((second near6 positive) with convex with image) and ((third near6 negative) with concave with object with convex with image) and (fourth with concave with image)).clm.	PGPUB;	OR	OFF	2015/01/12 07:30
L16		(lens\$2 and (first) and ((second near6 positive) with convex with image) and ((third near6 negative) with concave with object with convex with image) and (fourth with concave with image) and Td and HFOV).clm.	PGPUB;	OR	OFF	2015/01/12 07:30

1/12/2015 7:31:07 AM

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### Search Notes



Application/Control No.	Applicant(s)/Patent Under Reexamination
14105811	CHEN, WEI-YU
Examiner	Art Unit
JACK DINH	2872

Date	Examiner
	Date

CPC COMBINATION SETS - SEARC	CHED	
Symbol	Date	Examiner

	US CLASSIFICATION SEARCHE	:D	
Class	Subclass	Date	Examiner
359	771,772,779,781,715	01/12/15	JD

SEARCH NOTES		
Search Notes	Date	Examiner
Search EAST and NPL.	01/12/15	JD

	INTERFERENCE SEARCH		
US Class/ CPC Symbol	US Subclass / CPC Group	Date	Examiner
See search history.		01/12/15	JD

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Ex. 1002
Daga 210

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Papp Paper No.: 20150112



UNITED STATES DEPARTMENT OF COMMERCE United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov

#### **BIB DATA SHEET**

#### **CONFIRMATION NO. 5836**

SERIAL NUM	BER	FILING O			CLASS	GRO	OUP ART	UNIT	ATTC	RNEY DOCKET NO.
14/105,81	1	12/13/2			359		2872		1	4970-94702
		RUL	E							
APPLICANTS LARGAN		SION CO., L	TD., Taich	iung, T	AlWAN, Assigne	e (wit	h 37 CFF	R 1.172 I	nteres	st);
INVENTORS WEI-YU CHEN, Taichung, TAIWAN;										
** CONTINUING	G DATA	<b>4</b> **********	*****	<b>k</b>						
** <b>FOREIGN AI</b> TAIWAN		ATIONS ***** 0029 10/29/20		*****	*					
** <b>IF REQUIRE</b> 01/02/201		EIGN FILING	LICENS	E GRA	ANTED **					
Foreign Priority claime 35 USC 119(a-d) cond		Yes No	☐ Met af Allowa	ter ince	STATE OR COUNTRY		IEETS WINGS	TOT.		INDEPENDENT CLAIMS
	JACK DIN Examiner's		Initials		TAIWAN		23	26		3
MORRIS IP Depart 3343 PEA 1600 ATL ATLANTA	ADDRESS  MORRIS MANNING MARTIN LLP IP Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326 UNITED STATES									
TITLE										
IMAGE C	APTUF	RING LENS S	YSTEM, I	MAGIN	NG DEVICE AND	MOE	BILE TER	MINAL		
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		foi					☐ 1.18 F	ees (lss	sue)	
							Other			
							☐ Credit			

## Issue Classification



Application/Control No.	Applicant(s)/Patent Under Reexamination
14105811	CHEN, WEI-YU
Examiner	Art Unit
JACK DINH	2872

CPC	CPC						
Symbol			Туре	Version			
G02B	13	7 004	F	2013-01-01			
G02B	9	34	I	2013-01-01			
		/					

CPC Combination Sets									
Symbol	Туре	Set	Ranking	Version					

NONE	NE					
(Assistant Examiner)	(Date)	2	6			
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure			
(Primary Examiner)	(Date)	1	1A			

U.S. Patent and Trademark Office Part of Paper No. 20150112

## Issue Classification

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Application/Control No.	Applicant(s)/Patent Under Reexamination
14105811	CHEN, WEI-YU
Examiner	Art Unit
JACK DINH	2872

	US ORIGINAL CLASSIFICATION						INTERNATIONAL CLASSIFICATION							
	CLASS SUBCLASS								С	LAIMED			N	ON-CLAIMED
359	59 779			G	0	2	В	9 / 34 (2006.0)						
	CROSS REFERENCE(S)					G	0	2	В	3 / 02 (2006.01.01)				
CLASS	SU	BCLASS (ON	E SUBCLAS	S PER BLO	CK)									
359	781	715												

NONE			ns Allowed:
(Assistant Examiner)	(Date)	2	Ь
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure
(Primary Examiner)	(Date)	1	1A

## Issue Classification



	Application/Control No.	Applicant(s)/Patent Under Reexamination
)	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

☐ Claims renumbered in the same order as presented by applicant									☐ CPA ☐ T.D. ☐ R.1.47						
Final	Original	Final	Original	Final	Original	Final	Original	Final	Original	Final	Original	Final	Original	Final	Original
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2	2	18	18												
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NONE			ns Allowed:
(Assistant Examiner)	(Date)	2	0
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure
(Primary Examiner)	(Date)	1	1A

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Beceipt date: 12/01/2014

14105811 - GALL::2872

Doc description: Information Disclosure Statement (IDS) Filed

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# INFORMATION DISCLOSURE STATEMENT BY APPLICANT

( Not for submission under 37 CFR 1.99)

Application Number		14105811				
Filing Date		2013-12-13				
First Named Inventor	WEI-Y	/U CHEN				
Art Unit		2872				
Examiner Name						
Attorney Docket Number	er	14970-94702				

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Examiner Initial*	Cite No	Patent Number	Kind Code <sup>1</sup>	Issue D	)ate	Name of Pate of cited Docu	entee or Applicant ument	Relev	s,Columns,Lines where ant Passages or Relev es Appear	
	1	8842379	B2	2014-09	9-23	Largan Precision Co., Ltd.				
If you wis	h to ac	_   ld additional U.S. Pate	nt citatio	n inform	ation pl	l ease click the	Add button.		Add	
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Examiner Initial*	Cite I	No Publication Number	Kind Code <sup>1</sup>	Publication Name of Patentee or Applicant of cited Document			Pages,Columns,Lines whe Relevant Passages or Rele Figures Appear			
	1	20100165485	A1	2010-07	'-01	Milestone Co., Ltd.				
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	1	2014-178623	JP			2014-09-25 Hitachi Maxell, Ltd.				×
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Receipt	date	: 12	2/01/2014	Application Number		14105811 14	1105811 - GAU:	2872
				Filing Date		2013-12-13		
			DISCLOSURE	First Named Inventor	WEI	-YU CHEN		
			BY APPLICANT	Art Unit		2872		
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				Attorney Docket Numl	er	14970-94702		
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<sup>&</sup>lt;sup>4</sup> Kind of document by the appropriate symbols as indicated on the document under WIPO Standard ST.16 if possible. <sup>5</sup> Applicant is to place a check mark here if English language translation is attached.

		Filing Date		2013-12-13			
STATEMENT BY APPLICANT (Not for submission under 37 CFR 1.99)			First Named Inventor WEI		YU CHEN		
			Art Unit		2872		
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			Attorney Docket Nu	mber	14970-94702		
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Name/Print Tim Tingkang Xia		Registration		n Number	45242		
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**Application Number** 

14105811

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14105811 - GAU: 2872

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- 6. A record in this system of records may be disclosed, as a routine use, to another federal agency for purposes of National Security review (35 U.S.C. 181) and for review pursuant to the Atomic Energy Act (42 U.S.C. 218(c)).
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Date FEBRUARY 5, 2015

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Authorized Signature \_/Tim Tingkang Xia/

Typed or printed name \_\_\_TIM\_TINGKANG XIA

Electronic Patent Application Fee Transmittal								
Application Number:	141	105811						
Filing Date:	13-	Dec-2013						
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TER							
First Named Inventor/Applicant Name:	WEI-YU CHEN							
Filer:	Tim Tingkang Xia/Michelle Ellis							
Attorney Docket Number:	149	970-94702						
Filed as Large Entity								
Filing Fees for Utility under 35 USC 111(a)								
Description		Fee Code	Quantity	Amount	Sub-Total in USD(\$)			
Basic Filing:								
Pages:								
Claims:								
Miscellaneous-Filing:								
Petition:								
Patent-Appeals-and-Interference:								
Post-Allowance-and-Post-Issuance:								
Utility Appl Issue Fee		1501	1	960	960			

Description	Fee Code	Quantity	Amount	Sub-Total in USD(\$)
Extension-of-Time:				
Miscellaneous:				
	Tot	al in USD	(\$)	960

Electronic Acknowledgement Receipt						
EFS ID:	21413714					
Application Number:	14105811					
International Application Number:						
Confirmation Number:	5836					
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL					
First Named Inventor/Applicant Name:	WEI-YU CHEN					
Customer Number:	24728					
Filer:	Tim Tingkang Xia/Michelle Ellis					
Filer Authorized By:	Tim Tingkang Xia					
Attorney Docket Number:	14970-94702					
Receipt Date:	05-FEB-2015					
Filing Date:	13-DEC-2013					
Time Stamp:	16:13:28					
Application Type:	Utility under 35 USC 111(a)					

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	issue ree rayment (170 656)	1437 0347 0211 Halls.pai	e9bd3b49fe968014aae0f6c3ba7a6e23a5b 10b97	110	
Warnings:					
Information:					
2	Fee Worksheet (SB06)	fee-info.pdf	30962	no	2
2	ree worksheet (3500)	ree imo.pui	a3a145258b1acecbb216b5689e7580bb1e 1c8a5b	110	
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#### New International Application Filed with the USPTO as a Receiving Office

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eipt date: 12/01/2014

14105811 - GA

Doc description: Information Disclosure Statement (IDS) Filed

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Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it contains a valid OMB control number.

	Application Number		14105811	
NEODMATION DIOCE COURT	Filing Date		2013-12-13	
INFORMATION DISCLOSURE	First Named Inventor WEI-		/U CHEN	
STATEMENT BY APPLICANT  Not for submission under 37 CFR 1.99)	Art Unit		2872	
Not for Submission under or or it 1.00,	Examiner Name			
Change(s) applied	Attorney Docket Number	er	14970-94702	

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/M.I.G./ Remove 2/10/2015 **U.S.PATENTS** Pages, Columns, Lines where Examiner Cite Kind Name of Patentee or Applicant Relevant Passages or Relevant Patent Number Issue Date Initial\* Code<sup>1</sup> of cited Document No Figures Appear 1 8842379 B2 2014-09-23 Largan Precision Co., Ltd. Hsu, et al.

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	1	2014-178623	JP		2014-09-25	Hitachi Maxell, Ltd.		X		
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APPLICATION NO.	ISSUE DATE	PATENT NO.	ATTORNEY DOCKET NO.	CONFIRMATION NO.
14/105,811	03/24/2015	8988796	14970-94702	5836

8988796

24728

7590

03/04/2015

MORRIS MANNING MARTIN LLP **IP** Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326

#### ISSUE NOTIFICATION

The projected patent number and issue date are specified above.

#### **Determination of Patent Term Adjustment under 35 U.S.C. 154 (b)**

(application filed on or after May 29, 2000)

The Patent Term Adjustment is 0 day(s). Any patent to issue from the above-identified application will include an indication of the adjustment on the front page.

If a Continued Prosecution Application (CPA) was filed in the above-identified application, the filing date that determines Patent Term Adjustment is the filing date of the most recent CPA.

Applicant will be able to obtain more detailed information by accessing the Patent Application Information Retrieval (PAIR) WEB site (http://pair.uspto.gov).

Any questions regarding the Patent Term Extension or Adjustment determination should be directed to the Office of Patent Legal Administration at (571)-272-7702. Questions relating to issue and publication fee payments should be directed to the Application Assistance Unit (AAU) of the Office of Data Management (ODM) at (571)-272-4200.

APPLICANT(s) (Please see PAIR WEB site http://pair.uspto.gov for additional applicants):

LARGAN PRECISION CO., LTD., Taichung, TAIWAN, Assignee (with 37 CFR 1.172 Interest); WEI-YU CHEN, Taichung, TAIWAN;

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